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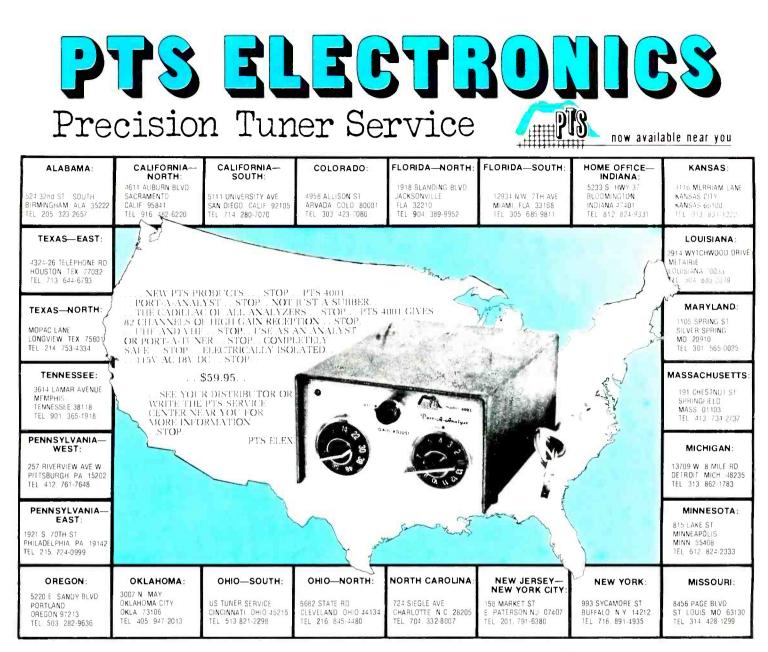
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Radio-Electronics

More than 65 years of electronics publishing

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ON THE COVER

This complete computer terminal is equipped to operate over phone lines and has an output you can connect a tape recorder to. Best of all, you build it from a kit. Get all the details in the article starting on page 42.



DIGITAL MULTIMETERS UND == \$300? There's a heap of them. Here's a wrapup showing what's available and what they will do.see page 45

ugo Gernsback (1884-1967) founder I. Harvey Gernsback editor-in-chief and publisher arry Steckler, CET, editor tobert F. Scott, W2PWG, CET, technical editor

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contributing high-fidelity editor David Lachenbruch, contributing ad tor Barbara Schwartz, editorial assistant Vincent P. Cicenia, production mainager Sarah Martin, production assistant Harriet I. Matysko, circulation director Artine R. Bailey, advertising coordinator Advertising Sales Offices, see page 16

Cover photograph by Walter Herstati Cover design by Louis G. Rubsamen

Radio-Electronics is indexed in Apolied Science & Technology Index and Readers Guide to Periodical Literature.

Radio-Electronics, Published monthly by Gernsback Publications, Inc., 200 Park Averue South, New York City 10003, Phone: 212-777-1400. Second-class postage paid at New York, N.Y. and additional mailing offices. One-year subscription rate: U.S.A., U.S. possessions and Canada, \$8.75. Pan-American countries, \$10.25. Other countries, \$10.75. Single copies 75c. © 1974 ty Bernsback Publications, Inc. All rights reservent. Printed in U.S.A.

Subscription Service: Mail all subscription orders, changes, correspondence and Postmaster Notices of undelivered copies (Form 3579) to Radio-Electronics Subscription Service, Boulder, Colo. 30302.

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1974

NOVEMBER

looking ahead

Flat TV screen

The long quest for a thinpanel electroluminescent TV screen as a substitute for the cathode ray tube may be nearly over, according to scientists at Japan's Sharp Corp. They claim to have overcome the drawbacks in previous devices-short life and low brightness. Lab samples of Sharp's thin-film panels have been operated for 10,000 hours "without any indication of degradation'' and with brightness of more than 60 foot-lamberts at the regular 60-fields-per-second TV scanning rate. Contrast ratio was given as better than 60 to 1.

Sharp's panel, said to be about the thickness of a windowpane, is a three-layer sandwich (electroluminescent layer between two insulating layers) and is driven at a peak voltage of 260 volts ac. The experimental unit is 48 x 36 mm (about 1.9 x 1.4 in.), has 81 picture elements vertically, 108 horizontally, and is addressed by horizontal and vertical grids. Sharp says production is now feasible and the initial applications probably will be for calcuator and computer display, rather than TV. The device currently is monochrome (orange-yellow), but Sharp is working on a three-color version. Sharp officials are so confident they're on the right track that they predict the first no-tube television set within "the next few years.'

Digital watches

The electronic digital watch soon will be the hottest new product on the market, and there are indications that prices will decline as rapidly as those of electronic calculators. Until very recently, LED and liquid-crystal types were selling at \$250 and up. During the summer, new models came out in the \$200 range, followed shortly by watches as cheap as \$120. Next step: \$85. Timex is now marketing a liquid-crystal quartz wristwatch at that price. Not only are the traditional watch manufacturers in the race, but the calculator manufacturers such as Bowmar, Casio and Eiko—are joining in, and before long the makers of IC's are expected to enter the market with their own brand watches, just as they did in the calculator field.

Calculators, meanwhile, are glutting the market. With an oversupply, the calculator industry underwent a severe recession last summer and was counting on the student and Christmas markets to help pull them out. Despite inflation, prices continued to drift downwards, with under-\$20 units no longer unusual and an occasional bargain showing up at less than \$15.

Audio price probe

Is there illegal price-fixing in the audio components business? Spurred by complaints from dealers, the Federal Trade Commission has launched a nationwide investigation to determine whether brand-name manufacturers and importers are withholding merchandise illegally from dealers who sell below specified minimum prices. The FTC revealed no details of its inquiry, but it's believed to cover not only the traditional audio retailers but mail-order houses which advertise in audio publications and various other discount operations, such as those in large cities which quote discount prices by telephone.

Solid-state sweeps TV

It probably won't come as any surprise that solid-state circuitry is finally overtaking the television industry. In the first half of 1974, nearly 63% of all color sets produced or imported into the United States were solid-state models, as compared to only 36.5% in the first half of 1973. In the 1974 period, more than 83% of all consoles and 54.5% of all portables and table models were solid-state, but solid-state construction accounted for only a little more than 30% of monochrome sets.

Portables and table models continued to increase their share of the color TV market. representing 71% of all sets in the 1974 period, up from 66% in the first half of 1973. The fastest growing picture tube sizes were the new 13-, 15- and 17-inch categories, at the expense of the 12-inchand-under and the 25-inch sizes. Remote control may be coming into its own, accounting for a record 8.2% of color sets in January-June 1974, up from 4.6% in the same 1973 period.

In black-and-white, the 11and 12-inch sizes represented more than one half of the total supply for the first time (it was less than 40% one year earlier), and the monochrome console finally has virtually disappeared, dropping to only 2% of the total.

Tighter UHF rules?

After 22 years of UHF broadcasting, there is a strong feeling among engineers on the FCC staff that new measures are necessary to bring a greater level of equality between UHF and VHF television stations. These could take the form of new regulations aimed at better performance of UHF transmitters or receivers or both. Recent FCC tests of receivers indicate that the performance level of UHF tuners has improved little, if at all, in two decades. The Public Broadcasting System is beginning a series of tests of both transmitters and receivers which could result in recommendations to the FCC for further action to mandate UHF-VHF parity. The all-channel law already resulted in bringing the UHF receiver population close to 100% of TV households. The more recent tunerparity rules make UHF as simple to tune as VHF in current-model receivers—if the viewer can locate the UHF signals at all.

Some sentiment is discernable at the FCC for an amendment to the all-channel law to give the Commission the authority to establish UHF tuner performance standards. The FCC currently has the power to fix noise levels only -and it's felt that congressional action would be required to give it greater authority over other performance factors. So far there's no groundswell for further action on UHF, but it could build up in the coming months.

\$31.6 billion for electronics

The U.S. electronics industry brought in \$31.6 billion in factory sales last year, according to EIA. The biggest segment was the communications and industrial market, which accounted for \$12.9 billion, followed by government electronics (military, space, etc.) at \$10.8 billion. The consumer market accounted for sales of \$6.9 billion, while replacement parts represented \$920 million in sales. All segments of the market registered increases in 1973, and total electronics business was up 7.4% from \$29.5 billion in 1973.

The other matrix

Although most of the publicity in the four-channel record race has gone to the discrete CD-4 (Quadradisc) and SQ matrix systems, another matrix system is now making a major bid. This is the QS system, being pushed by Sansui.

Sansui's catchword is Vario-Matrix, which describes a new four-chip decoder circuit that has a three-position switch for decoding QS discs, SQ discs and synthesizing fourchannel from regular stereo records.

by DAVID LACHENBRUCH CONTRIBUTING EDITOR

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new & timely

Active Citizens Bander is named "Handicapped American of Year"

H. Keith Russell, Silver Spring, MD, a member of the Montgomery County REACT No. 2348, has been named Handicapped American of the Year by the President's Committee on Employment of the Handicapped, and was awarded the President's Trophy, the nation's highest honor to its handicapped citizens. (REACT—Radio Emergency Associated Radio Teams—is an organization of Citizens Band groups who keep a 24-hour watch on CB channel 9, give help to motorists in difficulties and assist in emergencies and catastrophes.)

Mr. Russell, who moves about with crutches and long leg braces, works continuously for handicapped people especially in the area of removal of architectural barriers— in addition to his REACT volunteer work. In Montgomery County he was instrumental in helping the passage of special parking privileges for the handicapped, ramping of shopping centers, curb-ramping ordi-



H. Keith Russell

nances, and the removal of discriminatory employment practices.

He is also active in local and national organizations concerned with the removal of such architectural barriers as stairs, narrow doorways, etc., which prevent 10% of the population from moving about freely.

Mr. Russell is chief of the Armed Forces Institute of Pathology Histopath Laboratory of Walter Reed Hospital and has an additional part-time occupation as a musician. He also builds musical instruments and installs automobile hand-controls for a large manufacturer. In addition, he often travels to speak to medical groups about the correct use of medical aids for severely handicapped patients.

Duval Payne and David Robinson win latest Gernsback Award

Duval W. Payne, a home-study student

of the National Technical Schools, Los Angeles, is the most recent winner of the 1974 Hugo Gernsback Scholarship Award, a check for \$125 given annually to a student in each of eight leading



Duval W. Payne

electronics home-study schools. The Award is in memory of the late Hugo Gernsback, who devoted much of his energy to encouraging young men in the study of electronics.



David B. Robinson

A second prize—an RCA WV-529-A "Service Special" VOM—contributed by RCA for the runner-up in each of the 1974 Award contests, goes to NTS student David B. Robinson.

Mr. Payne, who lives in Pittsburgh, writes: "I am employed at present as foreman of Building Equipment Maintenance for the U.S. Postal Service, which has become so highly automated that they have need for technicians.... The things I have learned are a tremendous asset on my present job, and I also intend doing part-time TV repair."

Mr. Robinson is an auto mechanic,

shop foreman for Daniels Chevrolet in Colorado Springs, CO. He says: "The knowledge gained (in my current Electronics course with NTS) has been of extreme importance in the presently expanding use of electronics in cars. In coming years, I think courses like this should be included in expanded Auto Mechanics courses."

Radio waves may affect human health

Radio waves may affect the nervous system and behavior, and normal development and growth processes "at lower levels than anticipated in the past," the government Office of Telecommunications Policy stated in a report to Congress. The Office warns, however, that the tentative findings are based on a small number of experiments on a limited number of subjects, and that "casual relationships between the electromagnetic fields and observations are not yet clearly established."

High concentrations of radio frequency radiation is known to cause adverse biological effects by generating heat in the tissues. The thermal effects are fairly well understood, and it has been fairly well established that power densities of less than 10 mW per cm² are harmless to human beings, as far as their heating effects are concerned.

Less is known of other effects of rf radiation, though they have been suspected to exist for some time, especially with microwaves. In the 1940's, while he was manufacturing microwave diathermy equipment, Lee de Forest suggested a study of "the non-thermal effects of higher radio frequencies." Some effects of radio waves are rather sharply tuned: ants align their antennas parallel to an electromagnetic field at 9 MHz; emissions at 29-MHz have been used to kill bugs in bread, and radiations at 388-MHz have killed monkeys. On the other hand radiation at 21-MHz increases the germination of gladiolus bulbs. These are obviously non-thermal phenomena; effects due to heat would cover wide frequency bands.

Emergency audio transmitter is help for seizure victims

A device for persons who may be liable to heart attacks, epileptic seizure or diabetic coma is now being marketed by a Denver firm.

Called the Emergency Medical Instructor, it is a small case that contains a taped message pre-recorded by the patient's own physician, telling what is (continued on page 12)

Avoid serious trouble in color TV sets by using the <u>right</u> replacement capacitor!

SPRAGUE

TYPE PP

polypropylene film

This capacitor is GREAT for 90% of your film capacitor replacements. But . . . it's <u>NOT</u> designed for certain critical applications.

polyester

film

The next time you replace a dipped tubular in one of the newer color TV sets, don't automatically assume you're replacing an ordinary every-day film or paper capacitor. If it happens to be a deflection capacitor used for commutating or S-shaping, you need a polypropylene or polycarbonate film replacement with (1) high a-c current-carrying capability; (2) close capacitance tolerance; (3) good capacitance stability. The standard replacement capacitors used in the industry, even our superior Type PS dipped tubulars, just won't do the job ... and they could cause serious trouble after the set is put back into operation.

These capacitors

are a MUST for critical

commutating and S-shaping

applications.

SPRAGU

TYPE PM

olycarbonate f

Play it safe . . . dipped tubulars may lock alike on the surface, but there can be a big difference in the film dielectric. Keep a supply of Sprague Type PP and PM capacitors on hand for those critical situations where ordinary replacements wan't work.

SPRAGUE TYPE PP POLYPROPYLENE FILM CAPACITORS

μF @ WVDC	Cap. Tol.	D. x L.	Cat. No.	μF @ WVDC	Cap. Tol.	D. x L.	Cat. No.
1.75 @ 100 1.5 @ 150 .01 @ 400 .015 @ 400 .033 @ 400 .06 @ 400 .081 @ 400 .2 @ 400	±5% ±5% ±5% ±5% ±5% ±5% ±2% ±2%	.900 x 1.000 .800 x .937 .400 x .750 .450 x .750 .500 x .750 .800 x 1.250 .600 x 1.300 .700 x 1.700	PM1-M1.75 PM15-M1.5 PP4-S10 PP4-S15 PP4-S33S PP4-S60S PP4-S81S PP4-S81S PP4-P20	.0039 @ 600 .01 @ 600 .066 @ 600 .075 @ 600 .022 @ 800 .047 @ 800 .051 @ 800 .0018 @ 1600 .002 @ 1600	±5% ±5% ±5% ±5% ±5% ±5% ±5% ±5%	.400 x .800 .500 x 1.250 .800 x 1.250 .750 x 1.250 .600 x 1.300 .700 x 1.250 .800 x 1.250 .500 x 1.300 .500 x 1.300	PI'6-D39S PI'6-S10S PI'6-S66S PI'S-S75S PI'8-S22S PI'8-S47S PI'8-S51S PI'16-D18
.0018 @ 600 .0022 @ 600	±5% ±5%	.400 x .750 .400 x .750	PP6-D18S PP6-D22S	.002 @ 1800 .0033 @ 1600 .0039 @ 1600	$\pm 5\%$ $\pm 5\%$ $\pm 5\%$.550 x 1.300 .600 x 1.300	PP16-D20 PP16-D33 PP16-D39

For cross-reference information on close-tolerance polypropylene and polycarbonate film capacitors, showing original part numbers with correct Sprague replacements, ask your Sprague distributor for Cross-Reference Guide C-873, or write to: Sprague Products Company, 81 Marshall Street, North Adams, Mass. 01247.

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*Summary of survey results upon request.

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new & timely (continued from page 6)

happening, the identity of the victim, and giving necessary instructions for emergency action. If the wearer falls to the ground, the device starts and continues to repeat the 4-minute message loud enough to attract attention, for up to two hours.

The manufacturer, National Identification Co., believes the equipment will save lives, since in the past some such cases have been mistaken for ordinary drunkenness and correct treatment delayed until too late.

Microneurosurgery is aided by compact color TV

Microneurosurgery—operation under a microscope—has been hampered by the fact that no more than two persons can watch the operation. Using extremely small surgical instruments, one surgeon operates looking through a binocular microscope while the other viewer uses the second lens of the binocular. This not only limits the possibility of training other surgeons, but places the surgeon in an isolated position, as the operating room staff are unable to observe the operation and therefore cannot intelligently anticipate the surgeon's needs.

With the help of a new compact color TV camera, devised by Motorola, New York's Mount Sinai hospital has overcome these difficulties. Since the size of the new camera permits connecting it directly to the microscope, the operation can be telecast to TV sets in the operating room exactly as the surgeon sees it. The operation can also be recorded on videotape as an aid in training future surgeons for the same operation.

Auto license plate to go electronic?

An electronic license plate proposed by Dr. Fred Sterzer, director of the RCA Microwave Technology Center in Princeton, NJ, may make that now littleregarded part of the car an important factor in highway safety, vehicle scheduling and control, theft protection, and traffic control.

The device is described as "a printedcircuit antenna covered by a visual display of the license number, a frequency doubler, a modulator and an rf detector." It would receive signals on an assigned frequency and retransmit them on double that frequency. An integrated circuit encoder would enable the license plate to transmit a signal that would identify the vehice carrying it. Costing only a few dollars to make in quantity, the electronic license plate could:

1. Respond with a vehicle's identifying code when interrogated electronically. (Electronic interrogators (transponders) placed along streets and highways, and connected into a dataprocessing network could schedule or dispatch ambulances, police cars, trucks or busses more efficiently. Trucking firms could reduce the risk of highjacking by monitoring the progress of trucks carrying valuable cargo. Interrogators could search for cars reported stolen, or report those whose owners were ignoring summonses for traffic violations.)

2. Receive and transmit messages to and from a vehicle. (The driver of a disabled car could transmit a coded call for assistance to fixed roadside receivers or to highway patrol cars, and could receive safety messages—or special calls from police vehicles, addressed directly to him.)

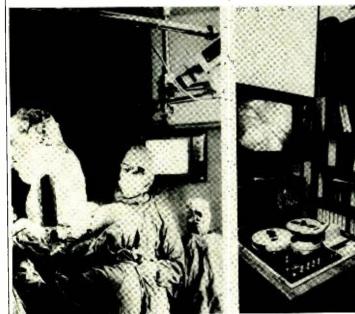


3. Serve as a transponder for a collision-avoidance radar. (The electronic license plate meets all the requirements for a second-harmonic reflector, as used in the second-harmonic highway collision avoidance radar demonstrated by RCA in 1972. Such radars avoid the clutter and confusion faced by ordinary radars, since they see only the signal transmitted—at twice the frequency from the electronic license plate instead of the reflection of the direct transmitted signal, which can be bounced off roadside objects, cars approaching in the opposite lane, etc.)

While the adoption of such a radar system would—like the present adoption of safety seat belts—require legislation or mass manufacturer cooperation, Dr. Sterzer believes that such action would be well-advised. "One person is injured every six seconds and one is killed every ten minutes in the United States," he says. "Increased control over motor vehicles would be a cheap price to pay for reducing this slaughter."

Television inventor Zworykin is unhappy with today's TV

Vladimir K. Zworykin, celebrating his 85th birthday, stated that to him the best control on the TV set is now the "off" switch. In language reminiscent of de Forest's "What have you done to my child?" speech, he said: "When TV (continued on page 14)



COMPACT COLOR TV CAMERA, SHOWN IN PLASTIC AT EXTREME LEFT, televises in color what the operating neurosurgeon sees through his microscope lens.

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--Ed Canby, AUDIO

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For independent lab test reports on the IC150. write CROWN, Box 1000, Elkhart, Indiana, 46514.



Circle 6 on reader service card

broadcasting began to develop, I hoped that it would be used for educational purposes, especially so that different cultures could learn to understand each other. Instead, most of the time when I turn on the TV-bang, bang, bang!"

The Russian-born inventor, working for Westinghouse in 1923, demonstrated a crude television camera and receiver. When the head of his department saw it, Zworykin revealed, he said: "Put that guy to work on something more useful!" Later, Zworykin took his neglected device to RCA, where Sarnoff saw its possibilities and supported it to the ultimate commercial success.

CETA of Poughkeepsie area elects its 1974-75 officers

Ron Palluth, CET, of Poughkeepsie, NY, was re-elected president of the Consumer Electronics Technicians Association (CETA), at a meeting held at the Kitchen Restaurant, Hyde Park, NY, last June. Vice president is Ken Parese, CET, of Wappingers Falls, also re-elected. Treasurer is Tom McNamara, Salt Point; recording secretary Dan Ellsworth, CET, Kingston, and correspond-

ing secretary, Dick Jones, also of Kingston.

Lessons from satellite teach teachers to teach

The first instructional television program to be broadcast by a satellite has been originated by the University of Kentucky at Lexington. One program is designed to show teachers how to teach children about adult careers, another includes lessons on conducting remedial instruction. The first programs were carried by land line from Lexington, KY, to Rosman, NC, and transmitted from there to Applied Technology Satellite 6, for re-transmission to waiting teachers from Huntsville, AL, to Fredonia, NY.

A New York Times reporter, covering 15 schools in the Applachian area, reports that signals from AT-6 came through strong and clear.

Other educational and medical programs were planned for later in the year, and it is anticipated that next year the satellite may be shifted farther east to transmit educational programs for 5000 villages in India. R-E

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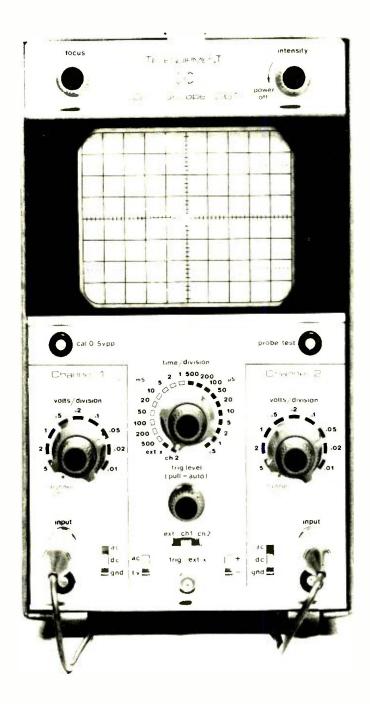
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MORE NEW TECHNOLOGY-PLEASE!

I would like to say that your magazine excells above the other publications when it comes to quality construction projects such as the character generator of the September 1973 issue. I'm sure you have received many letters appreciating this. I did send for the booklet also which I feel was well worth the cost. I have not as yet built the project, but plan to in the near future. I would like to see more projects of this caliber. I would especially be interested myself in monitor-receiver projects.

I like the idea of your magazine presenting new technology to its readers. Computers are now a part of our lives and with the number of calculators now on the market, we service technicians need all the updating we can get. No schooling is available of decent quality to aid technicians to service such equipment, so most people are forced to pay large service fees for manufacturer-oriented service personnel.

The quality of technicians in general is below what it should be overall. The

CET licensing program will help tremendously. Shop owners should encourage the study and acquisition of CET certificates to their technicians. Right now, many shop owners either don't seem to know or don't care if a technician even possesses such a certificate.

Thank you again for the opportunity to "sound off."

GERALD F. CLEMENT JR. Canoga Park, Calif.

City of New York Dept. of Consumer Affairs 80 Lafayette Street New York, NY 10013 Elinor Guggenheimer. Commissioner

Dear Mrs. Guggenheimer:

Re: Chapter 32 title b Art. 44 Admin code.

Thank you for sending us a copy of the New York City Rules and Regulations relating to TV, Radio & Audio Equipment repairs. The following are the observations I have:

1. Estimates have always been and

are now a most difficult problem for technicians. Often, diagnosing a problem from the symptoms displayed can lead even the best practicing technicians to believe a certain part is at fault when, in the end, it turns out something completely different is causing it. By requiring an estimate as outlined in the law, the technician and dealer are asked to be very accurate or face a loss or try to amend the estimate later.

I realize this is a most difficult area you have to deal with in the regulations, but it is one where after some experience, your department may want to modify the rules. This may benefit the dealers by relaxing the procedures while benefitting the set owner by allowing the dealer-tech to give more accurate estimates without over-protecting himself.

NESDA (National Electronic Service Dealers Association) is very interested in your experience in this regard and would be most happy to have your opinions on it, later, for our use in helping other areas solve problems in their legislation.

(continued on page 22)



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LETTERS

(continued from page 16)

2. Reg. No. 11 would be interpreted by a majority of judges as meaning any (TV-Set, Stereo, Radio, etc. as a unit) must be warranted or guaranteed, both parts and labor. I don't think that is your intent, but it must be spelled out that only those parts replaced and only the actual repair work charged for are guaranteed. As is, the dealer is expected to be a philanthropist, possibly repairing an inexpensive item (for example) and yet being asked to warrant the \$250.00 picture tube!

3. In Indiana and in all other of the nine states with electronic service legislation, there is an industry advisory board. Without these experts to advise you, some common servicing practices may seem wrong when they are right. To discredit a dealer unfairly or your department would lessen the effectiveness of the regulations. Consider appointment of such a board (preferably a five-man board).

4. The \$100.00 fee for a dealer license is quite high when compared with that in other states. I realize that for effective administration of the law that you will need investigators, a staff, etc. and other items. However, other governments with fewer shops have been able to have a greatly reduced cost for the license to the shop.

Since this cost, as well as the other costs in time and materials which this regulation will impose on the dealers, must be passed on to the set owners, reduction of the fee would be in the best interest of the public.

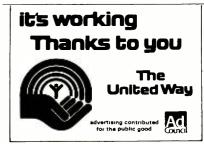
5. Equal justice under this act is so vital. Much of the problems of the electronics service business over the years has been caused by people performing service with an unfair advantage. Examples of this are those servicers who operate on a haphazard basis out of their homes, who hide their income thus not paying any taxes on it; who do not protect their customers by having insurance; etc.

If all servicers in New York have to play the game by the same rules equally, this law can be complied with, with the above modifications. However, if enforcement is not certain and swift, the law could merely increase the cost of service and lower its quality.

If I can be of further service to you or the dealers and techs in New York. feel free to call on me. DICK GLASS

Executive Vice President NESDA Indianapolis, IN

R-F



Circle 10 on reader service card

RADIO-ELECTRONICS



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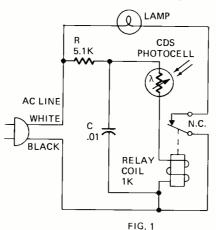
appliance clinic

AUTOMATIC LIGHT SWITCHES

by JACK DARR SERVICE EDITOR

AUTOMATIC LIGHT SWITCHES HAVE BEcome quite popular, not only in rural areas but in suburban areas as well. These switches use a very simple electronic circuit; a small relay which is controlled by a photocell. When the outside light is high enough, the relay is energized and the light goes off. Figure 1 is the schematic of a typical unit. This is one of the smaller types, for controlling lamps up to 300 watts. There are several different sizes, including types which can control highintensity mercury lamps.

The ac current flows through a 5100-ohm resistor (refer to Fig. 1), through a cadmium-sulphide photo-



cell (abbreviated CdS), then through the coil of the relay. The CdS cell here is used as a variable resistor. The arrows are the symbol for a lightactuated device.

When the cell is dark, it has a high resistance. More light falling on it decreases the resistance and more current flows. The relay contacts do the actual switching. They are normally closed ("NC") when the relay is *not* energized, and the light goes on. This gives us "fail-safe" operation. If anything goes wrong in the control circuitry, the light remains lit.

The control unit is usually mounted on top of the lamp reflector, under a small metal cover. This will have a little window in it; the photocell is mounted behind this. For best results, this window should be on the north side of the cover when installed. This keeps the direct rays of the sun from falling on it, and gives better control of the light.

To repair one of these, start with the lamp. If the lamp won't light, replace the bulb with a good one. Now, cover the window on the housing with your hand. You should hear the relay click. If this happens, but the light still refuses to go on, turn the power off and remove the cover. There are several hot wires exposed, so don't take any chances.

Check the relay contacts; they may be burned or pitted so badly that they do not make contact, even though the armature of the relay may pull in. In most of these units, the contacts are easily accessible. Pull a strip of fine sandpaper between them, holding the armature down with your finger (power OFF, remember!) Close the relay gently by hand and look at the contacts; you will be able to tell whether they're touching or not. Turn the power on, keeping clear, and recheck the unit to see if it's operating. You can cover the photocell with a piece of dark paper or cloth.

One common cause of damage to these units is a nearby lightning discharge. If this has happened, you will probably see burned parts, charred insulation or carbon "tracks" across insulators. If this is the case, take the unit off and repair it.

Disconnect both wires and remove the control unit and lamp socket. You'll need an ohmmeter to check it. Disconnect the capacitor across the relay coil and check it for shorts. If it has shorted, the 5100-ohm resistor will probably be well charred, too. Replace these, if they're bad. Before connecting them back, check the relay coil. If it too, has been damaged by the lightning, its coil will look very dark, or even charred. Normal resistance of a typical unit is about 1000 ohms.

If the capacitor took a direct hit, its case may have exploded, so that you can't read the markings. Fortunately, they aren't too critical; a .01- μ F capacitor at 600 volts is a good size.

While the circuit is opened up, check the photocell. With the surface

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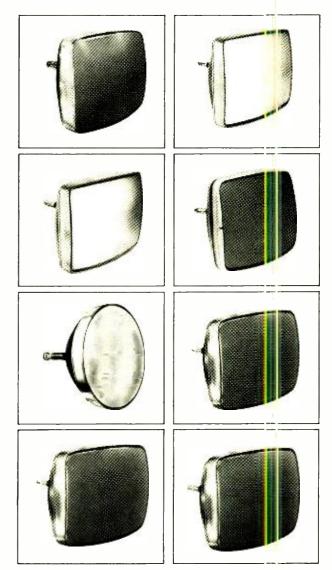
That's the kind of socket coverage you can count on from this popular new "middle line" of RCA replacement color picture tubes. With just eight Colorama A types, you can cover almost all of the replacement market with "Grade A" performance at a price your customers can afford.

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equipment report

Technics Model RS-676US Dolby Cassette Recorder



Circle 110 on reader service card WITH EACH NEW DEVELOPMENT IN high fidelity, manufacturers often just dip their toes in the water while checking on what everyone else is doing. Few take the full plunge at once.

But in the Technics (by Panasonic) RS-676US cassette recorder, we find virtually all the latest advancements made in hi-fi in the last few months.

Starting off, the RS-676US is basically a Dolby cassette deck with the addition of special switching and calibration that permits the Dolby processor to be used for monitoring (or recording) Dolby FM broadcasts. Next, we find the tape transport is unlike most other cassette mechanisms you've run across. This mechanism has two motors: one for the capstan drive and one for a "superspeed" rewind and fast forward. Looking even closer we find the mechanism is all solenoid operated-the control buttons operate only solenoids, which in turn provide the mechanical operations. All-solenoid control means remote control is possible, and the rear panel of this recorder has a remotecontrol socket for an optional control unit, or one you can easily build yourself.

Finally, we come to the *peak/aver-age* VU meters used for setting the recording level. When the cassette system first made the hi-fi scene, it was nothing more than an improved version of the basic Philips casette system, which was intended for recording speech. The reference recording level was pegged at tape saturation for the *average* program level, and signal peaks were driven well into tape saturation distortion — there was no "headroom". To maintain an acceptable signal-to-noise ratio, the reference recording level for hi-fi was maintained at tape saturation; a colossal blunder, because the tape got better but the signal level was still driving program peaks into tape saturation.

With the newer tapes plus Dolby B noise reduction, the signal-to-noise ratio is sufficient to permit reducing the average program level to provide "headroom", and that's just what Panasonic has done in their latest recorder. The 0-VU record level is 6-dB below tape saturation. When the VU meters are switched to NORMAL the meters indicate as do any other level meter, the difference being that 0-VU is 6-dB below 2% total harmonic distortion (from the tape).

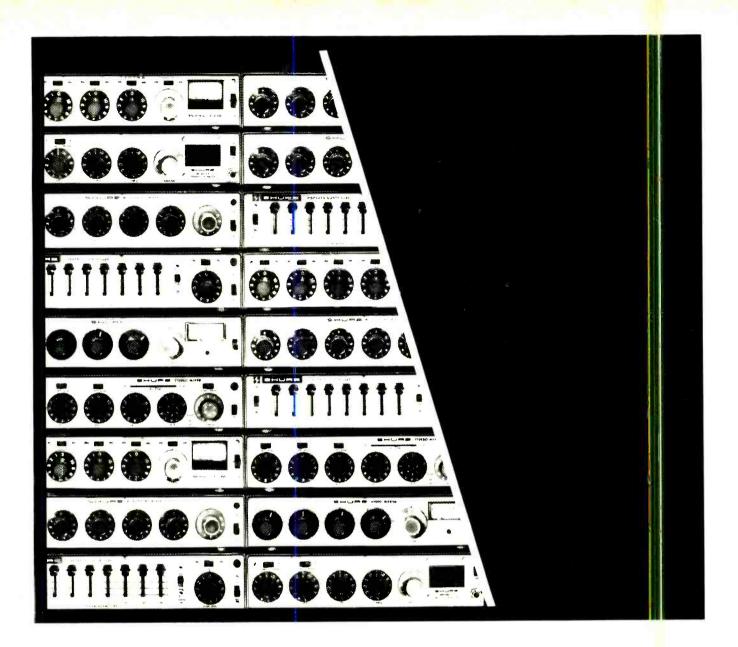
So in one package we find the latest developments in hi-fi: Dolby FM, automatic chromdioxide equalization switching. cassette tape "headroom", solenoid operation and superfast tape wind.

There are controls for record input selection, line/tuner record level, record balance, and concentric left and right microphone record level. There are switches for Dolby B in/out/filter, Dolby FM in/out, tape type and peak/normal VU meters. Left and right screwdriver-adjust controls on the front panel permit calibration of the Dolby FM circuit to 50% modulation the Dolby reference level for FM broadcasts. (FM stations transmit the calibration tone once or twice a day; and once the controls are adjusted their setting is permanent as long as the same FM tuner is used.)

The FCC has recently allowed Dolby FM stations to use a $25-\mu$ S preemphasis instead of the standard 75 μ S. The recorder has a $75/25 \mu$ S COMPENSATION switch on the rear to permit optimizing recording and reception of either pre-emphasis. When the recorder is set to Dolby FM, the output to the amplifier's tape monitor is "flat"—the Doly processor can be used for straight listening as well as recording.

The tape mechanism has pushbut-(continued on page 110)

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It's a mod. mod. modular world.



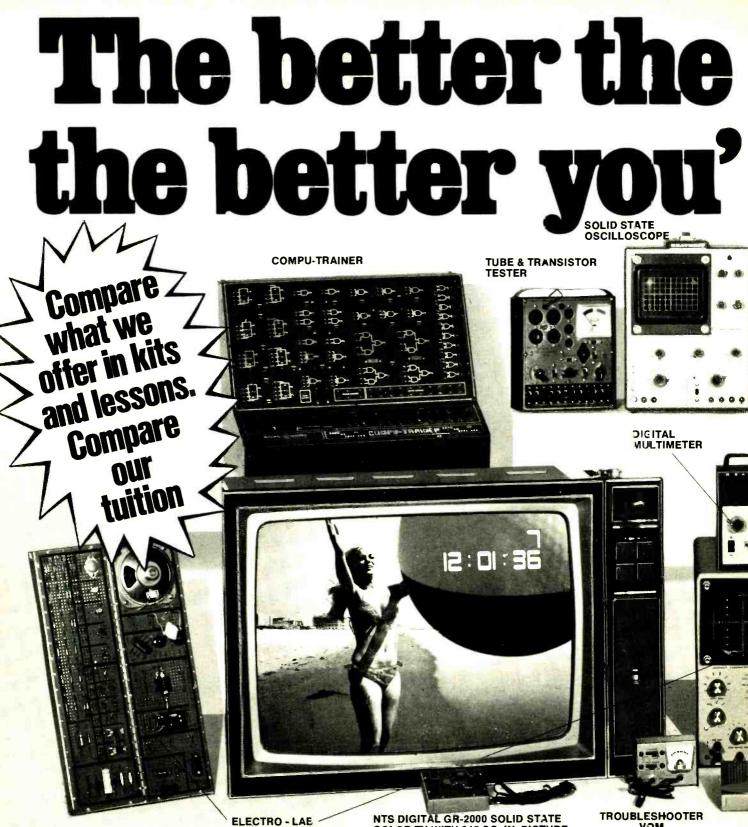
Simplify, simplify! Instead of paying more for bigger, bulkier audio control components, pay less for compact Shure modular components that — singly or in combination—handle critical functions flawlessly. Cases in point: (1) the M67 and M68 Microphone Mixers, the original high-performance, low-cost mixers; (2) the M610 Feedback Controller, the compact component that permits dramatically increased gain before feedback; (3) the M61 Audio Master, that gives almost unlimited response shaping characteristics; (4) the M688 Stereo Mixer, for stereo recording and multi-source audio-visual work; (5) the M675 Broadcast Production Master, that works with our M67 to create a complete production console (with cuing!) for a fraction of the cost of conventional consoles; and (6) the SE30 Gated Compressor. Mixer, (not shown above) with the memory circuit that eliminates "pumping." For more on how to "go modular," write for the Shure Total Communications Components Catalog No. AL280.

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while the guy down the street complains about how tough alignments are...I do them!



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Now, in the time it used to take me just to set up, I can almost complete an alignment. And I'm confident the set will perform as well as it possibly can. My customers notice, too. That's the difference B&K's 415 Solid-State Sweep/Marker Generator made

Setup is no problem. After I connect the 415's outputs to my scope (there's even low-frequency compensation to eliminate pattern errors), I connect its RF outputs (channel 4 or 10) to the antenna terminals or mixer test point, the direct probe to the video detector test point (or anywhere else after the video detector diode) and the demodulator probe to the bandpass amplifier output.

They're all clip-on connections, and the 415 comes with all the accessories I need. Once I've made the initial signal and bias hookups, there's nothing else to connect or reconnect. All intercabling changes and generator functions are controlled from the front panel. There's even a 15,750Hz filter to eliminate disabling

the set's horizontal output section.

Shaping the waveform is easy, because the 415 has 10 crystal-controlled IF markers, each of which lights up on the front-panel waveform diagram as it is used. Markers can be shown either vertically or horizontally on the scope trace. There's a 100kHz modulated marker that makes nulling the traps so easy it's almost automatic. And three low-impedance, reversiblepolarity bias supplies-two, 0-25VDC; one, 0-50VDC.



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BULD 200 Watt-Second Photoficsh

Build any of the three bare-bulb photoflash units described in this article. An optional optical trigger is also described.

by JIM GUPTON

BARE-BULB ELECTRONIC PHOTOFLASH units are becoming increasingly popular with amateur and professional photographers. Soft shadows and wide angle coverage increase the versatility of any camera and make those "Impossible" group shots...possible. Add a Lawson Enterprises "Reflectasol" to a bare-bulb photoflash and you have a professional studio light source for color portraits. By obtaining power from the standard 117-volt ac line, you eliminate the weight and expense of batteries and have the fastest recycling time of any electronic photoflash on the market.

This article contains the construction details for three bare-bulb photoflash units. The first unit uses computer-grade capacitors and has an output of 200 watt-seconds. The second unit has an output of 100 wattseconds and uses standard photoflash capacitors. A selectable output unit having 50, 100, 150, and 200 wattsecond outputs is also described.

All three photoflash units can also be used as slave units with an optical trigger circuit that is described. As a slave unit, the photoflash is triggered with the light from a photoflash mounted on your camera. This eliminates the need for sync cords and permits the placement of the slave unit anywhere in the picture taking area. Optically triggered slave units are commonly used among professional photographers.

Of all electronic construction projects, none can be more deadly than the electronic photoflash unit. Voltages ranging between 400 and 500 Vdc, at a current of 1 ampere, can kill you! Therefore, every step of the construction, including the final assembly and testing, must be and is, engineered to protect you against accidental shock hazards and possible fatal injury. It is imperative that no deviation from the specified material be attempted. When constructing one of the three alternate photoflash circuits, observe capacitor polarity at all times.

Plastic canister housing

The electronic circuits for the barebulb electronic photoflash must be housed in a shock-proof container. Metal cases offer considerable physical protection, yet the metal exterior is likely to become charged and it will create a shock hazard when contact is made with a common ground circuit. The ideal case to house the bare-bulb photoflash can be found in the household section of most any department store or discount house. The article's housing was originally one of a set of four kitchen canisters. It has rigid side walls and ample inside dimensions to house the electronic circuits securely with complete protection from accidental shock hazards.

To eliminate the molded handle grips and bottom depressions of the canister's top and bottom, simply cut away the surface containing the raised handle and bottom depressions, and replace it with a matching contour section of fiber glass printec-circuit board. The fiber glass board provides a metal shielding surface and is rigid and thin enough to support the flash tube circuits. They are easily attached to the plastic top and bottom with epoxy cement and small aluminum angle sections to assure firm attachment and rigidity. In my model, a metal ring surrounds the flash tube to provide mechanical protection to the tube and to serve as support for a large reflector. Remember that the wall thickness is an important item in selecting your plastic canister. The plastic walls must have enough trength to support the photoflash when mounted on a tripod. Flexible plastics should not be substituted as they cannot meet the support requirements.

Power-capacitor bank circuits

The schematic circuit diagram in Fig. 1 illustrates two types of capacitor banks. One type of capacitor bank is series connected, provides a 200 watt-second output, and is shown in Fig. 1-a. Figure 1-b shows the alternate, parallel circuit which provides a 100 watt-second output,

The series circuit takes advantage of high-capacitance computer-grade capacitors for high output power at a

minimum of space requirements. However, there are some who may be apprehensive about the ability of computer-grade capacitors to hold up under rapid discharge cycling and of the higher leakage rate common with this type of capacitor. The alternate, par-

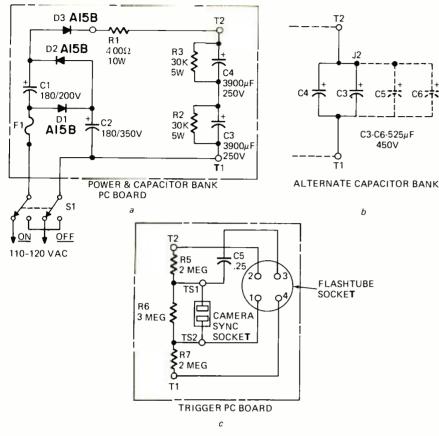
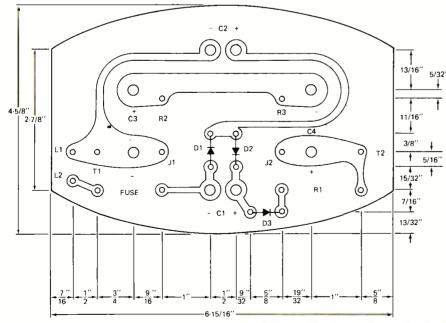
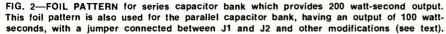


Fig. 1—BARE-BULB PHOTOFLASH CIRCUIT. Circuit a shows the series capacitor bank which provides a 200 watt-second output. Circuit b shows the alternate capacitor bank which provides a 100 watt-second output. With the optional addition of capacitors C5 and C6, circuit b provides 200 watt-seconds. An optional switch wired between the positive terminals of the capacitors in circuit b will also provide multiple power output ratings. Circuit c is the trigger circuit.





allel circuit employs the standard photoflash capacitors for maximum power output and requires a larger canister housing.

Computer grade capacitor circuit

The circuit board illustrated in Fig. 2 can be used for computer-grade ca-

SLAVE TRIGGER PARTS LIST

- SC1-National Semiconductors Ltd. NSL-701-3, 3-element, series-connected silicon cell
- C1-0.01 µF ceramic disc capacitor 50 Vdc
- R1-39K; 1/4 -watt resistor
- SCR-General Electric C106B3 SCR Ac plua

TRIGGER CIRCUIT PARTS LIST

- R5, R7-2-megohm 1-watt resistor
- R6-3-megohm 1-watt resistor
- C5---.25µF Mylar capacitor 400 Vdc
- Flash tube socket, standard 4 pin radio socket
- Flash camera sync socket, standard ac socket
- Flashtube DX-5-Kemlite Laboratories, 1819 W. Grand Ave., Chicago, III. 60622

200 WATT-SECOND SERIES CAPACITOR POWER PARTS LIST

- S1-Dpdt switch-rocker or toggle type, Allied Electronics No. 700-5110 or equal
- F1-11/4 amp. Slow-Blow
- D1, D2, D3-General Electric A15B or equal 1A 200V silicon rectifier
- R1--400-ohm. 10-watt resistor
- R2, R3-30K, 5-watt resistor
- C1-180 µF/200 Vdc Mallory
- No. CG181T200A1
- C2-180 µF/350 Vdc Mallory
- No. CG181T350B1
- C3, C4-3900 µF/250 Vdc Mallory No. CGS393T250FH1
- Ac line cord and plastic strain relief.

PARALLEL CAPACITOR-**POWER PARTS LIST**

- -Dpdt switch, rocker or toggle type, Allied Electronics No. 700-5110
- F1-1¼ amp. Slow-Blow
- D1, D2, D3-Silicon rectifier GE type A15B or equal
- R1-400 ohm, 10 watt resistor
- C1-180 µF/200 Vdc Mallory
- No. GC181T200A1
- C2—180 µF/350 Vdc Mallory
- No. GC181T350B1
- C3, C4, C5, C6-525 µF/450 Vdc Mallory type FF45052 or equal

pacitors in series or standard photoflash capacitors in parallel with minor changes. The series circuit employs Mallory 3900-µF. computer-grade capacitors. This amount of capacitance will produce a 200 watt-second output to the flash tube. Resistors R2 and R3 serve to equalize the voltage across the capacitor discharge bank, C3 and C4. To produce the charging dc voltage

for C3 and C4, capacitors C1 and C2, in conjunction with the silicon diodes D1, D2, and D3, form a voltagetripler circuit to transform 117 volts ac into 450 volts dc. Fuse F1 is rated at 1 ampere and must he of the Slow-Blow type due to the greater current drain during the initial forming of computer-grade capacitors. Likewise, the current limiting resistor R1 is rated at 10 watts and must be mounted no less than ½ inch above the circuit board to properly radiate the heat generated in the initial forming operation.

A jumper is indicated at J1 and J2 of Fig. 2. The jumper is only used when modifying the circuit board for standard photoflash capacitors and is not required for series capacitors. The dimensions indicated on Fig. 2 are to locate drill centers for components and capacitors. All electrolytic capacitor terminal holes are 1/4 inch in diameter. When mounting the capacitors, be sure that the number 10 washer is between the copper circuit and the capacitor terminal with the mounting screw inserted through the 1/4-inch hole from the component side of the circuit board. Be sure the correct polarity is observed in mounting the capacitors.

Parallel standard photoflash capacitors

Only minor modifications are needed to convert the circuit board in Fig. 2 to the parallel-connected standard photoflash capacitor bank. The 1050 μ F capacitance (525 μ F + 525 μ F) will produce an output of 100 watt-seconds or, if you prefer, you can use the larger circuit board in Fig. 3 with four standard photoflash capacitors. This will produce a 200 watt-second output similar to the computer-grade series capacitor circuit. In parallel use, the circuit board in Fig. 2 does not require R2 and R3. The 10-watt resistor R1 must now be connected between the cathode of D3 and the heavy foil strip running across the top of the board. (Use the holes provided for R3 in the series-capacitor circuit.) Capacitor C4 must be reversed in polarity so that the positive terminals of C3 and C4 are attached to the plus bus circuit. Now connect a number 18 wire between jumper terminals J1 and J2. Trigger terminal T2 cannot be used as shown. Move it to the positive terminal bus at point R2. No change is made to the voltage-tripler circuit or its associated capacitors or diodes.

The four-capacitor parallel circuit (Fig. 1-b, using the circuit board in Fig. 3) can be modified to provide selectable light output. For a choice of either 100- or 200-watt-second output, connect a single-pole, heavy-duty

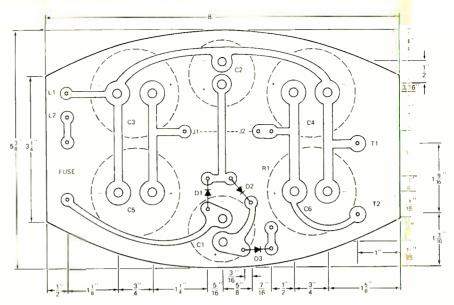
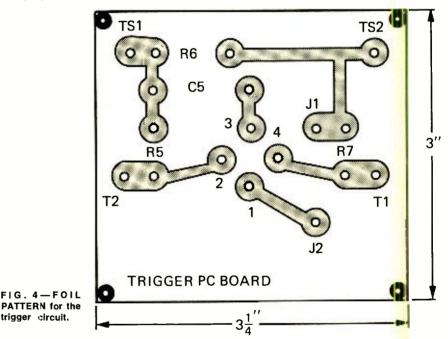


FIG. 3--FOIL PATTERN for parallel capacitor bank which provides 200 watt-seccnc output (connect jumper between J1 and J2). With modifications, the foil pattern is also used for the multiple power output flash (see text).



toggle or rocker switch instead of the jumper between points J1 and J2 in Fig. 3. For a choice of 50, 100, 150 or 200 watt-seconds, modify the circuit board by removing the copper foil paths between the positive terminals of C3 and C5 and C4 and C6. Install a heavy-duty single-pole, 4-position *progressive-shorting* switch on the housing top. Connect the four terminals to the positive terminals on C3— C6 and the arm to point T2.

WARNING: ONLY POWER-CAPA-CITOR BANK (Fig. 1-b) CAN BE MODIFIED WITH OPTIONAL POWER SELECTION SWITCH. UNDER NO CIRCUMSTANCES SHOULD A POWER SELECTION SWITCH BE ATTEMPTED ON FIG. 1-a SERIES-CONNECTED COMPUTER-GRADE CAPACI- TOR CIRCUIT. PLACING ONLY ONE CAPACITOR ACROSS 450 VOLTS DC WILL PRODUCE A DANGEROUS OVERLOAD OUT-PUT AND CREATE A POTEN-TIAL EXPLOSIVE CONDITION IN THE CAPACITOR.

Trigger circuit board

The trigger circuit shown in Fig. 1-c is simple with only 4 components. The PC board for the trigger circuit is shown in Fig. 4. Since the flashtube socket is on the component side of the circuit board, some minor difficulty may be encountered in connecting the flash tube socket to the circuit connections 1, 2, 3, and 4. All that is necessary to make the proper connections is to attach number 16 solid wires to the 4 tube socket pins and insert the other end of the wires in the corresponding

print board contact holes and solder. Firm mechanical connections must be made to the tube socket pins to prevent solder heat from breaking a solder-only connection.

To mount the trigger board to the housing's top, attach 4 stand-off terminals to top and solder stand-off pins through 4 corner holes of the trigger circuit board. TS1 and TS2 connect to the camera sync socket which consists of a standard ac connector, with either number 16 or 18 flexible, stranded wire. The camera sync socket is mounted on the housing's top and can be either a push-in, snap-lock, or screw-mounted socket. This location for the sync socket minimizes the number of connections between trigger circuit board and the power-capacitor bank and places the sync socket in the most advantageous position for use with an optical slave trigger.

Power input connections

Ordinarily, one would expect the power switch discussions to be along with the 117-volt ac tripler circuit. However, because there is a potential shock hazard associated with the ac power switch, it is described separately. Only a double-pole doublethrow switch should be used in the ac power line. The ac line must be connected to either the two top or two bottom terminals of the switch with the power-capacitor bank connected to the center terminals of the switch and a jumper connected to the unused terminals. This connection, shown in Figs. 1-a and 5, prevents voltage feedback through the switch to the ac plug terminals and eliminates a potential shock hazard. It also provides a capacitor discharge shunt when the switch is in the OFF position, to remove dangerous stored capacitor voltages.

Optical slave trigger

The most valuable accessory to electronic photoflash photography is the optical slave trigger for your photoflash (Fig. 6). It triggers the photoflash with the light from your camera mounted photoflash and eliminates the use of two sync cables. Figure 7 illustrates how the four components are assembled on the prongs of an ordinary ac plug and encapsulated in a clear plastic or epoxy resin. The General Electric C106B3 SCR is specified not only for the electrical specifications but for the anode terminal position opposite the gate and cathode terminals. This is most convenient for mounting the SCR on the prongs of the sync plug.

The light-sensitive device is a National Semiconductors Ltd. type NSL-701-3 silicon photodiode. It consists of

three 0.1 x 0.2 in, silicon chips connected in series to provide sufficient voltage output to trigger the SCR when struck by the light from the master flashgun. The NSL-701-3 can be purchased for \$6.00 from National Semiconductors Ltd., 331 Cornelia Street, Plattsburgh, NY 12901.

(The NSL-701-3 is sold as an assembly of bare silicon chips. These are very fragile and easily damaged. If you wish, you can purchase a com-

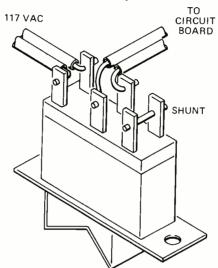


FIG. 5-AC POWER SWITCH wiring.

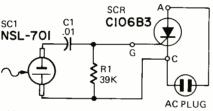


FIG. 6-OPTICAL SLAVE TRIGGER CIR-CUIT.

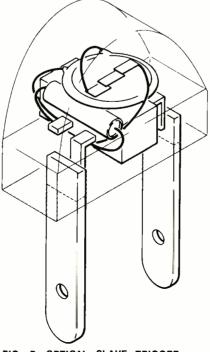
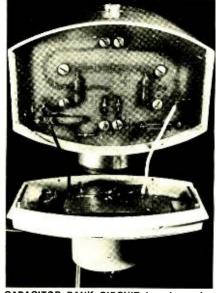


FIG. 7-OPTICAL SLAVE TRIGGER component placement diagram.

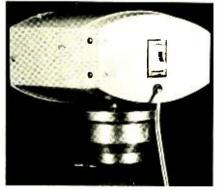


CAPACITOR BANK CIRCUIT board can be seen from component side of board.

plete optical trigger-ready to plug into the flashgun from most photo equipment supply houses for approximately \$15.00. The device is the Wein Micro Slave.-Editor)

Final assembly

Upon completion of the powercapacitor bank and trigger circuit



REAR VIEW OF PHOTOFLASH unit mounted on tripod shows power cord and ac switch.

boards, the final mounting of components in the plastic housing is begun. Figure 8 shows the side view of the component mounting inside the canistor housing. The ac power switch is mounted on the bottom plate of the housing with the 117 volt ac line connected to the end terminals on the switch and a shorting jumper connected across the opposite end terminals (see Fig. 5). Connect a 10-inch section of ac cord from the two center terminals of the switch and run it towards the top of the housing. Next, insert the power-capacitor bank circuit board to locate the tripod mounting position. The correct position for the tripod mount is slightly below the bottom of capacitor C1, with enough space below C1 for adequate backplate support. The tripod socket can

36

If you select the variable-output circuit for your flashgun, you'll find a progressive-shorting switch almost impossible to obtain because it appears that they're now being made only on special order.

Do not be misled by the terms "shorting" and "non-shorting" in switch catalogs. A shorting-type switch has its arm or wiper arranged so it establishes a new contact before breaking the old. In a nonshorting switch, the wiper breaks contact with one terminal before it makes contact with the adjacent one.

A progressive-shorting switch has a long wiper that progressively connects or shorts the fixed terminals until all are tied together. Your best chance at a suitable switch of this type is to salvage one from a surplus radio transmitter or antenna tuning unit. Diagram *a* shows how to connect it. (I have a hunch that the burners on electric ranges have a similar switch so you might look into this.)

If you can't find a progressiveshorting switch, you can make an equivalent from by wiring a 4-pole, 4-position rotary switch as in diagram *b*. It should have ceramic wafers and contacts rated at at least 5 amps at 350 volts dc.

The DX-5 flash tube is rated at 150 watt-seconds maximum, However, the author assures us that he has not noticed any shortening of the tube life due to its operation at 200 watt-seconds. Furthermore, this tube is used in several commercial 200 watt-second flash guns.

-Editor

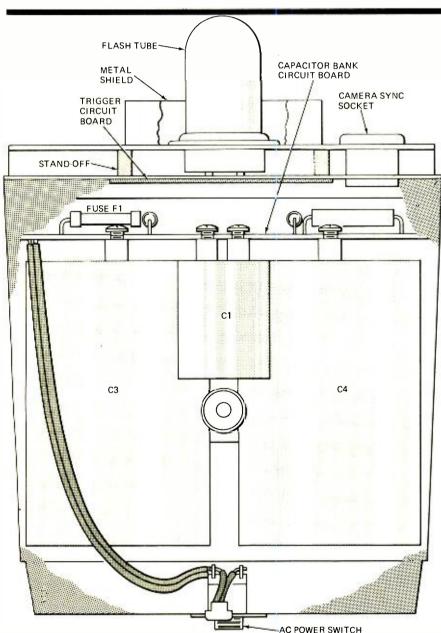
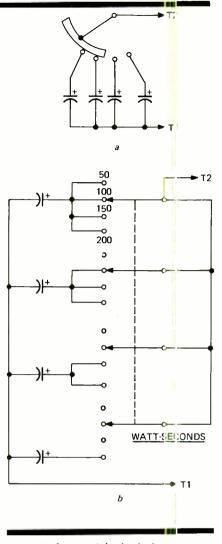


FIG. 8—COMPONENT PLACEMENT DIAGRAM for the barebulb photoflash unit.



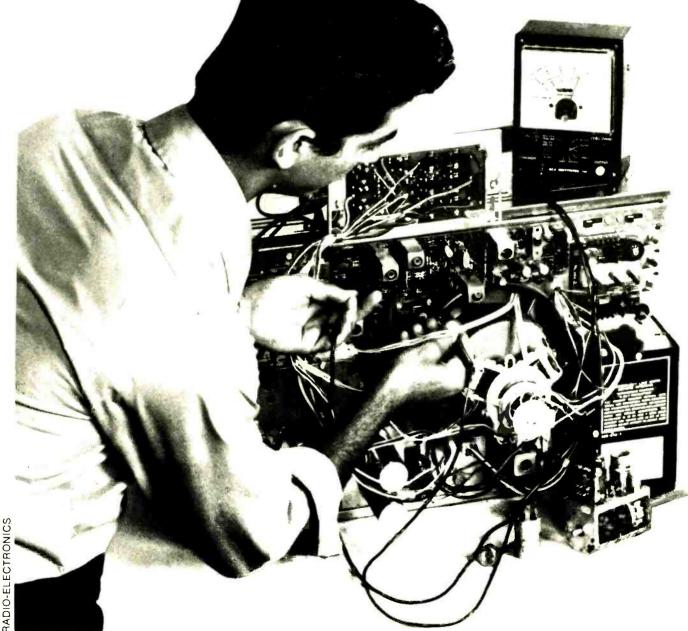
be made from a 1-inch circle or square plate of aluminum or brass, 14 inch thick and with a 1/4-20 threaded hole in the center point of the plate. Or, if you prefer, a tripod socket may be purchased from your local camera store or a quick-release triped base is available from Edmund Scientific Co., 101 East Gloucester Pike, Barrington. N.J. under catalog number 42941. With the tripod socket installed, wrap the capacitor bank, below the print board, with plastic film or acetate sheet and tape securely. This wrapping offers additional electrical shielding and will contain capacitor electrolyte should a capacitor rupture for any reason.

Insert the power-capacitor circuit into housing and firmly seat the pc board to housing sides. A small piece of tape is sufficient to secure the entire assembly if the pc board has been accurately contoured to the housing's interior dimensions. Attach the trigger circuit connections and insert the top of the housing onto the housing body. However, do not secure the top to the body at this point. Insert the 'lash tube in the flash tube socket.

(continued on page 80)

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THE LOW COST MINI-COMPUTER IS A reality today. Together with time-sharing systems, they are performing an increasing number of tasks in all types of applications.

However, the relatively high cost of terminals has slowed both the acceptance and the use of the computer in small businesses, homes, and schools. The MITS Comter 256 (CT256) computer terminal described here can be built for less than $\frac{1}{2}$ the cost of most terminals and offers many unusual features not found in terminals costing several times as much.

The terminals important features include:

A built in acoustic coupler making computer connection simpler and saving added cost.

An auto-transmit that allows transmitting data or program material to the computer from memory, line by line.

Complete cursor control by software as well as by manual control via the keyboard.

A tape recorder input/output jack to enable taping of frequency shift keyed (FSK) tones during telephone connection to a computer. This gives virtually unlimited memory capability. Almost any type of tape recorder may be used.

A 32-character Burroughs display with a soft orange, highly legible readout.

Standard ASCII encoded keyboard with TTY-33 format.

Internal memory capability of 256 characters per page and up to 4 pages of memory.

Automatic page change at the end

EXCLUSIVE!

First Computer

of each page for a total of 1024 character storage for a 4-page unit.

Flexible power requirements. Operable from line voltage of 100 to 130 volts or 200 to 260 volts.

A 25 pin input/output accessory jack for hardwire computer connection and add-on accessories.

Data flow in the terminal

The block diagram of the Comter 256 (Fig. 1) represents considerable digital circuitry (91 logic IC's in a 4page unit). The data path starts at the keyboard. When a character key is depressed, the character is encoded into a 7-bit binary code and is sent in parallel form on 7 lines to the UART (Universal Asyncronous Receiver-Transmitter-a 40-pin MOS chip) which converts the character data to serial information. The serial data is sent to the FSK modulator which converts a binary 1 to 1270 Hz and a binary 0 to 1070 Hz.

These tones are transmitted from the acoustic coupler to the computer, via the telephone lines. The computer processes the data and returns it back over the telephone wires to the terminal at a different frequency (binary 1 = 2225 Hz, binary 0 = 2025 Hz).

The data is fed to the acoustic coupler

You Build This is a special report

terminal in kit form. It a computer directly or via

where the tones are amplified, filtered and demodulated back into serial binary coding.

From the demodulator, the serial data goes to the UART and is converted to parallel form where it waits to be loaded into memory. When a data available signal from the UART coincides with the 32nd character display time for the self-scan (right hand end of display), the first 6 bits of the character are entered into memory (the seventh bit is not used in the CT 256 memory) and the data position is automatically moved one position to the left.

The self-scan display is connected to the memory so that as a character is entered into memory it is simultaneously displayed along with the other characters in memory. This process is repeated for every character

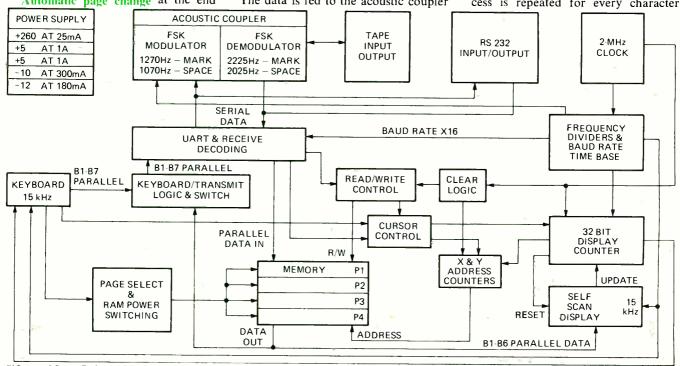


FIG. 1—COMTER 256 COMPUTER TERMINAL block diagram showing data flow. Data flow starts at the keyboard, which is shown at the left side of the diagram.

RADIO-ELECTRONICS

Terminal From A Kit

on a 4-page computer can be connected to telephone lines.

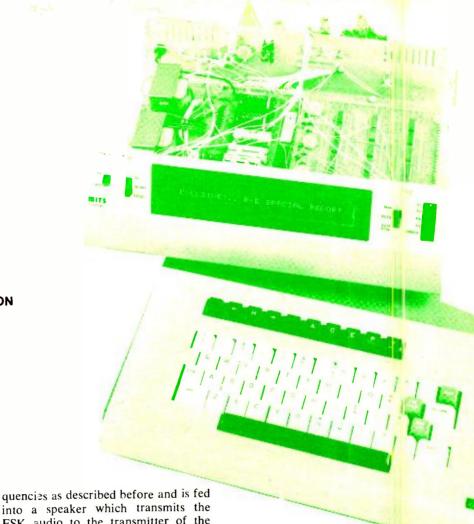
by THOMAS W. DURSTON

transmitted from the keyboard, plus the computer can also transmit its own characters to the terminal as the software requires.

How it works

The most important single circuit in the CT256 is the clock oscillator. It is a 2-MHz crystal oscillator that provides the time base for the logic, and is also used in the modulator of the acoustic coupler to provide the FSK tones. A crystal oscillator was chosen for its stability. The 2-MHz clock is divided down to provide 1 MHz, 62.5 kHz, and 15.625 kHz for logic time base. It is also used to determine baud rate (data transmission rate) for the UART. The baud-rate switch selects either 1760 Hz (110 baud X10) or 4800 Hz (300 baud X16) for the UART clock by setting a programmable counter to divide the 2-MHz clock by 1136 or 416 respectively. The modulator in the acoustic coupler works in a similar manner. Instead of setting a switch to set a programmable counter to divide by different rates, it uses the binary logic 1 or 0 of the data to derive the two divide rates.

Starting with the data path, the keyboard encodes the character by feeding a 15-kHz signal to a 4-bit binary counter that is connected to a 4-to-16 line decoder. The character keys are connected to the 16 lines according to the first 4 bits determined by the ASCII code. When a key switch is closed, and the line it's connected to is strobed, the 4-bit counter is halted. The 4-bit count where the counter stopped is the first 4 bits of the 7-bit ASCII code and the other 3 bits are encoded by a series of logic gates. After a 30-ms debounce period, a load signal is sent to the UART, where the parallel 7-bit character code is entered into registers and transmitted out serially at the selected baud rate. The serial data is sent to the modulator where it is converted into audio fre-



into a speaker which transmits the FSK audio to the transmitter of the telephone handset.

When the computer returns the data or originates its own, it is received as a 2225-Hz or 2025-Hz tone. The signal is picked up by a ceramic microphone adjacent to the receiver in the telephone handset, and is amplified and converted to a low-impedance output by a JFET-NPN transistor circuit. This low-impedance circuit feeds the tape cutput and a two-stage op-amp active filter.

The two-stage filter removes noise and irterference and provides a gain of about 400. The filter output feeds a carrier detector circuit that turns on the carrier LED, enables the transmit circuit, and enables the FSK demodulator which consists of an XR210 IC phase locked loop. The output of the op-amp filter also feeds the XR210 and the signal is demodulated into serial binary form. This serial binary data is fed into the UART and is sampled at the set baud rate. If the serial data is valid, it is converted into a 7-bit parallel format corresponding to the ASCII code for the character received.

The UART also indicates that it has new data available. Meanwhile, the receive decoding determines if the new 7-bit character is a display character or a control character. If it is a display character, it is allowed to be entered into memory, if it is a control character (bell signal, cursor control char; see table of control characters; the receive decoder inhibits memory loading and initiates the necessary operation.

Memory operation

Probably the most involved circuitry in the CT256 centers around the 5-bit (32 count) display counter and 4-bit (16 count) X-Y memory address counters. The X-Y memory address counters are both 4-bit (16 coi nt) updown, presettable counters, making a total combination of 256 addresses (16X by 16Y). For reference sake, the Y addresses are called lines and X addresses are called character positions (see Fig. 2 & 3). The start of the page is called "home" (see Fig. 4) and has address \emptyset , \emptyset (line \emptyset , position ()). When the black "H" key (home) is depressed, it homes the data to the cursor position (right hand en.) of display-32nd character) and risults in the X-Y address counters being at \emptyset , \emptyset during the 32nd character display time.

The cursor position is very important because it is during this 32ndcharacter display time that; n ≥w data is entered into memory, data is shifted right or left in the display, data is homed, memory is cleared, and many other timing chains are based.

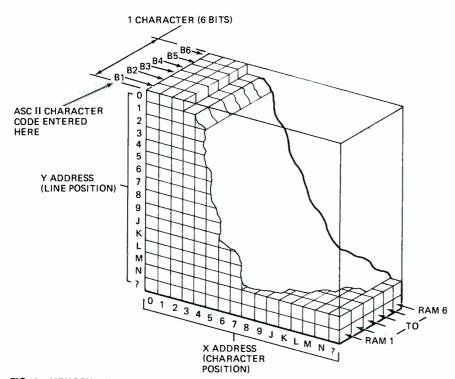


FIG. 2—MEMORY FORMAT. The 6-bit character is entered into memory in ASC11 code. The memory location is selected in accordance with the respective position on the page (line and character position.)

At the time when the UART indicates new data available and the 32ndcharacter display time starts, the read/ write logic generates a write pulse for the memory. The first 6 bits of data at the output of the UART are then written into 6 RAMs (Random Access Memory) at that address. The write pulse also goes to the cursor control logic, where, upon completion of the write pulse, the X-address is incremented one position, shifting the data one position to the left on the display. The write pulse also triggers a circuit that resets the data available line from the UART.

The clear circuit, activated by either pressing the black "C" key or receiving a control "L", enters the ASCII code for a blank into all 256 positions of memory for that page. It works by holding the write circuit on and forcing the data input lines to the memory to coding for a blank. This only takes place during the 32ndcharacter display time during which it "homes" the X & Y counters and advances the X-counter 256 positions (one complete page) at a 1-MHz rate.

The auto transmit circuit works by depressing the black "T" key which activates logic that switches the transmit data lines from the keyboard to the data output lines from the memory. Whatever character is in the cursor position of the display is transmitted out to the computer. As that character is received back, it is re-written into the same position in memory, the data is shifted left one position and the next character in memory is transmitted. bits of ASCII code to locate a particular address in memory and display it in the cursor position. The first character received after the address function is initiated, selects the line number (1-16) by setting the Y address counter equal to the first 4 bits of that charac-

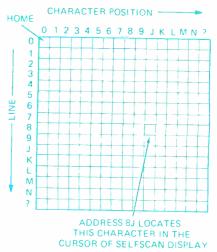


FIG. 3—MEMORY FORMAT shows the page position and character location respectively. Address 0, 0 is the "home" position on the page.

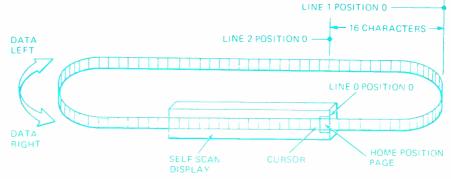


FIG. 4—PAGE FORMAT shows how the page is displayed on the Self Scan display. Each line of the page is 16 characters long and the page is displayed one line at a time.

Since the memory only stores the first 6 bits of the 7-bit ASCII code, the 7th bit must be derived by logic gating.

This is one reason why the CT256 cannot auto-transmit control characters.

The 7th bit cannot be derived for control characters, and since the memory does not receive and store them anyway, they have to be transmitted manually via the keyboard. To allow entry of control characters such as carriage return, the detection of the @ symbol will cause auto-transmit to stop and the desired character may be manually transmitted. The @ symbol is detected in the cursor position and auto transmit cannot take place unless it is shifted out by manually entering a new character.

The address function is initiated by pressing the black "A" key or by receiving a control "O". It sets up the receiving decoding to accept the next two characters and use their first fourter's ASCII code. The second character received selects the position in the line (1-16) by setting the X address counter equal to the first 4 bits of that character's ASCII code. These two characters are used only for address location and are not loaded into memory. For Y (line) and X (position) identification see Fig. 3.

Page circuitry

The page control circuit for a multi page unit consists of two circuits for each page. The first set of circuits enables each set of 6 RAM's, making them active for the page selected; the second set of circuits reduces power to the unused pages to standby levels, reducing current drain by 75%.

The operation of the page control circuit is determined by the setting of the PAGE switch. In MANUAL, the page can only be changed by depressing the black "P" key. Pressing the black "P" (continued on page 91)



The digital multimeter has finally moved out of the laboratory and onto the service bench. Here's a rundown on those that sell for \$300 or less.

by ROBERT F. SCOTT TECHNICAL EDITOR

FOR YEARS THE MULTIMETER HAS BEEN the principal—and sometimes the only —test instrument used by the service technician for voltage, current and resistance measurements. Many oldtimers have an almost continuous squint acquired from peering at a meter and trying to read the voltage indicated by a pointer that has banged against its pins once-too-many times.

Digital meters—presenting the metered quantities in large easy-to-read numbers—have been used in laboratories, industrial plants, etc. for years but have just recently been developed to the point that they are priced within the reach of electronic service technicians and many experimenters.

The digital multimeter, often called a dmm or dvm, offers many advantages to the busy service technician. For example, in some dmm's, range selection, polarity indication and decimal point placement are performed automatically. The indications are often large erough to be easily read from up to 20 feet away. Parallex does not exist so it cannot affect reading accuracy. The accuracy of the instrument is much greater than a typical analog vom or vtvm.

There are quite a few new dmm's in the \$300 and under class that will appeal to the service technician and advanced experimenter. We are going to discuss the features and operating principles of the dmm and present the pertinent specifications of the instruments you should consider before making your selection.

How the dmm works

The analog instrument takes the meterec quantity-voltage, current or

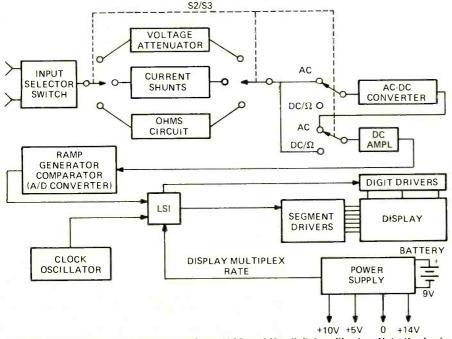


FIG. 1—BLOCK DIAGRAM OF BALLANTINE MODEL 3/24 digital multimeter. Note the basic similarities between this and an analog multimeter.

resistance—and converts it into a voltage that is read on the meter in the proper values and terms. A precision voltage divider attenuates the test voltage so it is within the basic voltage range of the meter movement. The dmm is similar except that the movingcoil meter is replaced by an analogto-digital converter whose cutput drives a digital display or readout.

Compare the block diagram of the Ballantine model 3/24 dmm (Fig. 1) with that of your Simpson 260, Triplett 630 or similar instrument and you'll see the resemblance. The dmm is basically a dc instrument with a scaled-down portion of the input voltage applied to the display through the analog-digital (A-D) converter. Resistance is measured by passing a constant current through the unknown resistor and measuring the voltage drop across it. Current is mete ed by measuring the voltage drop across a current shunt. When measuring ac voltage or current, a rectifier is inserted between the input attenuator and the A-D converter.

The A-D converter is the in erface between the analog dc input and the digital display device. There are a number of different ways of converting an analog dc voltage to a digital value. Among these are: voltage-controlled oscillator, single-ramp and double-ramp integration, charge balancing and successive approximation. All have advantages and disadvantages that affect accuracy, resolution, and the rate at which the display can follow or track a changing input signal. The study of A-D converters as applied to dmm's is quite interesting; but is beyond the scope of this article. If enough of you are interested, we'll cover A-D converters in a future issue.

Displays

The three types of displays in com-

mon use are LED's in both 5×7 dot matrix arrays and seven-segment arrangements; liquid crystals in both transmissive and reflective types and gas-discharge tubes such as the Nixie. Each type has its advantages and disadvantages.

Gas-discharge tubes generally offer brighter and larger digits that can be read from greater distances. However, they require a relatively high excitation voltage and their current drain is high enough to restrict their use to line-operated bench-type instruments. LED's are the most common type of display. They are easy to read in either format; are high-efficiency devices that operate from approximately 1.5 volt and draw about 25 mA per segment. When the display is strobed, the average power is low and long life can be expected from high-quality dry cells.

There are reports that some bench technicians complain of eye strain and fatigue after long hours of reading LED and gas-discharge displays. Too, both types tend to wash-out when viewed in bright sunlight.

Liquid crystals are the new-comer to the display field and seem to be the ideal in terms of power consumption. A liquid-crystal display draws only microwatts while an equivalent LED display will draw many milliwatts. This type of display is made in both transmissive and reflective types. The former must be backlighted which compromises the power

TWENTY TWO RANGES, four each for dc and ac volts and current and six for resistance are included on the *Data Precision model* 134. Its 3½-digit, 7segment gas-discharge display incorporates 200% over-range and has a reading rate of approximately 1 per second. Voltages up to 1.5 kV rms; current



to 2 amps and resistance to 20 megs can be read. At 100% overrange, the reading is 1999. Readings above 1999 are indicated by the lighted "1" and selected decimal point. The other three digits are blanked.

The least significant digits are 1, 10, and 100 mV and 1V on the voltage ranges; 1, 10, 100 μ A and 1 mA on current; and 0.1, 1, 10, 100, 1K and 10K in the resistance mode.

Optional isolation probe has switchable 100K isolating resistor. High-voltage probe extends range to 30 kV. $3\frac{1}{2}$ \times 7¹/₈ \times 8⁷/₈ in. 4¹/₄ lbs. \$189. saving gained through its use. The reflective-type display can be used in areas where high ambient light and widest angular visibility are not needed.

Battery operation

Most dmm's are line-operated with built-in batteries. Some have throwaway dry cells and others have rechargeable batteries, either installed or in optional battery packs. If you want a battery-only instrument, be sure that the batteries will last long enough for a couple of days use.

LINE-OPERATED VERSION of the model 21 is Data Technology's model 20. Ranges, functions and specifications are the same as in the hand-held model 21.



Options include single and side-by-side rack mounts, carrying case, high-voltage probe; 100-, 115- and 230-volts ac line operation and IC sockets for quick component replacement, 2.5 x 6.25 x 9 in., 2.3 lbs. \$269.

FOUR RANGES and cold-cathode readouts and indicators are used in the *Heathkit IM-1202* portable digital multimeter. This 2½-digit instrument is well within the reach of hams and beginning electronics experimenters while meeting the specifications required for many operations on the radio/TV service bench.

Its ranges are: 2, 20, 200 and 1000 Vdc; 2, 20, 200 and 700 Vrms (25 Hz to 10 kHz); 2, 20, 200 and 2000 mA dc and ac; 200, 2000, 200,000 ohms and 2 megs. Overrange is 25% on all ranges—within maximum limits. Resolution on the low-



est ranges is 10 mV, 10 μ A and 1 ohm. Accuracy (full scale ± 1 digit): dc volts $\pm 1\%$; dc and ac current and ac volts $\pm 1.5\%$; ohms $\pm 2\%$.

Input impedance is 1 megohm on all voltage ranges. Power requirements 110–130 or 220–260 Vac, 50/60 Hz. 734 $\times 5\%_{6} \times 3\%$ in., 2½ lbs. \$79.95.

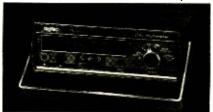
WORLD'S SMALLEST is the claim made for the *Non-Linear Systems model LM-4*, a full 4-digit instrument with full-scale count of 10,000 on 0.31-in. red LED display elements. It measures ac and dc volts from 100 μ V to 500 V and resistances from 0.1 ohm to 10 megohms and operates from the 117-volt line.



The case is $1\frac{34}{100}$ inches high, $2\frac{1}{2}$ inches wide and $3\frac{1}{4}$ inches deep. Its carrying handle also serves as an adjustable tilt stand. \$187.

PLUG-IN BOARDS, IC'S AND readouts for easy replacement are features of the *DigiTec model 2110* and *2120*. Internal rechargeable batteries facilitate operation independent of power lines. A built-in automatic charger keeps the batteries charged as long as the dmm is connected to the power line.

Dc voltage ranges extend from 199.9 mV to 1000 volts full scale with basic accuracy of 0.1% of the reading. Ac voltage can be measured from 1.999 to 500 volts (750 volts on the 2120) with



accuracy of 0.5% of the reading. Basic accuracy of 0.5% of the reading is available on five resistance ranges extending from 199.9 ohms to 19.99 megs. A zero control permits nulling test-lead resistance.

Functions are selected by pushbuttons while ranges are changed with a rotary switch that includes a BATT CHK position. Input impedance is 10 megs on dcV; 1 meg shunted by 10 pF on acV. The 3½-digit display uses 0.3-in. high LED numeric indicators. Overrange blanks all numerals except the overrange "1", polarity sign and decimal point.

Gulton R-200 batteries operate the model 2110 a minimum of 8 hours and the 2120 5 hours in continuous operation. Recharging takes 16 hours after full discharge.

The 2120 (not shown) has all the features of the 2110 plus five ac and dc current ranges extending in decades from 1.999 μ A to 1.999 A.

Power requirements 115/230 V, 50– 400 Hz; 2.5 W for the 2110 and 5 W for the 2120. Size 2.43 \times 7.25 \times 7.95 in., 2 lbs. less batteries. *Model* 2110 \$219, 2120 \$275. **AUTOMATICALLY POSITIONED** decimal point, 100% overrange capability and fool-proof out-of-range indications are features of the *B* & *K* Precision model 281. On this 2¼-digit instrument, out-of-range is indicated when the first digit remains on while the second and third digits are off.

Ac and dc voltages are measured on 100 mV, 1.00, 10.0, 100V and 1.00 kV ranges. Accuracy is $\pm 1\%$ of reading



 \pm 1 digit on dc and \pm 1.5% of reading \pm 1 digit on acV. Current measurements (ac and dc) are in 100 μ A, 1.00, 10.0 and 100 mA and 1.00 amp ranges with accuracy of \pm 1.5% of reading \pm 1 digit. Frequency response is 20 Hz to 1 kHz.

Seven decade resistance ranges (10 ohms to 10.0 megohms) provide accurary 2% of range to 1 megohm and 3% of range on 10 megohms. The instrument provides 100% overrange on all functions.

The 281 operates from 117 Vac, 15 W. 31/2 $\,\times$ 7 $\,\times$ 9 in. 5 lbs. \$170.00.

CAPACITANCE READING CAPABILITY

in a hand-held dmm is a unique feature of the *Data Technology model 21*. It is a 3½-digit instrument powered by four internal rechargeable batteries that provide up to several weeks of intermittent usage. It comes with a plug-in battery charger that can be specified for 100-, 115- or 230-volt operation. Battery charge life is extended by the use of PUSH-TO-READ switches.



Voltage ranges are 2, 20, 200, and 1000 volts dc and peak ac with 1-mV resolution. Resistance ranges are 2K, 20K, 200K and 2 megohms. Capacitance is read in four ranges from 2 to 2000 nF (.002 to 2.0 μ F) with resolutions of 1, 10, 100 and 1000 pF.

Accuracy on resistance and capacitance is $\pm 0.15\%$ of reading +0.05% of full scale; $\pm 0.1\%$ of reading +0.05%of full scale on dcV and 0.5% or reading +0.1% of full scale (50 to 500 Hz).

The model 21 slips into a pocket or into a handy carrying case that clips onto a belt. It is $6.8 \times 3.25 \times 1.75$ in. and weighs only 12 oz. \$269.

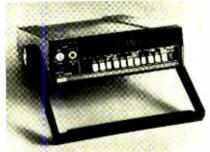
Reading specifications

The $\frac{1}{2}$ digit: Dmm's are generally specified by the number of digits (numeral indicators) in the display. Each digit is capable of displaying any numeral from 0 to 9. A 3-digit instrument will have a maximum reading of 999 and a minimum of .001. If it has 1, 10, 100 and 1000 volt ranges, it reads maximums of .999, 9.99, 99.9 and 999 volts, respectively.

Each digit added to a display increases zircuit complexity and cost proportionately. Manufacturers found that they could improve the *resolution* (the smallest change in the quantity being

NOISE COMPONENTS on the signal being metered are removed $\pm y$ a two-pole filter before being processed by the A/D converter in the *Fluke model 8000A*. It is a compact $3\frac{1}{2}$ -digit instrument featuring pushbutton range and function selection, automatic polarity switching, a self-locating decimal point and selfzeroing to eliminate offset uncertainties. The basic dmm is designed around ± 0.2 and ± 2.0 Vdc and has twenty six ranges and six functions.

The 8000A measures ac and dc volt-



ages from 100 µV to 1199 V; current from 100 mA to 1.99 A; and resistance from 100 milliohms to 19.99 megs. Dc voltage and current are measured with accuracy of $\pm 0.1\%$ of reading +1 digit and $\pm 0.3\%$ of reading +1 digit, respectively. On ac (45 Hz to 10 kHz) voltage accuracy is $\pm 0.5\%$ of reading + 2 digits. Current measurements are $\pm 1\%$ of reading +2 digits (except on 2000 mA where frequency is limited to 3 kHz). In the range of 10 kHz to 20 kHz, voltage accuracy is $\pm 1\%$ of reading +2 digits. Resistance accuracy is \pm 0.2% of reading +1 digit on all ranges except $\pm 0.5\%$ of reading +1 digit on 20-mec range.

Input impedance is 10 megs on dcV and 10 megs shunted by 100 pF on acV. Optional probes extend measurement capabilities to 30 kV dc, 200 amps dc and to 500 MHz on acV.

The Fluke dmm is available in somewhat more expensive options. The 8000A-01 includes an optional rechargeable battery pack providing over 8 hours of portable operation. The 8000A-02 has a digital printer output; the -05 features a 10-amp current range and the -06 has low ohms (2 and 20 ohms) ranges.

The 8000A operates from 100–115 and 230 Vac, 50–400 Hz, 2 W. 2.52 \times 8.55 \times 9.9 in., 2.75 lbs. \$299.

measured that will produce a change in the display reading) of their instruments at little increase in circuit complexity or cost by adding a lef -hand digit that displays only the numeral "1." This "1" is called the hill-digit. Thus, a 3½-digit instrument can display 1999.

Overrange is an extension of the half-digit technology and is a means of extending the readings beyond what would be full-scale on an analog instrument. Most multimeter have ranges of 1, 10, 100 and 1000 or similar decades. Now, suppose that we want to measure the precise voltage of a standard 1.5-volt dry cell. Using an analog instrument, we would have to use the 10-volt range and would not be able to read the voltage with any degree of accuracy. With a cmm, we would use the 1-volt range. The applied voltage would be greater than the range selected. The instrument would sense an over-range; the halfdigit "1" would light and the voltage

TRUE PORTABILITY AND LAB precision are claimed for the 4½-cligit Data Precision model 245. It is about the size of an Instamatic camera and even includes a wrist strap. Voltage, current and resistance are read on 21 ranges with 100% overrange. It comes with carrying case, wrist strap, test leads and a battery module that includes rechargeable batteries, battery charger and line cord.

When operated on the ac line, the batteries remain on charge whether the dmm is turned on or off. When disconnected from the power line for portable or field use, the batteries last at least 6 hours before recharging is required. Recharging takes about 12 hcurs.

Ranges: Dc volts 1.000 to 1000 with 100% overrange. Input impedance 10 megs on three highest ranges; over 1000 megs on 1.000-volt range. On ac, the ranges are the same as on dc



except on the 1-kV step where overrange voltage is limited to 500 volts. Ac input impedance is 1 megohm shunted by 50 pF or less. Maximum rms input is 500 V, 30 Hz to 10 kHz, above 10 kHz it decreases linearly to 2:00 V at 50 kHz. Settling time (to settle within \pm 0.1% of final reading with full-scale input) is 2.5 sec.

Current (ac and dc) 1 mA tc 1 A in four decade ranges with 100% overrange. Resistance: 1K to 10 megs in five decade steps. Least significant digit on lowest range is 1 milliohm. Maximum open-circuit voltage is 3.5 V.

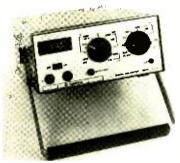
Operates from 105-125-volts 47-63 Hz. $5\frac{1}{2} \times 1\frac{3}{4} \times 3\frac{1}{2}$ in. 1.3 lbs. \$295.



could be read with three-place accuracy —1.470 for example—an impossibility with an analog vom.

Accuracy of an analog vom is usually specified as a percentage of the full-scale reading—generally 2 to 3%. Parallax, pivot wear, needle unbalance and other deficiencies of the movingcoil meter can further degrade accuracy. On the other hand, the accuracy of a dmm is specified as \pm a percentage of the *reading* plus 1 digit. A reading of 1.000 volt would have a possible error of $(1.000 \times .001) + 1$

FULL 3-DIGIT LED DISPLAY is used on the *Ballantine 3/24* dmm. Two rotary panel switches provide 25 operating ranges including one for battery check. A flashing left-hand digit and an indication of less than 200 indicate a reliable reading between 1000 and 1200. Automatic polarity indication when measuring dc voltages and current. Ranges are: 1000 mV, 10, 100 and 1000 Vdc; 100 and 1000 μ A, 10, 100 and 1000 mA dc and ac; 1000 mV, 10, 100 and 500 Vac; 100, 1000, 10,000, 100,000 ohms and 1 and 10 megohms.



Accuracy is $\pm 0.2\%$ of reading +1 digit on 1000 mV dc, $\pm 0.5\%$ of reading +1 digit on 10, 100, 1000 Vdc and the five current ranges; $\pm 1\%$ of reading +2 digits on acV; $\pm 1.5\%$ of reading +2 digits on ac current and $\pm 1\%$ of reading +1 digit on all resistance ranges.

The optional 10850A peak detector can be used to measure sinewaves to beyond 500 MHz. Maximum input signal is 30 Vac. The optional 10800 HV probe measures dc up to 30 kV.

The 3/24 operates from any one of four dc power sources; NEDA type 1603 dry cell battery, any external 6.2-10volt source delivering 50 mA, a voltagedropping network or the Ballantine 32401 dc adapter permitting operation from 9.8 to 34 volts dc at 10 to 100 mA, depending on the input voltage and setting of the display brightness control. Ac operation is from the optional 32402A plug-mounted supply requiring 100 to 135 Vac at 3 watts. The unit stores in the dmm's battery compartment. A 32403A rechargeable NiCad battery supply powers the dmm for 16 hours and incorporates a charger that restores full charge in 16 hours. Fits in battery compartment and operates from 100-125 and 200-250 Vac, 48-420 Hz.

The 3/24 is 5.5 x 2.4 x 7.1 in., and weighs 2 lbs. with battery. \$195.

or \pm .002 volt.

Auto-ranging is a feature of some dmm's. The operator selects the desired function (volts, current, resistance, etc.) and connects the test leads to the point or component being mea-

ANALOG OUTPUT AND DISPLAY are features of the *Simpson 360* that are unique in dmm's in its class. The analog output terminals of the 360 provide 1 Vdc (open-circuit) corresponding to a digital reading of 1000. This analog signal voltage can be used to drive a graphic recorder.

The analog meter is a zero-center instrument that is handy for peaking, nulling and making other adjustments on circuits evolving rapidly varying signals.

The 360 is a 3½-digit instrument employing 7-segment LED display elements. It can operate from 117 or 240 Vac, 50– 400 Hz lines. For complete isolation from power lines or in cases where ac power is not available, rechargeable NiCad batteries provide up to five hours



of continuous operation. Recharging is automatic when the line cord is plugged in and the function selector is in the BATT CHRG ONLY position. A LED on the panel shows when the battery is being charged.

The function selector switch has four positions: OFF disconnects all power from the internal circuits; BATT CHRG ONLY fully charges the battery in 16 hours; DC OHMS connects the appropriate input jacks for measuring dc current, voltage and resistance; depending on the setting of the range selector. AC connects the appropriate panel jacks to the ac voltage or current metering circuits selected by the range switch.

Voltage ranges are from 200 mV to 1000 Vdc and 600 Vac. The 0-200 and 0-2000-ohm resistance ranges are "low power" with a maximum 150 mV opencircuit. The other ranges are 20K, 200K, 2 megs and 20 megs full scale.

Input jacks—20 μ A, 200 μ A, 2 A and 10 A—are used for current measurements with full scale values selected by the range switch with accuracy $\pm 0.5\%$ of the reading +1 digit (except on 2 A and 10 A ranges where accuracy is $\pm 1\%$ of reading + 1 digit). Six ac ranges cover from 200 μ A to 10 A. Accuracy $\pm 1.0\%$ of the reading +1 digit through 200 mA; $\pm 2.0\%$ of reading +2 digits on 2- and 10-amp ranges.

Size 7.2 \times 5.4 \times 3.75 in., 4.5 lbs. \$295.

CONDUCTANCE AND LEAKAGE current are two unique features of the *Tekelec 357 Multex* dmm. Like the *TA 355* and *TA 356*, the *TA 357* has optional transmissive or reflective liquid-crystal readouts, ZERO control and Touch-n-Hold probe. There are six decade volt age ranges covering 0.1999 volt to 19.99 kV. Input impedance is 10 megohms on



the first three ranges and 1000 megohms on the 1.999- and 19.00-kV ranges with the 100:1 HV probe. An ON-OFF switch displays the ac line voltage when the ac-volts function is selected.

Current (ac and dc) is metered in 0.1999, 1.999, 19.99 and 199.9 mA ranges. Conductance is mhos is measured in four ranges: $2 \times 10^{.6}$, $2 \times 10^{.6}$, $20 \times 10^{.6}$ and $200 \times 10^{.6}$. Leakage current ranges are 10 pA, 100 pA and 1 nA. Size 23% x 51/4 x 91/2 in.\$179.

ITS 3¹/₂-DIGIT DISPLAY makes the *B* & *K* Precision model 282 the "Big Brother" of the 281. It reads voltages in four decade ranges from 1.000 to 1000 volts ac and dc. The 100% overrange feature permits maximum readings of 1.999, 19.99, 199.9 and 1999 on all ranges. On the 1-, 10-, and 100-Vdc ranges accuracy is $\pm 0.5\%$ of the reading ± 1 digit and $\pm 1.0\%$ of the reading ± 1 digit on the 1-kV range.

On ac volts (50 to 200 Hz), accuracy is $\pm 1.0\%$ of the reading ± 1 digit on the three lowest readings and $\pm 1.5\%$ of the reading ± 1 digit on the 1-kV range. Accuracy (50 to 1000 Hz) is $\pm 1\%$ on the 1-, 10- and 100-V ranges and $\pm 1.5\%$ on



the 1.5-kV range. Response is \pm 0.5 dB, 1000 to 10,000 Hz on the 1- and 10-volt ranges; \pm 1 dB, 1000–10,000 Hz on 100-V range and 1000 to 2000 Hz at 1 kV.

Resistance is measured in six decades from 100 ohms to 10 megohms. Accuracy is $\pm 1\%$ of reading ± 1 digit, 100 ohms to 1 megohm; $\pm 2\%$ of reading on 10-meg range.

The test probe has a selectable 100K resistor that is used in making measurements in high-impedance and high-frequency circuits. This resistor, in series with the 10-meg internal voltage divider causes a - 1% error in the reading. When precision is needed, increase the meter reading by 1%.

Operates from 105-125 Vac, 50-60 Hz. $3\frac{1}{2} \times 7 \times 9$ in., 3 lbs. \$200.

RADIO-ELECTRONICS

BUILT IN A PROBE, the *Hewlett-Packard model* 970A has automatic ranging, zero and polarity indication.

The voltmeter ranges are 0.1, 1.0, 10, 100 and 1000 volts with 500 V dc and ac maximum input. On dc the accuracy is $\pm 0.7\%$ of the reading $\pm 0.02\%$ of the range. On ac, accuracy (1 V to 1 kV) is $\pm 2\%$ of the reading $\pm 0.5\%$ of the range —from 45 Hz to 1 kHz. From 1 to 3.5



kHz, accuracy is $\pm 3\%$ of reading +0.5% of range. Five ohmmeter ranges cover from 1K to 10 megs with accuracy of $\pm 1.5\%$ of reading +0.2% of range.

Accessories include 5-range dc and ac ammeter adapters measuring 100 μ A to 1 A fullrange, an rf probe that adds 100 kHz to 500 MHz to the ac measurement range of the 970A.

Size 6½ \times 1¾ \times 1¼ in. 3 lbs. \$275.

FIVE MODELS in the Weston series 4400 of dmm's are within the \$300 limit set for this listing. They vary in accuracy, number of ranges, functions and the type of operation. They are all $3\frac{1}{2}$ -digit instruments. The 4440, 4442 (shown) and 4443 are self-contained portables with rechargeable battery packs that deliver up to twelve hours of continuous power. The 4448 and 4449 are for use on 117 Vac, 60-Hz only.

Models 4442 and 4449 have twenty ranges covering from 20 mV to 1 kV ac and dc, 200 ohms to 20 megs plus 199.9



 μ A and 1.999 mA dc and ac current ranges. The 4443 measures only dc volts and current and resistance in the same ranges as the other instruments in the series.

All instruments in the 4400 Series are 2.25 \times 5.45 \times 7 in. and weigh less than 2.5 lbs. Prices range from \$220 for the model 4448 to \$275 for the 4442.

sured. The dmm automatically selects the correct range and positions the decimal point to give the most accurate reading.

Now that we've had a look at the dmm. let's take a look at the pertinent specifications of dmm's in the \$300 and under range.

MANUFACTURERS

Ballantine Laboratories PO Box 97 Boonton, NJ 07005

B & K, Div. of Dynascan Corp. 1801 W. Belle Plaine Ave. Chicago, IL 60613

LIQUID-CRYSTAL DISPLAYS using fieldeffect 7-segment devices are featured in the *Tekelec model TA 355, TA 356* and *TA 357* dmm's. The *TA 355* bench model and the *TA 356* portable dmm have five functions, 25 ranges with pushbutton range and function selectors. Sensitivity is 100 μ V on ac and dc voltage, 100 nA ac and dc and 0.1 ohm.

The standard displays are transmissive types—black on a white background. The optional reflective displays are black on a grey-green background. The ZERO control is a screwdriver adjustment on the 355 and a thumb-wheel control on the 356. Range-to-range shift is 1 digit, maximum. The reading rate on the portable is fixed at 3 per second.



A 3-position rocker switch on the 355 selects 3 readings/second, 1 reading/ second or "hold" the reading indefinitely.

The *TA* 356 operates from internal rechargeable NiCad batteries with a life of about 6 hours per charge with the transmissive display and 8–10 hours with the reflective display. The separate power supply/battery charger is standard for either 117 V, 60 Hz or 230 V, 50 Hz.

The *TA 355* can be specified to operate from either 117 Vac, 60 Hz or 230 Vac, 50 Hz. Interchangeable NiCad batteries and charger/ac supply are optional.

Dc and ac voltage ranges are 0.1999, 1.999, 19.99, 19.99 and 1000 volts. Current ranges are 0.1999, 1.999, 19.99, 19.99, 19.99 and 1999 mA. Resistance ranges are 0.1999, 1.999, 19.99, 19.99 ohms and 1.999 megohms.

Options are Touch-n-Hold probes and BCD printer output (*TA* 355 only). The *TA* 355 is $3\frac{1}{2} \times 8\frac{1}{2} \times 12\frac{3}{4}$ in.; the *TA* 356 is $2\frac{3}{8} \times 5\frac{1}{4} \times 9\frac{1}{4}$ in. \$289 each. Dana Laboratories 2401 Campus Drive Irvine, CA 92664

Data Precision Corp. Audubon Rd. Wakefield, MA 01880

Data Technology Corp. 2700 Fairview St. Santa Ana, CA 92704

DigiTec (United Systems Corp.) 918 Woodley Rd. Dayton, OH 45403

John Fluke Mfg. Co. PO Box 7428 Seattle, WA 98113

Heath Co. Benton Harbor, MI 49022

Hewlett-Packard Co. 1501 Page Mill Rd. Palo Alto, CA 94304

Keithley Instruments Corp. 28775 Aurora Rd. Cleveland, OH 44139

Non-Linear Systems PO Box N Del Mar, CA 92014

Schneider Electronics 11 Riverside St. Medford, MA 02155

Simpson Electric Co. 853 Dundee Ave. Elgin, IL 60120

Tekelec, Inc. 31829 W. La Tienda Drive Westlake Village, CA 91361

Weston Instruments 614 Frelinghuysen Ave. Newark, NJ 07114

A TEMPERATURE RANGE of -50°C to +200°C is a unique feature of the Digitest 610, a product of Schneider Electronics, Inc. It is a 4½-digit instrument with four piano-type function keys —for temperature, resistar cc. voltage and current—along the right edge of the case and six range keys across the bottom. It operates from built-in NiCad batteries and from 117 or 200 V, 50– 6- Hz. A BATTERY-TEST function is included.



Resistances from 0.1 ohm to 5 megs are measured in five ranges. Ac and dc currents from 100 nA to 1 mA are measured in one range; voltage from 100 μ V to 1 kV in four ranges.

The Digitest 610 is 3.35 \times 4.73 \times 9.06 in., 3.5 lbs. with batteries. \$295.

(Product Listing continues on page 81)

THINGS ARE GOING DIGITAL ALL OVER the place. Aside from the advantage of getting a definite figure for a given reading, the digital-readout instruments have the advantage of high accuracy. A lab instrument can be as accurate as 0.002%, and field type instruments are now in use at 0.2% and even better.

There are places where the old-fashioned D'Arsonval meter still has a slight advantage. It is easier to see a peak in a reading with a meter-needle. or sudden current-surges, etc. However, for use in labs, R&D, and service work, the precise figures displayed by the digital readouts is definitely better. In many modern circuits we must

they can be made with letters, etc.). Each cathode is switched on to display the digit.

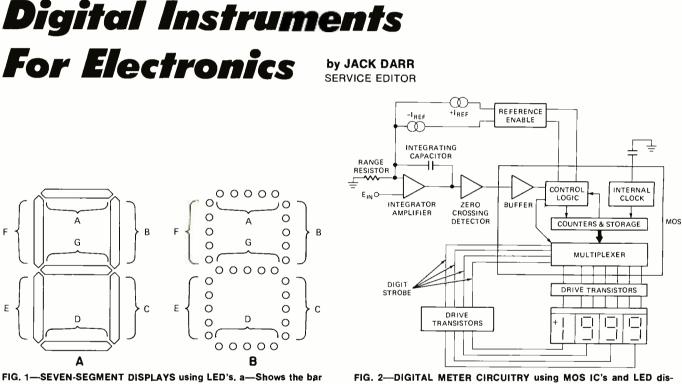
The latest thing is a light-emitting diode (LED) readout. These are mostly of the GaAs type, and emit red light with only a very small amount of voltage and current (other materials are used to produce green or yellow readouts). There are two major types; the dot and the "seven-segment" type, with seven bars. These are arranged in a pattern like Fig. 1. To make an "8", all bars are activated. To make a "3", bars A, F, G, E and D are energized, and so on.

The LED dot displays work just like the 7-segment bar type, but they use

er) are often combined in the same IC. It decodes the BCD (Binary-Coded-Decimal) signals from the Memory-Latch, and converts them into signals to actuate the display.

The Memory-Latch is fed by the Decade Counters; we'll trace this out in a moment. The main difference between Nixie and LED readouts is the voltage. Nixies use about 100 volts, LED's about 15 volts. So, LED's work well with the low-voltage TTL IC's used in the control circuitry. LED's, however, do draw more current than the Nixie type display and do not use very much less power.

Now let's follow the control process through, from the counter inputs.



type, and b-The dot type. Five dots equal one bar.

play. Display units light in sequence, but so fast that there's no flicker.

be pretty accurate; transistor voltages, etc. The digital readout gives us our measurement as "10.75 volts" or whatever is called for. (It is slightly disconcerting to some old goats to see such a reading displayed as "10.7543 volts"! It takes a little practice to learn to ignore the "LSD" which is not a chemical but "Least Significant Digit"!)

How they work

Digital readouts are made with several different types of display units. The original was the Nixie tube made by the Burroughs Co. It is a cold-cathode tube like a neon lamp. It has a common anode, and ten cathodes-0 through 9 (in the most common type; sets of four or five individual LED's to make the equivalent of the bar. Liquid-crystal displays have been used in some instruments, but there are still some drawbacks-visibility to name just one. As a result, they're not quite as common as the others.

The control circuitry

All of these readouts use a control system which is basically similar. Starting at the display unit and working back toward the input, we go through a Display Driver. This is a set of solidstate switches which controls the illumination of the desired segments of the display. It is fed by a Decoder. These two circuits (decoder and display drivThe decade counters do just that; count to ten. Their input will be a series of digital pulses, usually BCD, from the input of the instrument. Each of these counts up to 9 pulses, then transfers the tenth pulse to the following decade counter and starts over. The counters are connected in series; each one controls one of the digital readouts. The first operates the "units" readout, the next the "tens", next the hundreds, and so on and on.

Their input signal is controlled by a "clock oscillator"; its high frequency has been divided down to get a longer sampling period. A sampling circuit controls the gating of the input signal into "slices" of a given time-duration,

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say 1.0 ms. If we're counting a frequency, these circuits will slice off a 1.0 ms sample, square it into square waves, and feed it to the decade counters.

The counters receive the input for the period of time selected by the instrument controls. While doing this, the first decade counter counts up to 9, then passes the next pulse along to the tens counter. This one takes the first 9 counts, and then passes along a "100" count to the following counter. This can go on as long as necessary, depending on the number of units (digits) in the display, and the signal heing counted.

At the end of the counting or sam-

commands them to deliver one output (that is, the output signal which will light only one digit of the display) for giver combinations of high and low on the inputs. A Nixie driver will have the four logic inputs, and ten individual outputs, one for each digit. The one corresponding to the desired digit will go low (grounding the proper cathode in the tube) and all others will remain high. In a Nixie display, all of the tubes light at the same time.

For LED displays, the same basic circuitry is used. But there can be some differences in the actual operation. For example, the Weston panelmeter unit, Model 1221, in Fig. 2, has a four-digit LED display. This one ily obtained with low-voltage TTL logic units, since it takes only a few volts to bring an LED to full brilliance.

Needless to say, this kind of work can only be done by liberal use of integrated circuit technology. In many of the new instruments, even these are being supplanted by large scale integrated MOS IC's (LSI-MOS). Fig. 3 shows the "works" of a Weston Model 1230 bipolar panel-meter. Fig. 4 shows a front view of the Model 1220 and 1221, which does the same thing with only a single LSI chip! You can do it with discrete transistors but you'll need a U-Haul truck to carry it around!



FIG. 3—INSIDE A DIGITAL PANEL METER. This unit is a Weston Model 1230.



FIG. 4—A SINGLE IC does all the work in this digital panel meter.



FIG. 5—HEATHKIT MODEL IB-1100 frequency counter uses Nixie type readout.

pling period, the total number of counts is present on the string of counters, as logic highs or lows at their terminals. Next, a "transfer pulse" commands the counters to send the stored numbers along to the Memory Latch, and reset themselves to zero. These memory latches transfer the stored signals to their outputs when the transfer line goes to a logic low, they "remember" the figure, and hold it. This is then transferred to the decoder-drivers.

These decode the BCD signal, which is on four lines (called A, B, C and D to avoid confusion with figures (and we'll have enough confusion as it is). The "truth-table" for the decoders



FIG. 6—THIS FREQUENCY COUNTER has eight digits in its readout and goes out to 120 MHz.



FIG. 7—A FREQUENCY COUNTER CAN be used to check the frequency of an amateur radio rig.

uses a seven-segment display.

A mildly unusual method of lighting the LED's is used. The count comes through the logic, the multiplexer unit, and goes to seven lines leading to the display. All lines are connected to each LED unit, in parallel. To display different figures, the entire display is "strobed" by the second set of drive transistors; in other words, each unit is flashed in sequence, by the strobe signal from the multiplexer. So it displays only the digit which its logic signals tell it to.

The scanning is so fast that the display seems to be continuously lit; in this instrument, at a 100-Hz rate. This kind of switching and scanning is eas-



FIG. 8—HIGH-FREQUENCY MEASURE-MENTS can be made with instruments like H-P 5354A. It goes to 4 GHz.

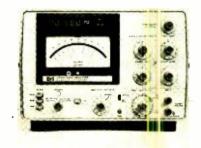


FIG. 9—COMBINATION INSTFIU MENT is a wave analyzer and a selective voltmeter. Interesting combination of digital meter and analog meter.

Typical instruments

Now let's look at a few of the ways in which a digital readout can be used to improve the usefulness of an instrument. We have always had instruments which were potentially very accurate; now we have a readout that can match this. For the first, look again at the Weston Dig tal Panel Meter in Figs. 3 and 4. This is a simple (On the outside, anyhow!) black hox.

It is basically a voltmeter. By selecting values for built-in range resistors, it can be anything from a 0 to 100-mV voltmeter to a 1000-volt meter. De current from 10 mA (ful-scale to 100 mA can also be read. Ac voltages and currents can be read with an ac adapter, Model 9744.

Data can be provided to make the model 1220 or 1221 read engineering units—feet, pounds, rpm, pressure, and so on. The only difference between the two models is the power supply; the 1220 uses 5.5 volts dc, and the 1221 is 117-volt ac powered.

Frequency-countnig is one of the tricks that digital readouts do well. The Heath Co. has four models, the IB-1100 (5 digits, to 30 MHz), the IB-1101 (5 digits, to 100 MHz +), the IB-1102, (8 digits, to 120 MHz) and the IB-1103 ($8\frac{1}{2}$ digits, to 180 MHz). These are shown in Figures 5 and 6.

Figure 10 shows the H-P 8640B vhf signal generator, with a digital readout that can be used to show the output frequency, or to read the frequency of an external signal. It will go from 450 kHz to 550 MHz, on AM or FM. The D'Arsonval meter on the panel will also do tricks! It read AM modulation percentage, FM peak deviation or output level in dBm or volts, and it is an autoranger. No switching is needed: it adjusts itself.

Figure 12 shows an H-P Model 5270A Automatic Capacitance Bridge. It has a dual digital readout; one reads the capacitance, and the other the dissipation factor or conductance, whichever is desired, simultaneously.

to a signal that is drifting or changing in frequency. Indicator lights on the panel tell whether the circuit is locked or unlocked to the signal.

Figure 11 is the front panel of an oscilloscope. Innocent-looking enough, isn't it? It isn't. This is a *digital oscilloscope*, the Nicolet Instrument Corp. Model 1090. The difference lies in the way the signal can be displayed. A standard analog scope displays the instantaneous waveform. Storage scopes can hold it, on the special screen of the crt. In the Model 1090, the signal is not fed to the crt. It goes, instead, to a memory bank with a capability of storing 4096 words of 12 bits each.

To display the recorded waveform



FIG. 10—VHF SIGNAL GENERATOR (450 kHz to 550 MHz) has digital readout to show what frequency signal it is producing.



FIG. 11—DIGITAL SCOPE made by Nicolet Instrument converts visual signals into digital code and then remembers the code so it can display the remembered waveform on demand.

Hewlett-Packard makes a Model 5307A counter. It is basically a frequency counter, but with the proper transducers can be used for many measurements; vibration, shock, transients, and so on. The Model 5307A is a high-resolution type.

Figure 7 shows another use for a frequency counter. Here, the Hewlett-Packard Model 5382 is being used to check frequency on an amateur rig. This would be the height of something or other to me! Carrier frequency can be accurately read to within 10 Hz!

Figure 8 shows an H-P Model 5354A counter. It will go to 4 GHz, and lock automatically on pulse-trains, as well as CW.



FIG. 12—AUTOMATIC CAPACITANCE BRIDGE has a dual digital readout.



FIG. 13—ELECTRONIC STOP WATCH by TAFCO is a different kind of digital instrument.

Figure 16 is another capacitance meter. This one is the H-P Model 4282A High Capacitance Meter. The unusual thing about it is its top range; it will go to ONE FARAD. (When I first went into this business, one Farad was literally an inconceivable quantity.) The 4282A will make other handy measurements too: the internal capacitance of a battery; capacitance of a transistor, and so on.

Figure 9 shows an interesting combination instrument; the H-P 3681A Wave Analyzer and Selective Voltmeter. Tuned to a known frequency component of a signal, this instrument will read it to five-digit accuracy, or 1.0 Hz. It has afc which allows locking it

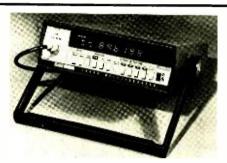


FIG. 14—AUTORANGING FREQUENCY counter by John Fluke Company uses LSI MOS IC's.



FIG. 15-UNIVERSAL COUNTER-TIMER from Tektronix.

the controls are adjusted, and the waveform is repeated indefinitely. Crosshair vertical and horizontal lines on the display can be adjusted to intersect any part of the waveform. When this is done, by pressing the COORDI-NATES button under Numerics, the time since the trigger is shown on the bottom of the crt screen in figures, at the left side. On the right side is displayed the voltage of the waveform at that point, also in figures. By adjusting the controls, any point along the whole length of the 4096-word recorded waveform may be frozen and studied. One engineer told me that this was equivalent to a scope with a trace twenty-two feet long.

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Nicolet Instruments also offers their Model 93 plug-in for their scope. This has a dual channel input. Either input may be recorded in the memory bank, at will. Note the STORAGE CONTROL pushbuttons in the center. By pushing HOLD NEXT the memory records the waveform that comes along after the next trigger signal. HOLD LAST records what followed the last trigger. LIVE shows that waveform as it is actually taking place, in real time. The Model 93 plug-in will even display the stored information while watching live signals, at the same time.

Figure 13 shows still another use. This is an electronic stop-watch, with a digital readout. Using a crystal-conthe same well known company, another unit in the same series, with a slightly different form of digital readout, is a dc power supply. It is very tightly regulated, and the exact voltage output is shown on the three-thumbwheel control — a special kind of "digital readout".

Tektronix also make a 550-MHz Frequency Counter, with digital readout, plus indicator lamps to make sure you know where you are in the band. Fig. 15 shows a Model DC-505 "Universal Counter-Timer", which will do so many things that I'm not even going to try. Check that panel.

A novel approach to the use of a scope as well as a digital meter can be

events-counting, etc.) you set the figures on the thumbwheel dials. When the number of events reaches the preset count, the DD-501 puts but a trigger pulse, for an oscilloscope or any other type of triggered instrument.

A well-known name in the service instrument field, the Simpson Electric Co., makers of the famous old 260 vom, also shows up in the digital field. Figure 19 shows an instrument that might be called "Son Of 260" It's the digital vom, Model 360. There is also a "lay-down case" type, the Model 460 in the same line. The same company also makes a digital panel-meter (Fig. 20). This basic instrument can be made to read almost any quantity de-



FIG. 16---HIGH-CAPACITANCE METER accurately reads capacitor values as large as one Farad.



FIG. 17—DIGITAL DELAY MODULE by Tektronix. Thumbwheel switch for getting count is also digital readout.

trolled clock, it can be used in two ways; for timing the overall time of an event, and also for checking lap times. etc. *without* losing the overall count.

Figure 14 is an autoranging counter from the John Fluke Co. It will go up to 80MHz, and count as low as 5 Hz. This versatile instrument is also made possible by LSI chips.

Figure 18 shows one of the numerous combinations of instruments possible in Tektronix's new TM-500 series. It shows an SG-503 oscillator, a DC 504 Counter-Time and a DM-502 Digital Multimeter, in a 3-unit Mainframe. The power supply for all three is provided by the mainframe. From

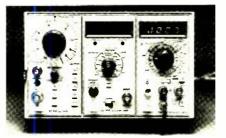


FIG. 18---COUNTER/TIMER module with digital display is part of new Tektronix instrument system.



FIG. 19—SON OF 260 is the Simpson model 360 digital vom.

yours mounting a DM-40 DMM on top of a 465 portable Oscilloscope. Now, many things can be done. For only one, you can read the time interval between any two points on the waveform; this is shown on the digital readout in whatever units are needed. Accuracy of this is within 0.1%.

A typical use of the plug-in concept of the TM-500 Series is in a Medical Instrument Calibration System; it can be used for calibrating EKG, ECG, Crash-carts, and many other types of medical electronic instrumentation.

Figure 17 shows an unusual digital readout application. It is a Tektronix DD-501 Digital Delay. To read any desired count (for applications such as



FIG. 20-DIGITAL PANEL METER can be used to read almost any quantity



FIG. 21----MOST UNUSUAL DIGITAL instrument we found is this Green Bant: Scientific Sobriety Tester.

sired, with a few simple charges. This is the Model 2830.

Last but not least, we see in instrument that could conceivably cause some arguments. It is made by Green Bank Scientific Co., Box 100, Green Bank, W. Va., along with several other similar instruments. It's a digital-readout Sobriety Tester. You get a definite PASS or FAIL readout. Figure 21 shows the instrument.

There are probably many other uses for these versatile and highly accurate instruments, but this is a representative sampling of what is being done in the field at the moment. **R-E**

40 PROJECTIS Using COSMOS Digital IC's

This is part III in a series of articles describing COSMOS IC's, the latest in solid-state technology. Monostable and astable multivibrator circuits are described here, along with simple circuits you can build.

by R. M. MARSTON

IN PART II OF THIS SERIES WE LOOKED AT the operating principles of COS/MOS digital IC's, and explored a number of practical ways of using the CD4001 IC in inverter, gate, and logic applications. We went on to discuss bistable multivibrator applications.

In this third part of the series, we go on to look at monostable and astable multivibrator applications.

Monostable multivibrator projects

A basic monostable or one-shot multivibrator can be made from two NOT or NOR logic gates by direct-coupling the output of one gate to the input of the other, and by coupling the output of the second gate to the input of the first via a simple R-C time constant network. Figure 21 shows a practical way of making a basic monostable multivibrator, or pulse stretcher, from one half of a CD4001 cos/Mos 1C. You can also use the KD4001.

Here, gate A is used as a NOR logic element, and gate B is used as an inverter or NOT gate. The circuit action follows:

Normally, when the circuit is in its quiescent state, the input to gate B is held high via R1, so the output at gate B is low: Both input terminals of gate A are thus low, so the output of gate A is high. Consequently, since both ends of C1 are high, C1 is fully discharged.

Suppose now that a brief positive trigger pulse is applied to the input of gate A. As soon as this pulse is applied, it drives the output of gate A to ground and drags the input of gate B with it via discharged capacitor C1: Consequently, the output of gate B immediately goes high, and thus holds the output of gate A in the low state even when the input trigger pulse is subsequently removed.

As soon as the output of gate A goes low as the result of the applied trigger pulse, C1 starts to charge via R1, and an exponential rising voltage is applied to the input of gate B via the R1-C1 junction. Eventually, after a delay determined by the R1 and C1 values, this exponential voltage rises to the transfer voltage of gate B, and at this point, the output of gate B switches sharply back into the low state. As the output of gate B goes low it

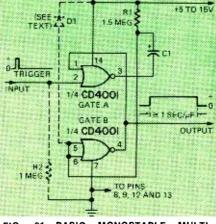


FIG. 21—BASIC MONOSTABLE MULTI-VIBRATOR or pulse stretcher.

causes the output of gate A to go high: C1 then discharges rapidly via the output of gate A and input protection diode D1 (see Fig. 7-b, September 1974 issue) of gate B, and the operating sequence is then complete.

Thus, the output of the Fig. 21 circuit is normally low, but goes high as soon as a brief positive trigger pulse is applied to the input: The output then remains high for a certain period, and then switches abruptly back to the low state again: The precise period of the output pulse is determined by the R-C time constant, and by the value of the transfer voltage of the individual CD4001 IC that is used.

Three points should be noted about this particular circuit. The first point is that, since the period of the circuit is dependent on the transfer voltage of the particular CD4001 that is used, the period that is obtained using a particular set of R-C values can vary considerably between one CD4001 and another. The CD4001 in fact has a production transfer voltage spread of 30% to 70% of the supply voltage.

In practice, the transfer voltage of any particular CD4001 is almost constant over a wide range of temperature and supply voltages, so the Fig. 21 circuit has excellent stability, but must have its time constant values individually adjusted to give a particular timing period. The Fig. 21 circuit in fact gives a period of roughly 1 second per μ F of C1 value when R1 has a value of 1.5 megohms.

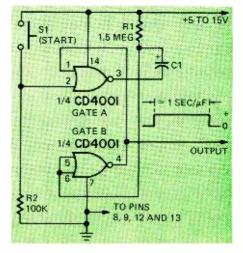
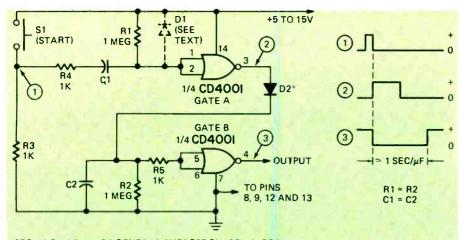


FIG. 22—"NOISELESS" PUSH BUTTON or manually-triggered monostable.

RADIO-ELECTRONICS



^{*}D2 = LOW-LEAKAGE GENERAL-PURPOSE SILICON DIODE

FIG. 23-BASIC COMPENSATED monostable multivibrator.

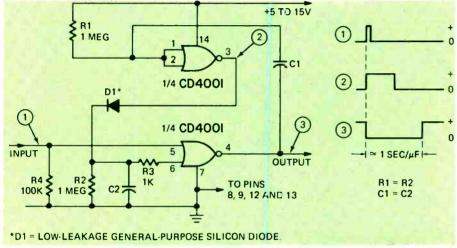


FIG. 24—IMPROVED COMPENSATED monostable multivibrator.

C1 can have any value between a few pF and hundreds of μ F: The value of R1 can range from a few thousand ohms to thousands of megohms, if required.

The second point to note about the circuit is that its input must always be tied to ground in the absence of the positive trigger pulse: This requirement can be met by applying the input from a permanently connected de source, or by strapping the input terminal to ground via a 1-megohm resistor, as shown dotted by **R2** in the diagram.

The final point to note is that, since an exponential voltage is applied to the input of one of the gates during the operating cycle, the gate is driven into its linear region during each operating cycle. A measurable current thus flows in the circuit during the operating period. All cos/Mos monostable and astable multivibrator circuits in fact pass a measurable current when they are in their functional modes.

Figure 22 shows how the circuit in Fig. 21 can be used as a 'noiseless' pushbutton or manually-triggered monostable by simply using the push-button to apply the positive trigger pulse to the circuit.

It has already been pointed out that a snag with the basic monostable circuit of Fig. 21 is that its period depends on the transfer voltage of the individual CD4001, and is not dictated solely by the R and C values. Figure 23 shows the basic circuit of a compensated monostable multivibrator that does not suffer from this snag. The diagram also shows the basic waveforms of the circuit. Note that the circuit uses two sets of R-C time-constant components. Circuit operation is as follows:

When the circuit is in its quiescent state the S1 side of C1 is grounded via R3, but the R1 side is held positive: C1 is thus fully charged under this condition, and the input of gate A is high. The output of gate A is thus low, so C2 is fully discharged at this time, and the output of gate B is high.

Suppose now that START button S1 is briefly closed and then released. As S1 is closed, the S1 end of C1 is connected to the positive supply line, and C1 discharges rapidly via R4 and D1 (which is one of the input protection diodes built into the CD4001): This action has no effect on the circuit. When S1 is released, however, C1 is fully discharged, so as soon as S1 is released. C1 starts to recharge via R1, R3, and R4, thus pulling the input of gate A low and making the output of gate A go high: As the output of gate A goes high, it charges C2 rapidly via D2, and thus causes the output at gate B to go low.

As soon as S1 is released, C1 starts to charge up, and a rising exponential voltage is applied to the input of gate A. After a time determined by the R1 and C1 values, this voltage RISES to the transfer voltage of gate A, and at this point the output of gate A switches sharply into the low state and removes the charging voltage from C2 as D2 becomes reverse biased. C2 then starts to discharge via R2, and after a time determined by the R2 and C2 values, the C2 voltage FALLS to the transfer voltage of gate B, and at this point the output of gate B switches sharply into the high state. The operating sequence of the circuit is then complete. Note that R4 and R5 are used purely as safety resistors, and prevent heavy capacitor discharge currents from flowing into the IC gates if power is removed from the circuit during the operating sequence.

Now, this particular circuit uses two identical R-C time constant networks, and its final output period is equal to the sum of the two individual time constants. The important point to note, however, is that one of these time constants causes a circuit action when its exponential voltage RISES to the transfer voltage of gate A, and the other causes a circuit action when its voltage FALLS to the transfer voltage of gate B. Consequently, if both gates have identical transfer voltages, the transfer voltage values effectively cancel out, and have no effect on the actual period of the circuit.

For example, if both gates have transfer voltages of 30%, C1 will have to charge to 30% of the supply voltage to cause gate A to change state, and C2 will discharge by 70% of the supply voltage to cause gate B to change state, thus giving a total voltage change of 100%. If, on the other hand, both gates have transfer voltages of 40%, C1 will charge to 40% and C2 will discharge by 60% during the operating sequence, again giving a total voltage swing of 100%. The total period of the circuit is thus independent of the transfer voltage value of the IC, providing that both gates have identical transfer voltage values.

Now, although transfer voltage values can vary over wide limits between individual \cos/mos IC's, the individual transfer voltage values of a set of gates within a single CD4001 are alway: virtually identical, since the gates are all formed on the same semiconductor chip at the same time. Consequently, the total timing period of the Fig. 23 circuit is dictated purely by the values of R1-C1 and R2-C2, and is independent of vertations in the parameters of individual CD4001 IC's.

The Fig. 23 circuit is shown as being manually triggered. The circuit can be modified for electronic triggering by simply eliminating S1 and applying the positive trigger pulse across R3. In either case, a practical disadvantage of the circuit in Fig. 23 is that the actual monostable action is initiated by the end, rather than the start, of the input trigger pulse. This snag can be overcome by modifying the circuit as shown in Fig. 24.

This circuit gives an cutput that is normally high (positive), but which goes low (to zero volts) for a preset period when a trigger pulse is applied. If re-

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quired, the polarity of the output signal can be reversed, so that it is normally low but goes high for the duration of the output pulse, by simply wiring an inverter into the output of the circuit in Fig. 24, as shown in the positive-output compensated monostable circuit of Fig. 25.

Astable multivibrator circuits

The most widely used type of multivibrator circuit is the astable, or squarewave generator. Figure 26 shows how one half of a CD4001 cos/mos IC can be used to make a basic 1-kHz astable multivibrator. Note that both gates of the circuit are connected as simple inverters, and that the circuit uses only a single set of R-C time constant components. The action of the circuit is as follows:

Suppose initially that a stage has been reached in the circuit operation where the output of gate B has just switched into the high state and the output of gate A has just switched into the low state, and that C1 is fully discharged at this moment.

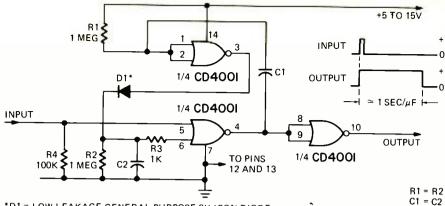
Since C1 is discharged at this time, the input of gate A is effectively shorted to the output of gate B, and is high. As soon as the above stage of operation is obtained, C1 starts to charge up via R1 and the low (effectively grounded) output of gate A (which is derived from the R1-C1 junction) starts to decay exponentially towards zero.

Eventually, after a delay determined by R1 and C1, the input voltage of gate A falls to the transfer voltage point of gate A and at this instant, the output of gate A switches into the high state and drives the output of gate B into the low state: As the output of gate B switches to the low state, it forces the positive end of C1 downwards, and thus forces the gate A input end of C1 to attempt to swing negative with respect to the zero volts line: As the input of gate A goes negative to the zero volts line, input protection diode D3 (see Fig. 7-b, September 1974 issue) conducts and removes the charge from C1.

Thus, at the end of this switching cycle, C1 is again fully discharged, the output of gate B and the input of gate A are low, and the output of gate A and the input of gate B are high.

As soon as this new stage of the operation is obtained, C1 starts to recharge in in the reverse direction via R1 and the low (grounded) output of gate B, and the voltage at the input of gate A (which is derived from the R1-C1 junction) starts to rise exponentially towards the positive voltage. Eventually, after another delay determined by R1 and C1, the input voltage of gate A rises to the transfer voltage of the gate and at this instant, the output of gate A switches into the low state and drives the output of gate B into the high state.

At this moment, C1 discharges rapidly via input protection diode D1 of gate A as the R1-C1 junction end of the capacitor attempts to go positive relative to the positive supply line, and the operating sequence is then complete. The switching sequence then repeats ad infinitum, and a series of approximately



HIGH (OFF)

GATE INPUT

LOW (ON)

*D1 = LOW-LEAKAGE GENERAL PURPOSE SILICON DIODE

FIG. 25—POSITIVE-OUTPUT compensated

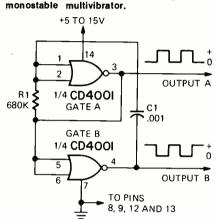


FIG. 26—BASIC 1-KHZ ASTABLE multivibrator or square-wave generator.

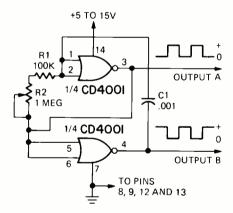
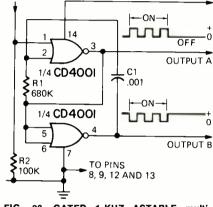


FIG. 27—VARIABLE FREQUENCY (600 Hz-6 kHz) astable multivibrator.

square waves are generated at the two outputs of the circuit: Outputs A and B are 180° out of phase.

An outstanding feature of the basic astable multivibrator circuit of Fig. 26 is that it uses only two time constant components (R1 and C1), and the values of both of these components can be varied over wide ranges to give required operating frequencies. The value of R1 can be varied from a few thousand ohms to thousands of megohms, and C1 (which must be a non-polarized capacitor) can be varied from a few pF to several μ F. The operating frequency is inversely proportional to the R1 and C1 values, and can be varied from less than one cycle per hour to several MHz.

The operating frequency of this circuit can be made variable, if required, by



+5 TO 15V

FIG. 28—GATED 1-KHZ ASTABLE multivibrator.

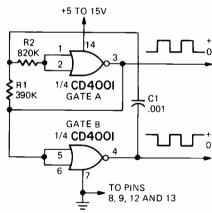


FIG. 29—COMPENSATED 1-KHZ astable multivibrator.

wiring a variable resistor in series with limiting resistor R_1 , as shown in the circuit of Fig. 27. With the component values shown, this circuit covers the approximate frequency range 600 Hz to 6 kHz.

If required, the basic astable multivibrator of Fig. 26 can be gated on or off via an external pulse signal by connecting gate A as a NOR gate and applying the gating signal to one of the NOR gate inputs, as shown in Fig. 28. The multivibrator is cut off when the gate input signal is high, and is operative when the gate input signal is low.

The basic astable multivibrator of Fig. 26 acts as a simple and very useful circuit, but suffers from several disadvantages. The first of these is that, since the *(continued on page 88)*

new FTC ratings for audio amplifier power

are they any good?

There are some potential loopholes in the newly imposed FTC rules. Here's a look at how they work and where the problems may lie

> by LEN FELDMAN CONTRIBUTING HI-FI EOITOR

BY THE TIME YOU READ THIS, MANY manufacturers of home entertainment audio products will be busily printing new advertising literature, specification sheets and even the outside of packing cartons. No, the industry has not suddenly redesigned its entire product line-the amplifiers haven't changed that much. But they are changing the statements regarding their power output capability to bring them into line with a new trade regulation promulgated on May 3, 1974 by the Federal Trade Commission. The new rule becomes effective November 4, 1974 and the FTC will consider violations after that date to be "an unfair method of competition and an unfair or deceptive act or practice within the meaning of Section 5 (a) (1) of the Federal Trade Commission Act 15 U.S.C. S 45 (a) (1) to violate any applicable provision of this rule."

Reasons for the FTC action

Over the past few years, some segments of the audio industry have been engaged in a quasi-technical semantic race to devise power output statements for audio amplifiers which would yield higher and higher numbers of "watts of output" for their products. About the only thing these assorted specifications had in common was their use of the word "watts" as a measure of power. But what "kind" of watts were used? There were "continuous watts" —the amount of power that an amplifier would deliver on a continuous basis into a fixed, resistive load.

This measurement, the most conservative of all, became known as rms power, a term which in itself is semantically meaningless. The letters rms stand for "root-mean-square." Many ac voltmeters are calibrated to read 0.707 of peak sinusoidal ac voltage applied to their terminals. In the case of a sine wave, power developed across a load is defined by the Formula $(E_{rms})^2/R = P$, where E_{rms} is the root-mean-square voltage, R is the resistive component of the load impedance across which the output voltage is applied and P is the resulting power in watts. Power itself cannot be termed rms because musical waveforms are seldom, if ever sinusoidal and as an amplifier is driven into clipping or overload, even a pure sinusoidal waveform changes shape so that voltmeter readings no longer correspond to 0.707 of peak voltage values. Nevertheless, the term "rms power" persists and for our purposes can be considered identical to "continuous power"---the more appropriate term.

Another term "music power" (also known as "dynamic power, IHF Dynamic Power or IHF Music Power") has been used to describe amplifier power output at somewhat higher numerical values of wattage. The numbers are based upon the fact that for short periods of time, most amplifiers can deliver somewhat more power than they can on a continuous basis. Since musical waveforms contain relatively short bursts of higher energy, many experts felt that "music power" represented a more meaningful way to describe an amplifier's power putput capability.

Unfortunately, "music power" quickly became corrupted anc gave way to such meaningless terms as "peak power," "peak music power," instantaneous peak power (IPF) and even "instantaneous peak music power." Each of these successive manipulations of terms gave rise to higher and higher wattage figures. It was not uncommon to find products rated at 100 watts "IPP" which actually produced 5 watts or less of "cont nuous power." Small wonder that the FTC stepped in and tried to bring some order into these chaotic audio specs.

A summary of the FTC rule

To begin with, the new FTC regulation requires that all audio products that deliver more than a 2-wait output must specify, in boldest advertising type, the following with regerd to power output:

- 1. "The minimum sine-wave continuous average power output, in watts, per channel
 - a. for each load impedance for which the equipment was designed
 - b. measured with all channels driven
- The manufacturers rated power band or power frequency response, in Hertz (Hz) for each of the rated power outputs required to be disclosed per item (1) and
- 3. The manufacturer's rated percentage of maximum total har-

monic distortion at any power level from 250 mW to the rated power output for **each** rated power output and its corresponding rated power band or frequency response.

A "Legal" power statement

Based upon our interpretation of the above, the following might constitute a proper power output disclosure:

"Brand "X" amplifier has a rated power output of 50 watts per channel, all channels driven, into an impedance of 8 ohms, at any frequency from 20 Hz to 20 kHz, with harmonic distortion not exceeding 0.5%." Similar statements would also have to be made with appropriate numbers substituted for 4 ohm and 16-ohm loads, if the amplifier were designed to operate into these additional load impedances.

Remaining ambiguities

To paraphrase astronaut Armstrong, the new FTC rule represents "one giant step" for the audio industry but the typical hi-fi component purchaser can still be subjected to ambiguities and confusion even if the new rules are strictly followed and enforced. Consider, first, the two power output curves of Fig. 1. Both amplifiers "A" and "B" could be described exactly as in the example

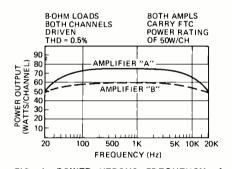


FIG. 1—POWER VERSUS FREQUENCY of two amplifiers at 0.5% THD rating.

above. Each can produce 50 watts at 0.5% THD at the frequency extremes of 20 Hz and 20 kHz. Note, however, that if the power bandwidth had been limited to from 50 Hz to 10 kHz, amplifier "A" could have well been rated as a 70-watt-per-channel amplifier and, with that limitation, would "read" as the better amplifier (which in fact, it actually is).

Figure 2 presents a more confusing situation. The manufacturer of amplifier "B" now *chooses* to rate his amplifier as a 100-watt unit—but at a power bandwidth extending only from 100 Hz to 5 kHz. While more conservative manufacturer "A" prefers to provide data on bandwidth from 20

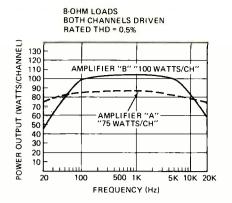


FIG. 2---"LOWER POWERED" AMPLIFIER A can actually produce more power at frequencies in shaded areas because of its better power bandwidth.

Hz to 20 kHz, and therefore limits his power rating to 75 watts. Amplifier "A" will probably sound better when pushed to its power limit, because the low frequency energy demands of music are great, and at 40 Hz, amplifier "A" is actually capable of audibly greater power output than amplifier "B". If this idea is carried to its ridiculous extreme, there is nothing to prevent an amplifier manufacturer from specifying power bandwidth from 999 Hz to 1001 Hz so as to come up with the highest wattage rating possible (power output at midfrequencies is almost always easier to achieve than at frequency extremes. Only an educated consumer could be expected to understand this subtle subterfuge and separate the good amplifier from the not-so-good one.

Thus far, we have given examples of pairs of amplifiers having identical rated harmonic distortion (THD). In this area, too, there is unlimited latitude for manufacturers to take. Consider Fig. 3. Amplifier "B" appears to have greater power output than amplifier "A" and even has great power bandwidth (20 Hz to 20 kHz against 30 Hz to 20 kHz) but is it, indeed the "better" amplifier? Its rated distortion is quoted as 1.0% while that of amplifier "A" is quoted as 0.1%. If amplifier "A" were driven harder, so as to produce the 50 watts shown for amplifier "B," would its distortion be

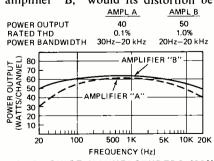


FIG. 3—SINCE MANUFACTURERS MAY QUOTE different rated harmonic distortions for their products, a fair comparison of these two amplifiers cannot be made without further information or lab testing.

better, equal to, or worse than the 1% quoted for amplifier "A"? Further, would its power bandwidth then equal or exceed the 20 Hz to 20-kHz bandwidth quoted for amplifier "A"? The only way a consumer can know would be to take both amplifiers to a properly equipped laboratory and have them measured under identical conditions, even though *both* manufacturers have fully complied with the new FTC rule.

Pre-conditioning tests

In an attempt to insure that all amplifier ratings are determined on the basis of long term operation and stability of the product being specified, the FTC rule also calls for certain standard test conditions (120-volt supply voltage for example) and a one hour pre-conditioning test during which the amplifier is required to deliver $\frac{1}{3}$ of its rated power to a resistive load. Anyone familiar with class "B" operation of solid state amplifiers knows that maximum internal power dissipation of the output transistors occurs when 40% of maximum power is delivered to the external loads. Since $\frac{1}{3}$ of full power is very close to 40% of full power, this means that the output devices will be dissipating nearly their maximum. Many better amplifiers are equipped with electronic protection circuits which would interrupt power under these conditions. In theory, such amplifiers would have fulfilled their pre-conditioning tests even if no power were delivered to the loads for the last 40 minutes of the specified hour-though surely the avowed purpose of the pre-conditioning would not have been fulfilled.

On the other hand, manufacturers of less sophisticated amplifiers (which might well destroy themselves or blow their output fuses during these preconditioning tests) may well have to derate their stated power output figures or add cost to their products in the form of larger heat sinks or over rated power output semiconductors. This strikes us as unfair to the consumer and the manufacturer. It is well known that under musical playback conditions, average power output from an amplifier (over a long time period) can be expected to be about 10-dB lower than maximum power produced during moments of loud musical crescendos. Thus, a pre-conditioning test at 10% of rated power would have been more realistic and more meaningful. Such a 10% pre-conditioning test was, in fact, called for in the now obsolete IHF measurement standards.

Other power disclosures

The FTC rule does not specifically prohibit the publication of power out-

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put ratings other than the preferred "continuous" power. It does, however, require that such optional disclosures as "peak power" or "music power" be accompanied by a disclosure of the other accompanying parameters such as impedance and power bandwidth. Distortion, however, need only be quoted for the additionally disclosed rated output (and not all the way down to 250 mW, as in the case of continuous power). The FTC further requires that such optional disclosures be less conspicuously or prominently made than the continuous power output disclosure. They go on to define "less conspicuous" as not being in bold face type nor in type which is more than two-thirds the height of the continuous power disclosure. The advice to the audiophile would seem to be "Read the large print and ignore the fine print!"

A Noble Beginning

Our criticism of the newly issued FTC power rule should not be taken as a negative one in all respects. Certainly the need existed for some clarification of this primary specification as it applies to home audio equipment. We do, however, take issue with those who maintain that the new rule in and of itself, will solve all the problems of misinformation which have been rampant in the audio industry for many years. Literature and advertising matter printed by low-end audio producers of consoles, compacts and low fidelity components will, no doubt, have to be dumped in trash cans (hopefully for paper recycling) and no doubt these hi-fi opportunists will henceforth omit all references to power output rather than be caught with their one or two watts showing.

Reputable manufacturers of good quality component equipment will hardly be affected by the new rule, since they have generally gone beyond its disclosure requirements in the past.

The real point to be made is that the potential audio consumer not be lulled into a false sense of security when reading post-November 1974 specification sheets. There can still be confusion-and you are still not assured of being able to compare products on a totally equal basis. Hopefully, the Institute of High Fidelity will come up with new Amplifier Measurement Standards which should help to make power amplifier specifications more uniform. Until that happens, it's up to the consumer to read specs carefully, compare performance through listening tests, and rely on the hard earned reputation of legitimate high fidelity component manufacturers. R-E

equipment report

Hewlett-Packard 1221A and 1220A Oscilloscopes

THE HEWLETT-PACKARD CO., MAKERS of precision instruments have come up with a new solid-state triggered-sweep oscilloscope that should be ideal for most kinds of electronic work. There are two models; the 1221A singlechannel, and 1220A dual-trace. Otherwise, the two are identical.

The vertical amplifiers have a very wide response, from dc up to 15 mHz, at a risetime of 23 ns. The dual-trace displays in the 1220A use two different modes. The signals are "chopped" at the lower frequencies, from 0.5 s/div up to 1.0 ms/div. This causes the sweep to display small sections of each waveform alternately. While the beam is traveling from one channel to the other, it is completely blanked. So the two waveforms appear to be continuous.

For the higher frequencies, from 0.5 ms/div up to 0.1 ns/div, the switching goes into an "alternate" mode. Now, each trace is fully scanned, and the beam then switches to the other for a full trace.

Each vertical amplifier is identical. They have calibrated vertical attenuators which cover a range from 2 mv/ div up to 10 V/div in 12 separate ranges. A variable attenuator can be used for vernier settings if needed. Pushbutton selector switches allow a choice of CHANNEL A, CHANNEL B, or both at once. The displays are both locked by the signal in CHANNEL A for triggering. Since most work involves signals at the same frequency, one trigger signal can be used for both.

The triggering circuitry will lock in on any signal from 2 Hz to 15 MHz, provided the input signal is large enough to produce one division of vertical deflection. The trigger action is very stable and easily adjusted. Internal, external, or ac line sync can be used by pushing the proper button. For TV work, the 1220A has an internal TV sync separator. This helps to lock any standard TV waveform of either vertical or horizontal frequency.

A slope control allows triggering on

either the positive going or negative going portions of the waveform. Incidentally, the TV sync separator can be used as a low-pass filter for other waveform tests, if needed. Another pushbutton control allows the use of a fixed attenuator with the external trigger signal or external sweep. It has two positions 1:10 or 1:1.

For use with an external horizontal sweep signal, the 1220A can be switched to EXT. HOR. input, when the X-Y/ SWEEP switch is pushed. In the X-Y position, the internal horizontal sweep is disabled, and a sweep signal must be fed into the EXT. HOR. Jack. This is for use with sweep alignment equipment. For vectorscope use, the signal from the red grid can go to the CHANNEL A input, and from the blue grid to the EXT.HOR. input

The CRT used in the 1220A, is a special type. It has the graticule on the inside of the screen, to e iminate parallax errors. The phosphor used is a special P31 type. The trace is blue, and very bright thanks to the 2 kV accelerating voltage used.

A BEAM-FINDER pushbutton is used if there is no trace on the screen This partially collapses the sweep, showing you where the pattern is. In addition to this, the triggering circuitry has another very handy feature. If stead of blanking the trace completely if there is no input signal, an automatic circuit causes the trace to appear This is called the BRIGHT-LINE diaplay. When a signal is applied to the input, the bright-line circuitry is automatically disabled and the triggered sweep operates normally.

Despite all of its complex circuitry the 1220A is a very compact instrument. Only 17 cm high, 30.4 cm. wide and 39.7 cm deep $(7 \times 12 \times 15)$, in inches). The controls are very clearly marked, and the panel is divided into sections so that confusion is elimit ated.

The customary, highly detailed and well-written instruction book and service manual is provided. This gives you full instructions for setting up and operating the 1220A. In addition to this, a very detailed section or the theory and operation of the ir strument is included. R-E

Step-by-step TV Troubleshooters Guide

Analyzing output waveforms is an integral part of troubleshooting a television receiver. This method pinpoints the defective circuit quickly. Here's a guide to this effective method.

by STAN PRENTISS

WITH THE INTRODUCTION OF BOTH better instruments and solid-state color TV receivers, TV waveform analysis has become a science rather than an art. And several manufacturers are already indicating this as they offer factory-generated keyed rainbow signals for checking overall receiver operation and troubleshooting.

In hybrid and tube sets, marginal operation is still possible and even probable if a component is malfunctioning, but solid state receivers either play or shut down sectionally or completely if a single transistor or IC isn't doing its job. The reason is that semiconductors normally operate at 90% of maximum until they either open or short. Leakage (at least for silicon types) is usually negligible unless man made or caused by poor case seals. So, with RCA announcing no more tube receivers, and other set manufacturers probably following, the days of wholesale component substitutions are past, and an analytical approach to repair must prevail. Better color bar generators will help make this possible.

The general approach

When examining an ordinary block

diagram of a color TV receiver, it is important to look at the set in terms of functional units rather than limited stages (see Fig. 1). Using this approach, the overall area of trouble can be located accurately and quickly, then conventional methods such as examining individual parts can take over. With modular and IC receivers this approach should work, for in some of these sets selective waveforms will be either difficult or virtually impossible to obtain. You should, however, be very aware of what each waveform means and why it is there.

Video i.f. amplifiers and agc

As shown in Fig. 2, the upper display (Y1W1) is the total composite video signal. This signal is composed of the vertical sync tips (a); blanking pedestal (b); black peak (c); video information and white peak (d). Point d also shows you when the composite video signal is at full modulation so the agc may be properly set to avoid sync compression. The rf agc is adjusted visually (or with a voltmeter) on weaker signals so that it will become active at some pre-determined dc level (or i.f. agc's strongest output). It's better of course, to use a broadcast signal to set the agc than one from a signal generator since there is usually more than one station in each community, and their signal strengths will normally vary. Using the composite video signal is also an excellent way to determine if agc will drive i.f. amplifiers between cutoff and saturation; such action is normal in well-designed sets. In addition, if the i.f. amplifiers aren't operating correctly; sync, luminance, and chroma are all directly affected, as well as sound. So when servicing a color receiver, check its general video response following the video detector; often your problems begin here and not where they seem to be. Figure 2 also shows the conventional sync pulse tip (Y2W1) with the video removed and a swing of 30 volts p-p. The waveforms in Fig. 2 consist of slightly more than one field since each field is 16.664 μ s in duration, and the scope time base is set for a total of 20 μ s $(10 \operatorname{div} \times 2 \,\mu \mathrm{s/div.}).$

Sync pulses

In Fig. 3, all voltages, time base, and dc references for both waveforms

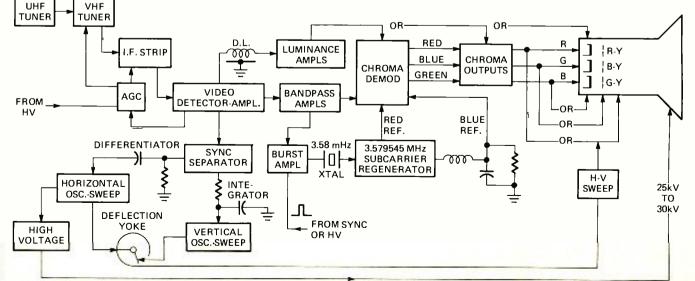


FIG. 1-BLOCK DIAGRAM OF TYPICAL COLOR TV is the same for tube, transistor or IC circuits.

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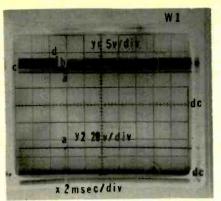


FIG. 2—COMPOSITE VIDEO and sync wave-

see, sync is transmitted only when there is no incoming video, so blanking intervals are important too.

The composite video signal is shown again in Fig. 4 (Y1W3) at a sweep rate of 10 μ s/div. The composite video signal has a blanking interval (g) of just under 12 μ s, and a horizontal sync pulse (h) width of 5 μ s. Note that the sync pulse (h) (Y2W3) has a sharp leading edge because of the instantaneous charge of the differentiator and coupling capacitor, but the capacitor discharge forms a sloppy trailing edge. Only the leading edge, however, is used for the receiver's afc

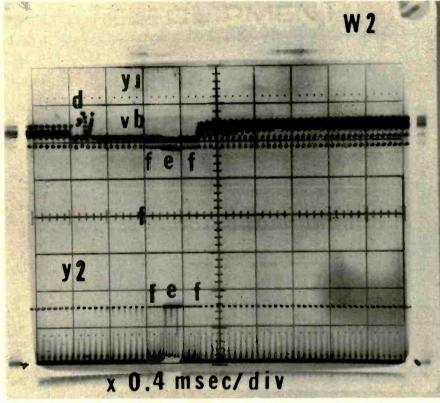


FIG. 3-USING THE SCOPE'S X5 EXPANDER shows the intricate details of Fig. 2.

are the same as in Fig. 2, except we're using the oscilloscope's X5 expander that produces a sweep of 0.4-ms per division instead of 2 ms/div. The blanking interval and sync pulse details now become quite distinct. The 1.4 ms vertical blanking (two fields to a frame) can now be measured quite accurately, and the six vertical pulses (e) are very evident in both waveforms as are the six equalizing pulses (f) which precede and succeed them. If this sync information had been compressed or distorted, the deflection circuits would be malfunctioning, especially the vertical oscillator which is often affected first. Although you won't be expected to count these vertical sync and equalizing pulses each time there is a sync problem, it is comforting to know they're there and not buried somewhere they shouldn't be. As you can sync time comparison. So there's no confusion between leading and trailing edges, let's reverse polarity of the sweep, and show the trace from left to right in Fig. 5, rather than vice versa. What's important about the waveshapes in Fig. 4 is that both sync pulses (Y1W3, Y2W3) should have enough amplitude, duration, and be of the proper shape, for without all these your sync problems can be severe.

Color bar generator substitution

There is only a slight difference in the waveform's video content as we substitute a color bar signal, but the horizontal sync pulse remains the same, as Fig. 5 shows. The pulses in place of video in Y1W4 are the 11 color bars. Bar No. 12 has already been used by the generator as a sync pulse, and No. 11 will be removed by the receiver's blanking circuit before it reaches the chroma demodulator. In the chroma-luminance output, therefore, you'll only see 10 color bars, which represent keying of the color bar oscillator at 30° intervals, producing a rainbow sweep from burst to 300°, inclusive.

The vertical output pulses for all receivers are somewhat similar, but there are horizontal drive differences between tube and solid state receivers. In the tube receiver, the horizontal output signal shown in Fig. 6 (Y1W5), measures 250 volts p-p while the vertical output (Y2W5) is almost 1000

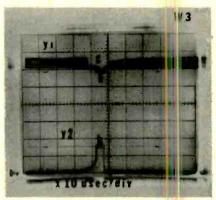


FIG. 4—A FAST SWEEP RATE IS USED to show the blanking interval and sync pulse.

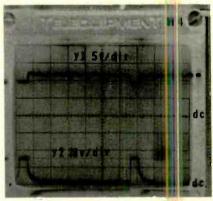


FIG. 5-INTRODUCING THE COLOR BAR GENERATOR.

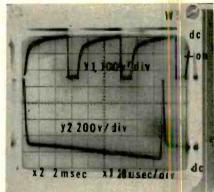


FIG. 6—HORIZONTAL DRIVE and Mertical output signals of a tube color set.

volts p-p. In addition, although the vertical waveform is universal for all sets, the tube horizontal drive pulse must be semi-trapezoid (pulse and NOVEMBER 1974

sawtooth combined) to drive both inductance and resistance in the yoke and flyback circuits, while solid-state versions interface at much lower impedances and may use rectangular waves with duty cycles of approximately 50%. Whether trapezoidal or rectangular, neither waveform drives the horizontal output for more than half the total cycle, so that the output is on for only half the waveform, and only reaches dc and cutoff at its very peak.

In RCA's SCR horizontal deflection drive circuit it's worthwhile looking at all three drive and output traces (Fig. 7). Here we're dealing with silicon controlled rectifiers, and when they conduct, the output voltage drops towards dc. And when they're cut-off the output voltage rises. Therefore, the horizontal oscillator trigger (trig, W6) sends the retrace (comm. W6) into conduction and it remains in that state for 25 µs. During that interval, the trace SCR cuts off and stops conducting for about 10 μ s. The scope trace then shows that the commutator SCR does not conduct for some 38 µs, making a total horizontal sweep time of 63.5 μ s. The trace SCR (and diode) conducts for a total of some 53 µs.

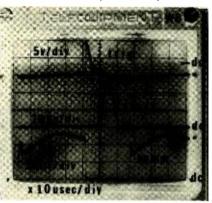
Chroma circuits

Chroma circuits are no more difficult to analyse than luminance and sync circuits, but you may not be used to the clean test patterns on some of the better sets. In these circuits the bandpass amplifiers, burst, 3.579545 mHz subcarrier oscillator, and the chroma-demodulated output are all needed to complete the analysis. So with the preset composite video signal following the video detector, the task shouldn't be that difficult. Deviations at this point, however, means there are specific problems in the receiver and they should be attended to before continuing.

Chroma and demodulator outputs should be examined first, if there is no color but good black and white. In most integrated circuit receivers, luminance information is added either in the demodulator chip itself (Fig. 1), or directly into the chroma output

The National Fire Protection Association adopted the revised and corrected 1975 National Electrical Code as its standard at its meeting in Miami last Spring. The new code's publishing date is September, replacing the present 1971 edition.

The new edition contains some significant changes, relaxing provisions of the old Code in some places and tightening them in others. Thus Section 336-3 (Nonmetallic Sheathed Cable) now amplifiers. The reasoning here is to combine luminance information and chroma (color) information before the picture tube so both signals can have identical impedances, proper ac and dc levels, and be routed to the picture tube through one set of electrodes. However, you may not see the red and blue amplifier outputs dis-





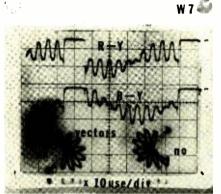


FIG. 8—R-Y AND B-Y OUTPUT and vector patterns.



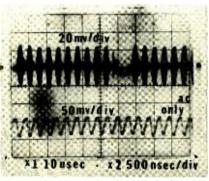


FIG. 9—CHROMA IC AMPLIFIER OUTPUT and subcarrier sinewave.

NEW ELECTRICAL CODE ADOPTED

permits types NM and NMC cable to be used in certain types of dwelling and other structures, and Sections 230-208 and 240-100 (Services and Overcurrent Protection) deletes requirements pertaining to visual current indication. But Section 300-15b (Wiring Methods) limits the use of certain devices without separate boxes. In several sections, some requirements that had been applied only where voltages were over 600 are now general requirements. played as cleanly as those in Fig. 8 (R-YW6 and B-YW6) unless the luminance signal is shunted to ground with about an 80 pF capacitor.

Obviously, if you have such waveforms with the red zero reference voltage at bar six, and the blue zero reference voltages at bars three and nine; and plenty of amplitude, your chroma sections are operating well. The two 11- μ S rectangular pulses cut off the pix tube during line retrace. Further confirmation of the chroma section comes from the two vector patterns in Fig. 8 (W6) although the right one is upside down and the scope's horizontal and vertical polarities must be reversed to turn it right side up (left vector).

If the chroma outputs are not satisfactory, backtrack to the bandpass amplifier and see if it has an output at least in the millivolt range in semiconductor sets, (Fig. 9, top trace) and in the volt range in hybrid sets. The bottom trace of Fig. 9 is the output of the 3.58-MHz oscillator viewed at 500 μ S/div. If either the color information or the subcarrier reference is missing or is off frequency, then there is no demodulation and no color. **R-E**

R-E's Substitution guide for replacement transistors

PART XXI by ROBERT & ELIZABETH SCOTT

- ARCH—Indicates the Archer brand of semiconductors sold only by Radio Shack and Allied Radio Stores. Allied Radio Shack, 2725 W. 7th St., Ft. Worth, Texas 76107
- DM—D. M. Semiconductor Co., P.O. Box 131, Melrose, Mass. 02176
- G-E-General Electric Co., Tube Product Div., Owensboro, Ky. 42301
- ICC--International Components, 10 Daniel Street, Farmingdale, N.Y. 11735
- IR—International Rectifier, Semiconductor Div., 233 Kansas St., El Segundo, Calif. 90245
- MAL—Mallory Distributor Products Co., 101 S. Parker, Indianapolis, Ind. 46201
- MOT—Motorola Semiconductors, Box 2963, Phoenix, Ariz. 85036
- RCA—RCA Electronic Components, Harrison, N.J. 07029
- SPR—Sprague Products Co., 65 Marshall St., North Adams, Mass. 01247
- SYL—Sylvania Electric Corp., 100 1st Ave., Waltham, Mass. 02154 WOR—Workman Electronic Products. Inc.,
- WOR—Workman Electronic Products, Inc., Box 3828, Sarasota, Fla. 33578
- ZEN-Zenith Sales Co., 5600 W. Jarvis Ave., Chicago, III. 60648

Radio-Electronics has done its utmost to insure that the listings in this directory are as accurate and reliable as possible; however, no responsibility is assumed by Radio-Electronics for its use. We have used the latest manufacturers material available to us and have asked each manufacturer covered in the listing to check its accuracy. Where we have been supplied with corrections, we have updated the listing to include them. The first part of this Guide appeared in March 1973.

	ARCH	DM	G-E	ICC	IR	MAL	мот	RCA	SPR	SYL	WOR	ZEN
2N4348 2N4349 2N4350 2N4352 2N4354	NA NA NA RS276-2021	T-707 TS-3020 TS-3001 T-803 T-708	NA GE-28 GE-28 NA GE-67	ICC-707 ICC-S3020 ICC-S3001 ICC-803 ICC-708	IRTR-61 NA NA NA TR-19	PTC 118 PTC 144 NA NA PTC 127	HEP-707 HEP-S3020 HEP-S3001 HEP-803 HEP-708	SK 3079 NA NA SK 3025	NA NA NA RT-115	NA NA NA ECG 159	WEP-707 WEP-S3020 NA NA WEP-717	PEN 204 NA NA NA NA
2N4355 2N4356 2N4359 2N4360 2N4381	RS276-2021 RS276-2021 NA NA NA	T-708 T-708 TS-0006 TF-1035 T-803	GE-67 GE-21 GE-67 NA NA	ICC-708 ICC-708 ICC-S0006 ICC-F1035 ICC-803	NA NA NA NA	PTC 127 PTC 103 PTC 127 NA NA	HEP-708 HEP-708 HEP-S0006 HEP-F1035 HEP-803	SK 3114 SK 3114 NA NA NA	RT-115 RT-115 NA NA NA	EGC 159 ECG 159 NA NA NA	WEP-717 WEP-717 WEP-717 NA NA	NA NA NA NA
2N4382 2N4383 2N4385 2N4386 2N4387	NA NA NA NA RS276-2025	T-803 TS-3026 TS-3026 NA T-702	NA NA GE-63 GE-63 GE-69	ICC-803 ICC-S3026 ICC-S3026 NA ICC-702	NA NA NA NA IRTR-58	NA NA NA PTC 136 PTC 113	HEP-803 HEP-S3026 HEP-S3026 NA HEP-702	NA NA NA NA SK 3083	NA NA NA RT-133	NA NA NA ECG 153	NA WEP-3023 WEP-3023 WEP-3020 WEP-700	NA NA NA NA
2N4388 2N4389 2N4390 2N4395 2N4296	RS276-2025 NA NA NA NA NA	T-702 T-57 T-713 T-247 T-247	GE-69 NA GE-27 GE-19 GE-19	ICC-702 ICC-57 ICC-713 ICC-247 ICC-247	IRTR-58 IRTR-54 IRTR-87 IRTR-59 IRTR-59	PTC 113 PTC 103 PTC 117 PTC 119 PTC 119	HEP-702 HEP-57 HEP-713 HEP-247 HEP-247	SK 3083 SK 3118 NA SK 3027 SK 3027	RT-133 RT-126 NA RT-131 RT-131	ECG 153 ECG 106 NA ECG 130 ECG 130	WEP-700 WEP-52 WEP-53 WEP-247 WEP-247	NA NA NA NA NA
2N4399 2N4400 2N4401 2N4402 2N4403	NA RS276-2009 RS276-2009 RS276-2021 RS276-2021	TS-7001 T-736 T-736 T-716 T-716 T-716	NA GE-20 GE-20 GE-21 GE-21	ICC-S001 ICC-736 ICC-736 ICC-716 ICC-716	TR-20 TR-21 TR-21 IRTR-54 IRTR-54	NA PTC 123 PTC 136 PTC 103 PTC 103	HEP-S7001 HEP-736 HEP-736 HEP-716 HEP-716	NA SK 3122 SK 3122 SK 3114 SK 3025	RT-148 RT-102 RT-102 RT-115 RT-115	ECG 180 ECG 123A ECG 123A ECG 159 ECG 159	WEP-ŴS7001 WEP-735 WEP-735 WEP-717 WEP .717	NA ZEN 120 ZEN 120 ZEN 107 ZEN 107
2N4404 2N4405 2N4406 2N4407 2N4409	NA NA NA NA RS276-2008	TS-3031 TS-3031 TS-3003 TS-3031 TS-0001	NA NA NA GE-18	ICC-S3031 ICC-S3031 ICC-S3003 ICC-S3021 ICC-S0001	IRTR-73 IRTR-88 IRTR-88 IRTR-88 IRTR-87	PTC 141 PTC 141 PTC 141 PTC 141 PTC 141 PTC 123	HEP-S3031 HEP-S3031 HEP-S3003 HEP-S3031 HEP-S0001	SK 3025 SK 3025 SK 3025 SK 3025 NA	RT-115 RT-115 RT-115 RT-115 RT-114	ECG 129 ECG 129 ECG 129 ECG 129 ECG 129 NA	WEP-242 WEP-242 WEP-242 WEP-242 WEP-712	NA NA NA TEN 125
2N4410 2N4411 2N4412 2N4413 2N4414	RS276-2008 NA NA NA NA	TS-0001 T-52 T-51 T-716 T-51	GE-18 NA GE-67 GE-67 GE-67	ICC-S0001 ICC-52 ICC-51 ICC-716 ICC-51	IRTR-87 TR-20 IRTR-88 TR-20 IRTR-88	PTC 123 PTC 103 PTC 103 PTC 103 PTC 103 PTC 103	HEP-S0001 HEP-52 HEP-51 HEP-716 HEP-51	SK 3045 SK 3114 SK 3025 SK 3114 SK 3025	RT-110 RT-115 RT-115 RT-115 RT-115	ECG 154 ECG 159 ECG 129 ECG 159 ECG 129	WEP-712 WEP-717 WEP-242 WEP-717 WEP-242	ZEN 125 NA ZEN 101 ZEN 107 ZEN 101
2N4415 2N4416 2N4417 2N4418 2N4419	NA NA NA NA	T-716 T-802 T-801 TS-0004 T-50	GE-67 GE-FET-2 GE-FET-2 GE-20 GE-20 GE-20	ICC-716 ICC-802 NA ICC-S0004 ICC-50	TR-20 NA NA NA TR-21	PTC 103 PTC 151 PTC 152 PTC 133 PTC 136	HEP-716 HEP-802 NA HEP-S0004 HEP-50	SK 3114 SK 3112 SK 3112 SK 3039 SK 3039	RT-115 RT-176 RT-176 RT-113 RT-113	ECG 159 ECG 133 ECG 133 ECG 108 ECG 108	WEP-717 WEP-801 WEP-801 WEP-56 WEP-56	Z EN 107 Z EN 123 NA Z EN 127 Z EN 100
2N4420 2N4421 2N4422 2N4423 2N4423 2N4424	NA NA NA NA	T-734 T-50 T/734 NA T-736	GE-20 GE-20 GE-20 GE-21 GE-20	ICC-734 ICC/50 ICC-734 ICC-52 ICC-736	IRTR-24 TR-21 IRTR-24 NA TR-21	PTC 136 PTC 136 PTC 136 NA PTC 123	HEP-734 NA	NA SK 3039 NA NA SK 3124	RT-113 RT-115	NA NA NA ECG 123A	WEP-723 WEP-50 WEP-723 WEP-717 WEP-735	2 EN 118 2 EN 100 2 EN 118 NA 2 EN 120
2N4425 2N4427 2N4428 2N4429 2N4430	NA NA NA NA	ts-3024 TS-3008 TS-3001 NA NA	GE-20 GE-18 GE-28 GE-28 GE-28	ICC-S3024 ICC-S3003 ICC-S3001 NA NA	NA IRTR-87 NA NA NA	PTC 123 PTC 143 NA NA NA	HEP-S3024 HEP-S3008 HEP-S3001 NA NA	SK 3024	RT-102 RT-114 RT-154 RT-154 RT-154	ECG 192 ECG 128 NA NA NA	WEP-735 WEP-243 NA NA NA	NA NA NA NA
2N4432 2N4433 2N4434 2N4435 2N4435 2N4436	NA RS276-2009 NA NA NA	T-736 T-734 T-709 T-709 T-736	NA GE-61 GE-17 GE-17 GE-20	ICC-736 ICC-734 ICC-709 ICC-709 ICC-736	NA TR-24 TR-21 IRTR-65 TR-21	PTC 123 PTC 132 PTC 132 PTC 132 PTC 132 PTC 123	HEP-734 HEP-709 HEP-709	SK 3018 SK 3117	RT-113	ECG 123A ECG 107 ECG 161 ECG 161 ECG 123A	WEP-735 WEP-720 WEP-719 WEP-719 WEP-735	21:N 120 21:N 118 22:N 105 21:N 105 21:N 105 21:N 120
2N4437 2N4440 2N4441 2N4442 2N4443	NA NA NA NA	T-736 NA SR-1220 SR-1221 SR-1222	GE-20 GE-28 GEMR-4 GEMR-4 GEMR-4	ICC-736 NA ICC-R1220 ICC-R1221 ICC-R1222	TR-21 IRTR-55 NA NA NA	PTC 136 NA NA NA NA	HEP-736 NA HEP-R1220 HEP-R1221 HEP-R1222	NA	RT-102 RT-154 NA NA NA	ECG 123A NA ECG 5442 ECG 5444 ECG 5446	NA NA NA	ZIIN 120 NA NA NA NA
2N4444 2N4449 2N4450 2N4451 2N4452	NA NA NA NA	SR-1223 T-50 TS-0004 T-715 T-716	NA NA NA NA	ICC-R1223 ICC-50 ICC-S0004 ICC-715 ICC-716	NA NA NA NA	NA PTC 133 PTC 136 PTC 127 PTC 103	HEP-S0004 HEP-715	SK 3039	RT-102 RT-126	ECG 5448 ECG 108 ECG 123A ECG 106 ECG 159	NA WEP-56 WEP-735 WEP-52 WEP-717	NA ZE N 100 ZE N 127 ZE N 106 ZE N 107
2N4453 2N4851 2N4852 2N4853 2N4854	RS276-2029	T-76 T-310 T-310 T-310 t-241	NA NA NA NA	ICC-76 ICC-310 ICC-310 ICC-310 ICC-241	NA NA NA NA	PTC 127 NA NA NA NA	HEP-76 HEP-310 HEP-310 HEP-310 HEP-241	SK 3118 NA NA NA NA	RT-126 NA NA NA NA	ECG 106 NA NA NA NA	WEP-52 WEP-310 WEP-310 WEP-310 WEP-241	NA ZEN 129 ZEN 129 ZEN 129 NA
2N4867 2N4868 2N4869 2N4870 2N4871	NA NA NA RS276-2029 RS276-2029	NA NA NA T-310 T-310	GE-FET-1 GE-FET-1 GE-FET-1 NA NA	NA NA NA ICC-310 ICC-310	NA NA NA NA	PTC 152 PTC 152 PTC 152 NA NA	NA NA	SK 3112	RT-176 RT-176 RT-176 NA NA		WEP-801 WEP-801 WEP-801 WEP-310 WEP-310	NA NA ZEN 129 ZEN 129
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NA=NOT APPLICABLE

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NOVEMBER 1974

	ARCH	DM	G-E	ICC	IR	MAL	. мот	RCA	A SPF	R SYL	WOR	ZEN
2N4872 2N4873 2N4874 2N4875 2N4876	NA NA NA NA	T-52 TS-0004 TS-3008 TS-3008 TS-3008	NA NA NA NA	ICC-52 ICC-S0004 ICC-S3008 ICC-S3008 ICC-S3008	NA NA NA NA	PTC 143	HEP-S3008	NA NA	RT-126 RT-113 NA NA NA	ECG 106 ECG 108 NA NA NA	WEP-52 WEP-56 NA NA NA	NA ZEN 127 NA NA NA
2N4877 2N4878* 2N4879* 2N4880* 2N4890	NA NA NA NA	TS-3010 T-738 TS-0007 T-729 T-708	GE-66 NA NA NA GE-67	ICC-S3010 ICC-738 ICC-S0007 ICC-729 ICC-708	NA NA NA NA	NA PTC 123 PTC 144 PTC 121 PTC 141	HEP-S3010 HEP-738 HEP-S0007 HEP-729 HEP-708	NA	RT-150 RT-109 NA RT-109 RT-115	NA NA NA ECG 129	NA WEP-728 WEP-712 WEP-729 WEP-242	ZEN 207 ZEN 121 NA ZEN 115 NA
2N4891 2N4892 2N4893 2N4894 2N4898	NA NA NA NA RS276-2025	T-310 T-310 T-310 T-310 T-702	NA NA NA GE-69	ICC-310 ICC-310 ICC-310 ICC-310 ICC-702	NA NA NA IRTR-58	NA NA NA PTC 113	HEP-310 HEP-310 HEP-310 HEP-310 HEP-702	NA NA NA SK 3083	NA NA NA NA RT-133	NA NA NA ECG 218	WEP-310 WEP-310 WEP-310 WEP-310 WEP-700	ZEN 129 ZEN 129 ZEN 129 ZEN 129 ZEN 129 NA
2N4899 2N4900 2N4901 2N4902 2N4903	RS276-2025 RS276-2025 RS276-2027 NA NA	T-702 T-702 T-705 T-248 TS-5005	GE-69 NA NA NA NA	ICC-702 ICC-702 ICC-705 ICC-248 ICC-S5005	IRTR-58 IRTR-58 TR-29 TR-29 NA	PTC 113 PTC 113 NA NA NA	HEP-702 HEP-702 HEP-705 HEP-248 HEP-S5005	SK 3083 NA NA NA NA	RT-133 RT-133 NA NA NA	ECG 218 ECG 218 NA NA NA	WEP-700 WEP-700 WEP-S7001 WEP-S7001 WEP-S5005	NA NA NA NA
2N4904 2N4905 2N4906 2N4907 2N4908	RS276-2027 NA NA NA NA NA	T-705 T-248 T-248 T-248 T-248 T-248	NA NA NA NA	ICC-705 ICC-248 ICC-248 ICC-248 ICC-248	TR-29 TR-29 NA NA NA	NA NA NA NA	HEP-705 HEP-248 HEP-248 HEP-248 HEP-248	NA NA NA NA	NA NA NA NA	NA NA NA NA	WEP-S7001 WEP-S7001 WEP-S7001 WEP-S7001 WEP-S7001	NA NA NA NA
2N4909 2N4910 2N4911 2N4912 2N4913	NA RS276-2017 RS276-2017 RS276-2017 NA	TS-5005 T-703 T-703 T-703 T-247	NA GE-66 GE-66 GE-32 GE-19	ICC-S5005 ICC-703 ICC-703 ICC-703 ICC-247	NA NA NA NA TR-59	NA PTC 112 PTC 112 PTC 112 PTC 112 PTC 118	HEP-S5005 HEP-703 HEP-703 HEP-703 HEP-247	NA SK 3131 SK 3131 SK 3131 SK 3027	NA RT-150 RT-150 RT-150 RT-131	NA ECG 175 ECG 175 ECG 175 ECG 130	WEP-S5005 WEP-241 WEP-241 WEP-241 WEP-247	NA NA NA NA
2N4914 2N4915 2N4916 2N4917 2N4918	NA NA RS276-2023 RS276-2023 RS276-2027	T-247 T-247 T-52 T-52 T-700	GE-19 GE-14 GE-22 GE-21 GE-29	ICC-247 ICC-247 ICC-52 ICC-52 ICC-700	TR-59 NA TR-20 NA NA	PTC 118 PTC 118 PTC 103 PTC 103 NA	HEP-247 HEP-247 HEP-52 HEP-52 HEP-700	SK 3027 SK 3027 SK 3025 SK3114 NA	RT-131 RT-131 RT-115 RT-115 RT-153	ECG 130 ECG 130 ECG 159 ECG 159 ECG 185	WEP-247 WEP-247 WEP-717 WEP-717 WEP-WS5007	NA NA NA NA
2N4919 2N4920 2N4921 2N4922 2N4923	RS276-2026 NA RS276-2018 RS276-2018 RS276-2018	T-246 TS-5006 T-245 T-245 T-245 T-245	GE-29 GE-69 GE-28 GE-28 GE-28	ICC-246 ICC-S5006 ICC-245 ICC-245 ICC-245	IRTR-77 NA NA NA NA	NA NA PTC 110 PTC 110 PTC 110	HEP-246 HEP-S5006 HEP-245 HEP-245 HEP-245	NA NA NA SK 3054 NA	RT-153 RT-153 RT-152 RT-152 RT-152	ECG 185 ECG 185 ECG 184 ECG 184 ECG 184	WEP-WS5007 WEP-WS5007 WEP-WS5003 WEP-WS5003 WEP-WS5003	NA ZEN 202 ZEN 202
2N4924 2N4925 2N4926 2N4927 2N4928	NA NA NA NA	T-713 T-712 T-712 T-712 T-712 T-710	GE-27 GE-32 GE-27 GE-27 NA	ICC-713 ICC-712 ICC-712 ICC-712 ICC-712 NA	NA IRTR-78 IRTR-78 IRTR-78 IRTR-88	PTC 144 PTC 117 PTC 117 PTC 117 PTC 117 PTC 127	HEP-713 HEP-712 HEP-712 HEP-712 NA	SK 3045 SK 3045 SK 3045 SK 3045 SK 3025	RT-110 RT-110 RT-110 RT-110 RT-115	ECG 154 ECG 154 ECG 154 ECG 154 ECG 129	WEP-712 WEP-712 WEP-712 WEP-712 WEP-242	NA ZEN 205 ZEN 205 ZEN 205 NA
2N4932 2N4934 2N4935 2N4936 2N4937*	NA RS276-2011 RS276-2011 NA NA	NA T-56 T-56 T-56 T-715	NA NA NA GE-21	NA ICC-56 ICC-56 ICC-738 ICC-715	NA IRTR-66 NA NA NA	PTC 128 PTC 133 PTC 133 PTC 133 PTC 133 PTC 127	NA HEP-56 HEP-56 NA HEP-715	NA SK 3039 SK 3039 SK 3039 NA	NA RT-113 RT-113 RT-113 RT-115	NA ECG 108 ECG 108 ECG 108 NA	NA WEP-56 WEP-56 WEP-56 WEP-715	NA ZEN 104 ZEN 104 ZEN 121 ZEN 106
2N4938* 2N4939* 2N4940* 2N4941* 2N4942*	NA NA NA NA	T-715 T-715 T-715 T-715 T-715 T-715	GE-21 NA GE-21 GE-21 NA	ICC-715 ICC-715 ICC-715 ICC-715 ICC-715 ICC-715	NA NA NA NA	PTC 127 PTC 127 PTC 127 PTC 127 PTC 127 PTC 127	HEP-715 HEP-715 HEP-715 HEP-715 HEP-715	NA NA NA NA	RT-115 RT-115 RT-115 RT-115 RT-115 RT-115	NA NA NA NA	WEP-715 WEP-715 WEP-715 WEP-715 WEP-715	ZEN 106 ZEN 106 ZEN 106 ZEN 106 ZEN 106
2N4943 2N4944 2N4945 2N4946 2N4948	NA NA NA NA	T-714 T-714 T-714 T-714 T-714 T-310	NA GE-20 GE-18 GE-20 NA	ICC-714 NA NA ICC-714 ICC-310	IRTR-87 IRTR-87 IRTR-87 IRTR-87 NA	PTC 144 PTC 123 PTC 123 PTC 123 NA	HEP-714 NA NA HEP-714 HEP-310	SK 3024 SK 3024 SK 3024 SK 3024 NA	RT-114 RT-114 RT-114 RT-114 NA	ECG 128 ECG 128 ECG 128 ECG 128 ECG 128 NA	WEP-243 WEP-243 WEP-243 WEP-243 WEP-310	NA NA NA ZEN 129
2N4949 2N4950 2N4951 2N4952 2N4953	NA NA NA NA	T-310 NA TS-0004 TS-0004 T-736	NA GE-20 GE-20 GE-20 GE-10	ICC-310 NA ICC-S0004 ICC-S0004 ICC-736	NA NA NA TR-2		HEP-310 NA HEP-S0004 HEP-S0004 HEP-736	NA NA SK 3124 SK 3124 SK 3124	RT-102	NA NA ECG 123A ECG 123A ECG 123A	WEP-310 NA WEP-735 WEP-735 WEP-735	ZEN 129 NA ZEN 127 ZEN 127 ZEN 127 ZEN 120
2N4954 2N4955 2N4956* 2N4960 2N4961 *Indicate	NA NA NA NA NA es a dual transis	TS-0004 T-737 T-724 TS-3001 TS-3002	NA	ICC-S0004 ICC-737 ICC-724 ICC-S3001 ICC-S3002		NA PTC 121 PTC 123 PTC 123	HEP-737 HEP-724 HEP-S3001 HEP-S3002	SK3024 SK 3024	RT-109 RT-105 RT-114 RT-114	ECG 123A NA ECG 128 ECG 128	WEP-243 WEP-243	ZEN 127 NA ZEN 112 NA NA

*Indicates a dual transistor for high-speed switching, diff amplifier etc. Likely to be a matched pair. Use two of the type specified, matching when necessary, on a curve tracer or lab-type transistor checker.

NA=NOT AVAILABLE

(continued next month)

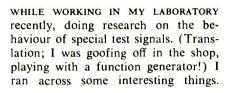
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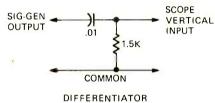
RE's Service Clinic

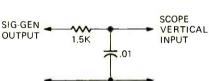
RC networks and different waveforms

The effects are weird if you don't know what to expect

> by JACK DARR SERVICE EDITOR





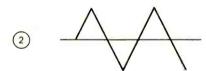


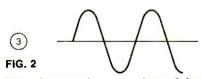
COMMON INTEGRATOR

f≈3kHz









They interested me, anyhow. I knew that you'd change a waveform if you fed it through an R-C network. However, I got one result that wiped me out. After a lot of digging, I found out why. See if you can predict the results, and then explain 'em.

I used the three standard signals

from a function generator; sine, square and triangular waveforms. I feel these through the two stock R-C network hook-ups; a differentiator and an integrator. A quick look at the schematic of any kind of electronic equipment will show you lots of these things.

Figure 1 shows the circuits used. Look at these. Now, draw your idea of what the *output* waveform looks like, and see if you can explain it. After you get through, read cn and see what I actually got, and my idea of why. Have fun!

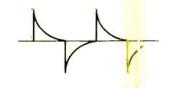
The answers.

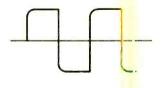
Figure 2 shows the inputs to the differentiator circuit and the output waveforms I saw on the scope

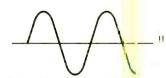
1. Almost everybody should get this one, or get close. The differentiator makes a spike waveform from a square wave. This is used in mary pulse generator circuits.

DIFFERENTIATOR

OUTPUT







2. This one fooled me. However, you can see what happened. The time constant is long enough so that the capacitor reaches full charge. So, it rounds off the leading edge of the square wave.

3. This is the wipe-out. What happended? Nothing. Output wave form

This column is for your service problems—TV, radio, audio or general and industrial electronics. We answer all questions individually by mail, free of charge and the more interesting ones will be printed here.

If you're really stuck, write us. We'll do our best to help you. Don't forget to enclose a stamped, self-addressed envelope. If return postage is not included, we cannot process your question. Write: Service Editor, Radio-Electronics, 200 Park Ave. South, N.Y. 10003.

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exactly the same as the input! We'll explain that in a minute. Go on to Figure 3. This is the integrator.

4. Surprise! An integrator makes a triangular wave out of a square wave. This is used in function generators to develop a triangular wave.

5. Look at this one. Integrating a triangular wave makes a *sinewave*. Another method used in function generators, although theirs is much

more elaborate.

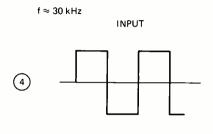
6. Here we go again. Nothing happens, just as before.

Wha' Hoppen?

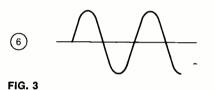
INTEGRATOR

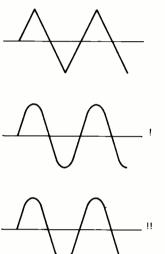
How come this reaction? Frankly, I expected to see a change in waveform in all of them. When the sinewave came through undisturbed, I couldn't believe it. Back to the books. Here is the best explanation I could

OUTPUT









find, after quite a bit of digging around.

As briefly as possible, both square and triangular waves can be considered as being made up of innumerable harmonics! The charging of the capacitor and the action of the resistor affects these; the waveform is distorted, although its fundamental frequency is still the same.

The really odd effect is the reaction on the sinewave. Why doesn't the R-C network upset it, as it does all others? Here's what they say.

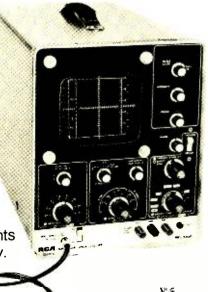
A sinewave, especially one with very low distortion, is considered as a "pure signal." That is, it's *not* made up of harmonics, but is just a single frequency, theoretically *without* any harmonics at all! So, you'll see practically no effect on the waveform. Most of what you will see will be only a small loss in amplitude.

You can try this yourself, with any audio signal generator and scope. It's fascinating. Try different values for R and C, and different frequencies. If you don't have a square-wave signal generator, feed the sinewave output into a pair of low-voltage Zeners, tied in parallel and reversed. This will make a fair square wave. You can get the triangle by feeding the square wave into a separate integrator, and then feeding the resultant into another R-C network. (continued on page 72)

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- Constants, Standards, Conversion: International System of Units (SI); Physical and Electrical Conversion Factors; Electronic Constants, Multiples, and Sub-Multiples; others.
- Symbols, Components, Codes: Electronic Circuit and Component Symbols; Summary of Resistor Types; Diode Symbols, Characteristics and Applications; Coaxial Cable Types and Sizes; others.
- IV. Mathematics, Mechanics, Charts: Computer Number Codes; Number Functions; Powers of Numbers; Four Place Log Tables; Twist Drill Sizes; others.
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Circle 19 on reader service card

SERVICE CLINIC (continued from page 70)

reader questions

THE "REGAUSSING" COIL

Originally, this Motorola TS-914 chassis came in with the circuitbreaker tripping. Replaced a bad diode in the voltage-doubler-no help. The resistor in parallel with the degausser coil was open and I replaced it. When I turned the set on, there was a spark from somewhere. After this the breaker didn't trip any more.

The purity is lousy. The best I can get is a 12-inch red circle in the middle with blotches around the edge. I cooked it for 6 hours. While this was going on, I noticed that the purity began to get worse around the edges. Manual degaussing will clear it up, but it comes back in a few hours.

I'm at a loss. HELP!-D.S. Oregon, OH.

The trouble is in the auto degausser circuit. It is obviously "re-gaussing" the tube! In this chassis, the most likely suspect would be the thermal degaussing switch. This *could* have been where your arc was. If the points have welded, this leaves the coil in-circuit all the time, and this *causes* impurity.

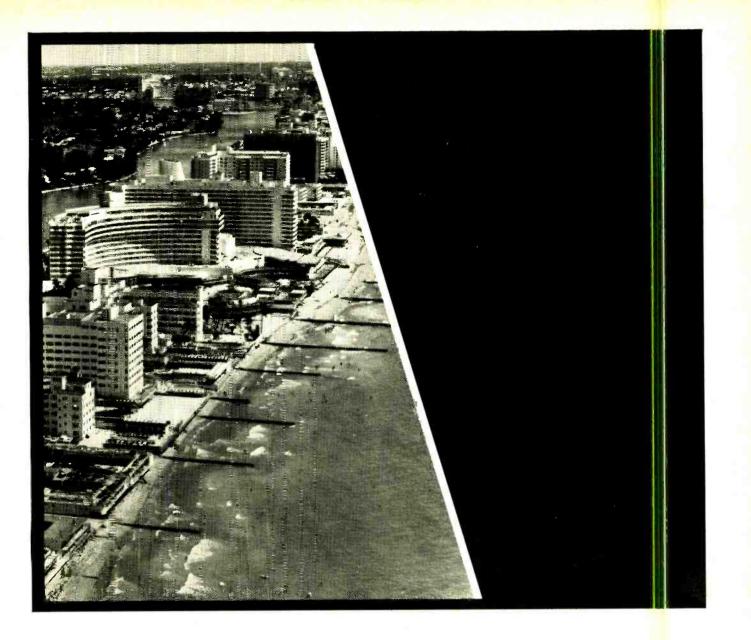
NO SNOW, THAT'S BAD

This Sylvania DO3 has been pretty well overhauled; tuner, new filters and so on. I'm still not happy with it. The agc control doesn't have the proper effect. Also, I have no snow on unused channels, nor with the antenna off. Distant stations won't come in, though the owner says they used to. Colors aren't good, even on local stations. What do you think?-R.D., Panama City, FL.

I think you're "losing it," somewhere. This set obviously doesn't have enough gain. The no-snow symptom is almost always an indication of very poor rf or i.f. gain. This could be due to one of two things.

Excessive negative agc voltage could be holding the gain down. This is the easy one. Clamp the agc to +18 volts. If this sounds funny in a tube set, remember that the 1st i.f. cathode is +21 volts above ground so that the actual agc bias on the tube is a -3volts. If this brings the snow and the colors back, check out the dc voltages (continued on page 78)

www.amencanradiohistory.com



Our town



Miami Beach visitors come to "our town" to stay at the famous ocean front hotels and enjoy the temperate southern climate. And when these vacationers visit the lively Miami Beach nightclubs and show rooms, ther want to hear the entertainers as well as see them perform. That's why sound technicians at most of the leading hotels "on the beach" rely on Shure microphones and Vocal Master Sound Systems for top performance and dependability. From a top show at a famous hotel to a huge political convention, Shure provides the sound Miami Beach professionals prefer.

Shure Brothers Inc. 222 Hartrey Ave., Evanston, III. 60204 In Canada: A. C. Simmonds & Sons Limited Circle 20 on reader service card



C. Martine

CIE graduate builds two-way radio service business into \$1,000,000 electronics company!

How about YOU? Growth of two-way transmitters creates demand for new servicemen, field and system troubleshooters. Licensed experts can make big money. Be your own boss, build your own company. And you don't need a college education.

Two-way radio is booming. There are already nearly seven million two-way transmitters for police cars, fire department vehicles, taxis, trucks, boats, planes, etc., and Citizens Band uses. And the number keeps growing by the thousands every month. Who is going to service them? You can — if you've got the know-how!

Why You'll Earn Top Pay

One reason is that the United States Government doesn't permit anyone to service two-way radio systems unless he's *licensed* by the FCC (Federal Communications Commission).

Another reason is that when two-way radio men are needed, they're *really* needed! A two-way radio *user* must keep those transmitters operating at all times. And, they *must* have their frequency modulation and plate power input checked at regular intervals by licensed personnel to meet FCC requirements.

As a licensed man, working by the hour, you would usually charge at least \$5.00 per hour, \$7.50 on evenings and Sundays, plus travel expenses.

Or you could set up a regular monthly retainer fee with each customer. Your fixed charge might be \$20 a month for the base station and \$7.50 for each mobile station. Studies show that one man can easily maintain at least 135 stations—averaging 15 base stations with 120 mobiles! This would add up to at least \$12,000 a year.



Edward J. Dulaney, Scottsbluff, Nebraska, (above and at right) earned his CIE Diploma in 1961, got his FCC License and moved from TV repairman to lab technician to radio station Chief Engineer. He then founded his own two-way radio business. Now, Mr. Dulaney is also President of D & A Manufacturing, Inc., a \$1,000,000 company building and distributing two-way radio equipment of his own design. Several of his 25 employees are taking CIE courses. He says: "While studying with CIE, I learned the electronics theories that made my present business possible."

Be Your Own Boss

There are other advantages, too. You can become your own boss — work entirely by yourself or gradually build your own fully staffed service company. Of course, we can't promise that you will be as successful as Ed Dulaney, or guarantee that you'll establish a successful two-way radio business of your own, but the opportunities for success are available to qualified, licensed men in this expanding field.

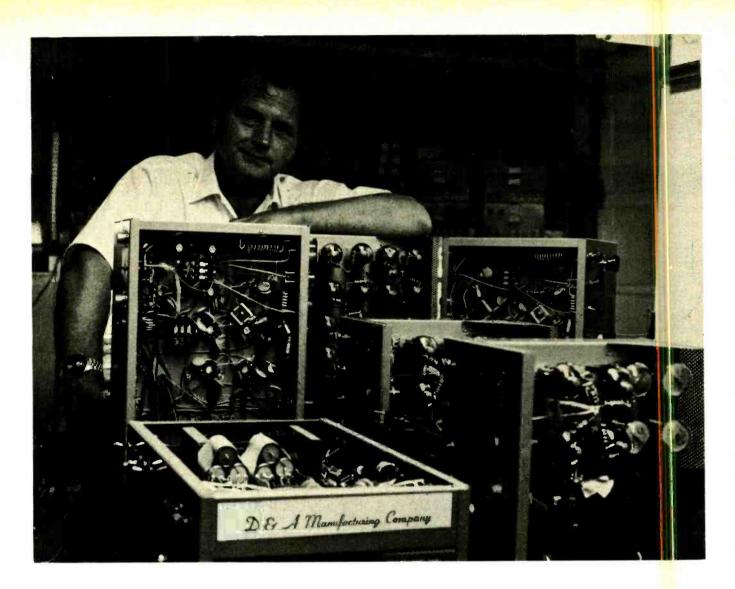
How To Get Started

How do you break in? This is probably the best way:

- 1. Without quitting your present job, learn enough about electronics fundamentals to pass the Government FCC exam and get your Commercial FCC License.
- 2. Then get a job in a two-way radio service shop and "learn the ropes" of the business.
- 3. As soon as you've earned a reputation as an expert, there are several ways you can go. You can move out and start signing up and servicing your own customers. You might become a franchised service representative of a big manufacturer and then start getting into two-way radio sales.

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You Get Your FCC License... or Your Money Back!

By the time you've finished your CIE course, you'll be able to pass the FCC License exam. A recent survey of 787 CIE graduates reveals that better than 9 out of 10 CIE grads passed the FCC License exam. That's why we can offer our famous Money-Back Warranty: when you complete any CIE licensing course, you'll be able to pass your FCC exam or be entitled to a full refund of all tuition paid. This warranty is valid during the completion time allowed for your course. You get your FCC License – or your money back!

It's Up To You

Mail the reply card for two FREE books, "Succeed in Electronics" and "How To Get A Commercial FCC License." For your convenience, we will try to have a representative call. If card has been removed, mail coupon or write: Cleveland Institute of Electronics, Inc., 1776 E. 17th St., Cleveland, Ohio 44114.

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SERVICE CLINIC

(continued from page 72)

around the agc tube. Remember that the schematic voltages are read with no signal. These are all critical voltages.

Second possibility is a problem of low gain in either the rf amplifier or possibly the 1st or 2nd video i.f. stages. Check all dc voltages and the tubes, etc.

While you're there, check the 5.6megohm resistor from the rf agc terminal to +265 volts. This is supposed to provide a small positive voltage to keep the agc from going too far negative. If it's open, you'll often get the type of symptom you have.

G-E M110YBG HINT

On the G-E M110YBG and other SY chassis models, they use a copper strip bolted to the top front horizontal bar of the chassis as the ground for the Aquadag coating on the picture tube. If the Aquadag burns off or has poor contact here, it will arc. This will radiate and mess up the horizontal sync. Fix this ground. Use a spring, or another thin strip like that used to ground the tuner. I've done this on several of these sets.

Thanks very much to Paul Fleming of Dallas, Texas for this one. **R-E**

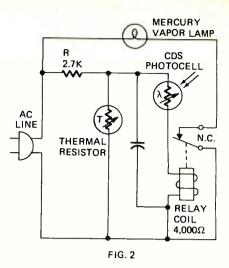
APPLIANCE CLINIC

(continued from page 24)

covered, this should read approximately 15,000 ohms or more. Now uncover the cell and let light hit it. The resistance should drop to somewhere around 1500 to 2000 ohms. The higher the intensity of the light, the lower the resistance. The relay should now close if power is applied to the unit. If it won't move, turn the power off and connect a jumper clip lead across the photocell. The armature should now close unless the coil has some shorted turns.

Figure 2 shows the schematic of a larger unit, used with the mercuryvapor lamps. Note the similarity. This one has a temperature-sensitive resistor mounted in shunt with the photocell and coil. Some units have a sensitivity control, so the lamp can be turned on at any desired level of outside light. (Some of these can be so sensitive that they turn on when the weather is fairly cloudy!)

The control unit in Fig. 1 is practically instantaneous. With the larger units in Fig. 2 and mercury-vapor lamps, there will be about one or two second delay. This isn't due to the control unit but rather the characteristics of a mercury-vapor lamp. These are actually "arc lamps," and it takes



a little time for the arc to form.

This delay will be almost impossible to notice during normal operation. However, during a violent thunderstorm with its associated bright flashes of lightning, you may notice the lamp going off. It may stay off for a moment, especially after a very bright flash. The photocells in this case are said to be temporarily "blocked". This is caused by very high-intensity light, just as human vision is temporarily blinded. This won't do any permanent damage, unless of course the unit takes a direct lightning hit. **R-E**

Here's everything you'd expect from a high-priced signal generator.

Except a high price.

Our new B&K Model 2050 Solid-state RF Signal Generator has features other companies charge much more for. Look at our specs: 100% Solidstate silicon circuitry with FET's in RF and audio oscillator stages. 6 bands with 1.5% accuracy from 100 kHz to 30 MHz. 3 outputs: RF, modulated RF (400 Hz), and externally modulated RF. Positive anti-backlash dial drive. Zener-regulated power supply. You needn't pay high prices for versatility, accuracy and reliability—now there's the Model 2050. And that's just what you'd expect from B&K.

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Very good equipment at a very good price. Dynascan Corporation. 1801 West Belle Plaine Avenue, Chicago, Illinois 60613

Here's everything you'd expect from a high-priced Hi-Low FET multimeter. Except a high price.

Introducing the B&K Model 290 solid-state FET Multimeter. Just by glancing at its specs, you can tell that the 290 is capable of more applications than any other multimeter in its class. 75 ranges. Hi-Lo power ohms ranges (low power only 33 mV). 15 megohms input impedance. A large 7"meter. 50 mV to 1500V full-scale sensitivity on both AC and DC. 50 micro-amp current range. Rx0.1 ohm range with 1 ohm center scale lets you measure low resistance down to .01 ohm. Circuit provides automatic overload protection with fuses and spark gaps. More multimeter for your money—that's



just what you expect from B&K. Contact your distributor, or write Dynascan Corporation. Model 290 Hi-Low FET Multimeter including Model PR-21 Probe: **\$15100**



Circle 23 on reader service card

Circle 22 on reader service card



NOVEMBER 1974

BUILD A PHOTOFLASH

(continued from page 37)

Series capacitor bank forming operation

Plug in the ac power line and turn the power switch to on. Before triggering the photoflash unit, allow the unit to charge for no less than three hours, overnight is even better.

After the minimum charging period, or overnight, attach a camera sync cord to the camera sync socket and with a pin or small piece of wire, short the end terminals to trigger the flash. Then allow 3 to 7 seconds for the recycle power to build-up. Then re-trigger the unit for approximately 30 flashes. The combination of 3 hour charge and repeated flashing will complete the forming operation and the flash unit will be ready to use with your camera.

Always trigger your flash unit several times before beginning to take pictures to assure maximum power output. Unused units will gradually de-form with age, and it is recommended that the forming operation be followed once every two to three months for better operation and to extend the life of the capacitors.



1 — Smooth working, machined mating parts that can never jump out . . . both the tongue and grooves are undercut. CHANNELLOCK imitators can't say this.

2—Patented reinforcing flange that eliminates stress breakage. Again, CHANNELLOCK imitators can't say this.

Be sure you get the genuine CHANNELLOCK. Look for the trade mark on the handle.

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Circle 25 on reader service card

Operation

Bare-bulb operation, without a reflector, usually has a guide number of 30 for a 200 watt-second power output, and as high as 150 with reflector for ASA 25 film. Guide numbers are just that ... a guide to use as a starting point for proper exposure. I recommend running a test film of varied exposures and shutter speeds to determine the proper guide number for your type of use. This involves shooting a series of pictures on a good resolution film, one rated at ASA 30 to ASA 65. Bracket your exposures 4 stops up and 4 stops down from f-8 at a shutter speed of 1/100-second.

Always use a maximum shutter speed of 1/60th of a second for cameras with focal plane shutters since the photoflash triggers at X or zero-delay shutter setting.

Troubleshooting the photoflash unit.

If you have properly made the circuit boards and installed each component properly, there should be no difficulty encountered in operating the unit. Usually, during the initial forming operation, considerable heat will be radiated from R1, and the possibility of the fuse blowing exists. This can be caused by excessive leakage of capacitors C3 and C4 that will correct its-self after completing the forming operation. It can also be caused by connecting the polarity of the capacitors incorrectly. Should your fuse blow, check the capacitor polarity FIRST.

Should the flash tube fail to fire, remove the flash tube from it's socket and measure across the socket pins with a DC Voltmeter. The positive lead of the voltmeter to pin 2 and the negative lead to pin 4. It should measure 450 volts. Should you be unable to measure the voltage; turn off power switch, open top, and check the following:

c <mark>hec</mark> k l	Open fuse
check 2	Open R1
check 3	Incorrect polarity of capa-
	citors C3 and C4
check 4	Open or shorted D1, D2,
	D3
c <mark>he</mark> ck 5	Incorrect polarity of capa-
	citors C1 or C2
check 6	Open connection between
	power circuit and trigger
	circuit

For those who would like to construct a bare bulb electronic photoflash unit but would prefer to assemble a kit, there is a kit for the Uniflash barebulb photoflash produced by Mitchell Enterprises, P.O. Box 1372, San Francisco, CA. 94101. **R-E**

NEW IN DVM's

(continued from page 49)

COLD-CATHODE DISPLAY TUBES and other similar lamps indicate voltage, current and resistance measurements on the Heathkit model IM-102 31/2-digit dmm. Most voltage and current ranges have overrange capability and an overrange indicator is provided. Polarity of dc voltage and current is automatically detected and displayed. Decimal-point positioning is automatic on each range.

Dc voltage ranges are 200 mV, 2, 20, 200 and 1000 volts. Input impedance is greater than 100 megs on the first range, greater than 1000 megs on the second and 10 megs on the 20, 200 and 1000volt ranges. Accuracy is $\pm 0.2\%$ ± 1 digit. Overrange capability 20%-subject to overload protection limits. Resolution (200-mV range) is 100 µV.



Ac voltage ranges same as dc; input impedance is 1 megohm/150 pF. Overload protection 250 Vrms on lowest two ranges; 500 Vrms on the top three. Accuracy ranges from $\pm 0.75\% \pm 1$ digit to $\pm 1.5\% \pm 1$ digit.

Current ranges (dc and ac): 200 μ A,

2, 20 and 200 mA and 2 A. Accuracy $\pm 0.3\% \pm 1$ digit on dc, $\pm 1.0\% \pm 1$ digit on ac.

The IM-102 is $3 \times 7.9 \times 7$ in., 4 lbs. \$239.95.

AUTO-RANGING AND LOW-POWER OHMS are but two of the features of the Keithley model 168 dmm. The five functions give you the capability of measur-



ing 100 µV to 1000 Vdc, 100 µV to 500 Vac, 100 nA to 1 amp ac and dc and 100 milliohms to 20 megohms. Input resistance is 10 megs on dc and 9 megs shunted by 90 pF on ac.

The 168 may be powered by line voltage or rechargeable NiCad batteries when the model 1688 rechargeable batterv set is installed.

With this dmm, you can turn on a semiconductor junction to see if it is good; or measure resistance in-circuit without turning on associated semiconductors. The 1.8 volts across the test prods, in the HIGH-OHMS mode, is enough to turn on most semiconductors. In the LOW-OHMS mode, a maximum of 180 mV is applied to the circuit under test so semiconductors are not turned on

This dmm operates from 90-110, 105-125, 195-235 or 210-250 V, 50-60 Hz, 6 W. It is 31/2 x 91/4 x 103/4 in., 31/2 lbs. \$299, \$359 with rechargeable battery pack installed.

ONE-YEAR BATTERY LIFE from a standard 9-volt transistor battery and liquidcrystal display are two novel feaures of Danameter model 2000, a product of Dana Laboratories.



Voltage ranges (ac and dc) are 2, 20, 200 and 1 kV with 1 mV resolution. Input impedance is 10 megohins on dc and 2 megs shunted by 40 pF on ac. Accuracy is $\pm 0.5\%$ of reading +.05%of range on 2-volt dc range; ±:0 75% of reading +.05% of range on the remaining dc ranges.

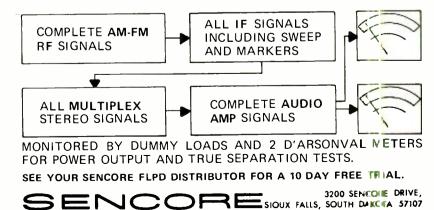
Direct current ranges are 20 #A, 200 mA and 2 A with 0.01 µA resolution. Resistances ranging from 20C cmms to 200 megohms are covered in four 100:1 ranges, Resolution is 0.1 oh 7. The Danameter 2000 is \$195. R-F

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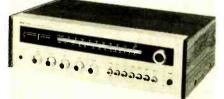
Circle 26 on reader service card

new products

More information on new products is available from the manufacturers of items identified by a Reader Service number. Use the Reader Service Card inside the back cover.

RECEIVER, model R36S features 30 watts per channel into 8 ohms, both channels driven from 20-20,000 Hz at less than 0.5% distortion. FM performance includes IHF sensitivity of 1.9 μ V, capture ratio of 2.5 dB and midband stereo separation of 35 dB minimum.

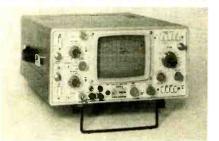
Operating features include channel selector, ganged bass, treble and volume controls, channel-balance control, switched loudness-



compensation, mono/stereo mode, tape monitor facilities, muting and high-frequency filter switches, speaker connections and switching for two sets of stereo speakers. Separate signal-strength and center-channel tuning meters are included. Rear panel features include choice of 300-ohm antenna strip or 72-ohm antenna jack, DIN jacks and multiple voltage selector for foreign operation, speaker fuses and extra accessory power outlets. Frequency response: 25-15,000 Hz. 5½ x 18 x 13 in.; 24 Ibs.; \$329.95.—H. H. **Scott, Inc.,** 111 Powdermill Road, Maynard, MA 01754.

Circle 31 on reader service card

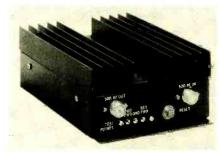
OSCILLOSCOPE, model 530A. Medium-band width, dual-trace portable scope features internal parallax-free 6 × 10 cm CRT graticule, 1-mV sensitivity on both vertical channels with a full 25-MHz bandwidth, five display



modes and stable, high-speed gated trigger capable of locking any signal from dc to 40 MHz, including TV line and frame. Special operating requirement such as dc trigger or $\times 5$ magnification is obtained by pressing the appropriate button. Also incorporates internal delay lines and offers optional battery pack. \$1,150.00—Scopes Unlimited, Inc., 1928 South Anaheim Blvd., Anaheim, CA 92805. *Circle 32 on reader service card*

AMPLIFIERS, models PA-2938 & PA-2939. Both models help to boost low-power mobile or base station and give it increased talk power and greater operating range. Operation is automatic and self-protecting. Balanced emitters are tested for all mismatched conditions. Extra heavy heatsinking is used to provide extended duty cycle in the course of everyday use.

Built-in low-pass filter attenuates harmonics in excess of FCC requirements. SWR pro-

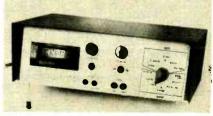


tection has reset button to reactivate power amplifier after shutdown. Frequency range: 150 MHz-175 MHz. Power input: *PA-2938*, 10 watts; *PA-2939*, 25 watts. Power output: *PA-2938*, 80 watts; *PA-2939*, 80 watts.—**Sonar Radio Corp.**, 73 Wortman Avenue, Brooklyn, NY 11207.

Circle 33 on reader service card

POWER SOURCE MONITOR, model VS-200 contains five regulated power supplies. Has dual ± 15 V, 110 mA supply for most common linear amplifier applications. Has dual polarity, tracking ± 200 mA power supply that can be controlled between 50 mV and 20 V. Also has 0-200 mV, 10-mA supply whose polarity can be reversed.

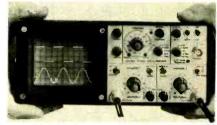
31/2 digit liquid-crystal meter is 0.5" tall; monitors the output of any power supply; can



be switched by front panel control to monitor the outputs of standard power supplies; can also be used to measure voltages produced by other devices; accuracy is 0.2%. Automatic decimal point placement; automatic short-circuit shutdown; unit doubles as digital voltmeter. 5 x 15 x 11 in.; \$395.00.—Thinc, Technical Hardware Inc., P.O. Box 3609, Fullerton, CA 92634.

Circle 34 on reader service card

OSCILLOSCOPE, model PS940A. Mini-portable scope features computerized triggering. TTL logic circuit eliminates the need for front panel adjustment to achieve a stable trace display. DC trigger mode most often used in digital test efforts allows user to make vertical position adjustments without losing sync. Twenty one sweep ranges, 20 MHz bandwidth, 10 mV/div sensitivity, built-in delay line for use in viewing pulse leading edges, full dual-trace switching capability, algebraic waveform as well as ac, low-frequency reject



and high-frequency reject trigger modes. Screen size is full 8×10 divisions with each division equal to $\frac{1}{4}$ ". Battery recharging circuitry is included within chassis. Operates from battery, ac or dc powered; battery charge indicator. $3\frac{1}{2} \times 8\frac{1}{2} \times 12$ in.; 9.5 lbs.; \$1,095.00. **Vu-data Corp.**, 7170 Convoy Court, San Diego, CA 92111.

Circle 35 on reader service card

CB ANTENNA, model M-306 is designed for use on motorcycles, fiber-glass bodied vehicles, boats, snowmobiles and other vehicles that do not have enough metallic ground area to assure good operation of a standard CB antenna. Secret of the unit's performance is its half-wave-length electrical design with both base-and-whip-loading coils. Heavy-



duty spring above the base loading coil provides shock protection.

Entire antenna is designed for reliable operation under high vibration conditions. Has white fiber glass whip and streamlined chrome spring assembly. Supplied complete with hardware for a variety of installation requirements that include mounting on vertical or horizontal surfaces or on round bars up to $34^{\prime\prime}$ in diameter. \$30.95—complete with coax cable and connector.—Antenna Specialists Co., 12435 Euclid Avenue, Cleveland, OH 44106.

Circle 36 on reader service card

SOLDERING IRON, *D I Line*. Heater and handle with two-conductor cord set and safety plug are double insulated; meet latest safety standard of OSHA and are UL listed. Modular in concept. Four rugged stainless steel heaters and three heat ranges provide flexibility for virtually every soldering job. Easyto-use, lightweight and compact design. Han-

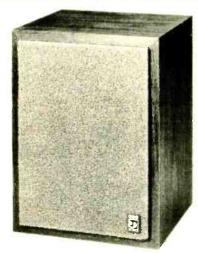


dle is molded of durable plastic with finger-ease cool drip.—**Ungar**, Div. of Eldon Industries, Inc., 233 East Manville, Compton, CA 90220.

Circle 37 on reader service card

SPEAKER, Formula 1 is a two-way system that is designed as the main speaker in budget systems or as a second stereo pair. Frequency response is 35—17,500 Hz; impedance is 8 ohms. For use with low-power amplifiers or receivers, yet it can handle as much as 50 rms watts per channel.

Bass energy is boosted as woofer's backwave energy travels through Venturi-coupled



path that functions as acoustic transformer. In that path, air motion velocity increases over broad band of bass frequencies. "Biconex" horn/compression driver assembly is used to cover mid-range and treble frequencies. 15 \times 10% \times 10 in.; \$74.95 each.— **BIC Venturi, British Industries Co.,** Westbury, NY 11590.

Circle 38 on reader service card

4-CHANNEL RECEIVER, model CS70R offers choice of 4-channel systems—discrete or matrix—or 2-channel stereo; full-featured digital clock that can be pre-set to turn complete system on or off; power switch that is actually a key that can lock the system in the off position.

Tuner features: FET FM front end, i.f.



amplifier with an IC and three solid-state filters, IC FM multiplex demodulator, ultrasensitive AM tuner section. Preamplifier sec-



The New Electronics Book

Sophisticated Electronics For Fun

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A totally new step by step guide to the "how to" of modern electronics, with 190 illustrations in this big 8 1/2" X 11" book.

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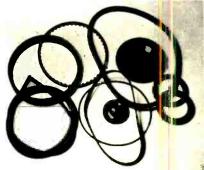
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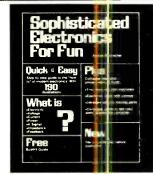


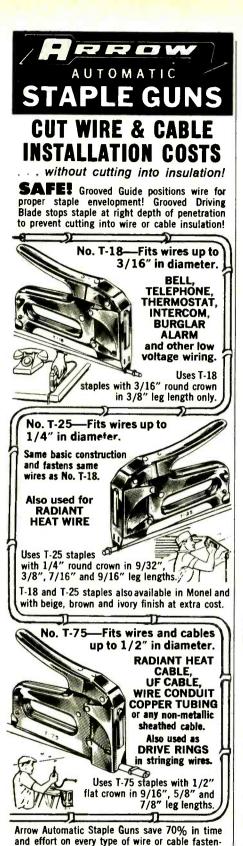
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PROJECTOR-RECORDER BELT CORP. 317 Whitewater St., Whitewater, Wisconsin 53190 414/473-2151 Circle 28 on reader service cert





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Circle 29 on reader service card

tion has 11 controls that include separate bass, treble and loudness controls; inputs for tape, phono and aux.; accommodates FM wireless microphone; stereo and 4-channel headphone jacks. Amplifier section has bridged transformerless circuit, power output in 2-channel mode 22 + 22 watts rms (each channel driven) into 8 ohms at 1000 Hz; in 4-channel mode 12 × 4 watts rms (each channel driven) into 8 ohms at 1000 Hz; total harmonic distortion in 2- and 4channel modes is less than 1% at rated power; power bandwidth in all modes is 30 to 40,000 Hz; frequency response is 40 to 20,000 Hz + 3 dB - 3 dB. \$370.00.-Yamaha, 6600 Orangethorpe Avenue, Buena Park, CA 90602.

Circle 39 on reader service card

SERVICE AID, Omni-Spra, is a nozzle extension that sprays in a 360° circle as well as out the end-used for cleaning the backs



and sides of components as well as the fronts. New aid is being packed with all cans of the company's "Blue Shower." For free sample, send note to attention of Jean Main. -Tech Spray, P.O. Box 949, Amarillo, TX 79105.

Circle 40 on reader service card

LEAD BENDER, model N-300 eliminates measurement and trial and error bending of component leads. Matching pointers with eyelet holes in circuit boards by spining knurled wheel with thumb automatically spaces bends for insertion of component into board. Bends are formed by pressing



leads against sides of pointers with thumb and forefinger. All axial lead components are accommodated, e.g., resistors, capacitors, diodes, transistors, inductors, etc. up to 1/2 in. diameter x 11/2 in. long with maximum distance between inside of bends of 1.725 in. \$32.50-complete with spare set of lead guides .- Harwil Co., 903 Colorado Avenue, Santa Monica, CA 90401.

Circle 41 on reader service card

TURNTABLE, model SR-212. Two-speed (331/3, 45 rpm) unit features a heavy beltdriven 12" aluminum alloy platter. Motor is a stable 4-pole synchronous design that maintains constant speed regardless of line voltage variations. Cueing device is damped going up as well as down. No chance for tone-arm snap-up and loss of correct position when just a pause in play is desired.

All you have to do is move tone-arm over the record groove and nudge cueing lever. Arm floats down over the groove and lifts up again when the side is completed; arm is an S-shaped design with anti-skate counter

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8008 CPU, 1024 x 8 memory; memory is expandable. Kit includes manual with schematic, programming instructions and suggestions; all ICs and parts supplied except cabinet, fuses and hardware. Includes p.c. boards. \$375.00 MANUAL ONLY, \$25.00

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Circle 30 on reader service card

SCELBI COMPUTER CONSULTING. INC. Announces The Totally New and The Very First MINI-COMPUTER Designed For The ELECTRONIC/COMPUTER HOBBYIST!

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Literature available by request: SCELBI COMPUTER CONSULTING, INC. 1322 Rear - Boston Post Road Milford, CT. 06460 Phone (203) 874-1573 Circle 61 on reader service cardbalance in addition to conventional stylus torce counter balance weight. Comes complete with walnut base. Connection from arm



to amplifier is low-capacitance lead that is suitable for CD-4 applications. \$149.95.---Sansui Electronics Corp., 55-11 Queens Blvd., Woodside, NY 11377.

Circle 42 on reader service card

DIGITAL MULTIMETER, model 2180. $3\frac{1}{2}$ digit, bipolar instrument has all five standard multimeter functions plus five decibel measurement ranges extending from -60 dB to +56 dB. Basic accuracy of 0.1% and resolution of 100 μ V; operates from either ac line or internal rechargeable batteries.

Functions are pushbutton selected and include ac volts, dc volts, ac current, dc current, resistance and decibels. Its 31 measuring ranges are selected by rotary switch with additional battery check position that allows internal battery conditions to be monitored. Automatic integral battery charging circuit will maintain batteries at full charge as long as instrument is connected to ac line. "HT Converter" A-D conversion technique,



coupled with LSI, has enabled reduction of components. Circuit boards, IC's and displays are plug-in. \$395.00.—**United Systems Corp.** 918 Woodley Road, Dayton, OH 45403. *Circle 43 on reader service card*

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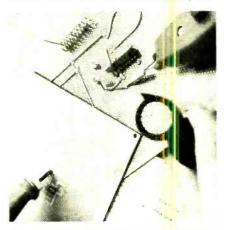


connectors. There are no wires to cut, strip, solder or splice. Power source is a standard 6- or 12-volt battery.

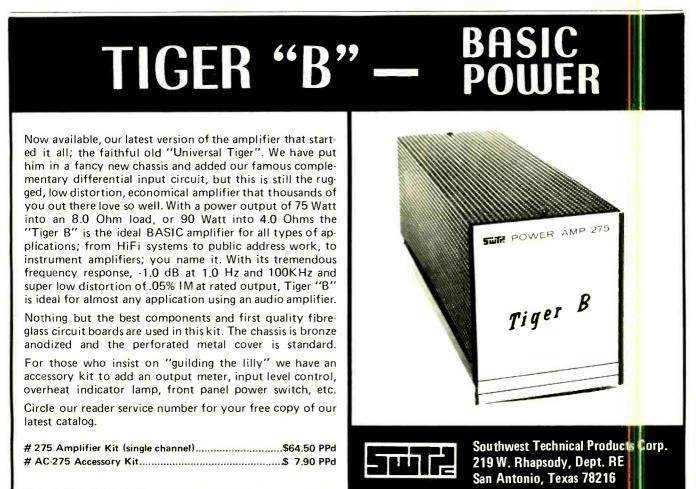
Each set includes a solid-state control center that is always alert to fire danger, even when the burglary system is turned off; an electronic siren with separate signals for fire or burglary; a key switch that permits the system to be turned on or off from outside the home; intrusion detectors for doors or windows; fire detectors; 20-foct extension cords; three-way connectors; an easy-tofollow installation manual; identifying warning decals. \$69.95; expanded deluse version \$99.50.—**Master Lock Co.**, 2600 North 32nd Street, Milwaukee, WI 53210.

Circle 44 on reader service card

NON-CONDUCTING METAL SHEET for printed circuitry. To make a simple circuit or a complex multi-layer breact ard, you draw or scribe your design directly on the surface of the material which institutly ren-



ders a working circuit. Pressure is all that is necessary. For mass production a letter press can be used. Without using a new board, circuits can be erased for meking new designs. Since the metal sheet is non-conducting, components and wiring can be spotsoldered at random, independent from adjacent areas of the board. For use in solid-



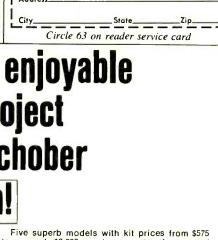
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state printed circuitry, breadboarding, terminal blocks, chassis, etc.-Metal Circuit Systems Corp., P.O. Drawer 2226, Houston, TX 77001.

Circle 45 on reader service card

WIRE STRIPPER, model EWS-10K. Cuts and strips 5000 wires per hour with 6 in. wire length. Strip length from 0-1.5 inches in 0.1 inch steps; wire length from 2.5-99.9 inches in 0.1 inch steps. Wire feeds via two stepping motors; wire length and strip length controlled by gating proper number of motor



OK MACHINE AND TOOL CORPOR BDONX N

steps. Same strip block used for all lengths. All solid-state control; no air required. Preset number stops operation automatically after selected number of cycles. Non-nicking blades are made of heat treated tool steel. Complete panel functions; three operating speeds-slow, medium, fast. For AWG24-30. 18 \times 20 \times 20 in.; 90 lbs.—OK Machine and Tool Corp., 3455 Conner Street, Bronx, NY 10475

Circle 46 on reader service card

EXACT REPLACEMENT ZENITH SOCKETS. Kit No. 39 contains a general purpose assortment of four sockets, none of which has a substitute. In addition to this kit, Oneida



also offers zenith sockets S-74-C, an exact 9-pin replacement and S-75-C, an exact 12pin replacement. Combination of the kit assortment plus the other two sockets provides complete Zenith coverage .- Oneida, Box 558, Meadville, PA 16335. R-E

Circle 47 on reader service card

American Airlines installs TV on all its luxury planes

Special television systems that provide recorded TV shows or full-length movies have been installed on all of American's DC-10 Luxury Liners. Each DC-10 is equipped with a color videocassette player/recorder in the first class section and a 25-inch RCA XL-100 television set in the cabin, R-E

new lit

All booklets, catalogs, charts, data sheets and other literature listed here with a Reader Service number are free. Use the Reader Service Card inside the back cover.

ELECTRONIC COMPONENTS CATALOG. 35page catalog contains 350 items carrying the Ultratec label. Among them are mike, tape and phono accessories, miscellaneous electronic accessories, audio cables and adapters, hi-fi and hobby electronics, tools and service aids, panel lamps, fuses and battery holders, wires and cables and electronic construction components. An alpha/numerical index appears at the end of the catalog. --Workman Electronic Products, Inc., Box 3828, Sarasota, FL 33578.

Circle 48 on reader service card

J-JACKS CATALOG. 12-page brochure explains the company's J-Jacks system for educational and medical TV systems; permits distribution of uhf, vhf, FM, closed-circuit video and audio signals simultaneously throughout the school or hospital; also has 2-way signal carrying capability. Covers design and installation, from basic distribution systems to sophisticated automatic 2-way systems. Architect specifications are also included.—Jerrold Electronics Corp., 401 Walnut Street, Philadelphia, PA 19105.

Circle 49 on reader service card

KIT CATALOG. 56-page catalog lists over 175 different kits ranging in price from a few dollars to a few hundred dollars. Product areas covered are amplifiers and preamplifiers, test instruments, power supplies, radio control apparatus, auto accessories, ham and CB accessories, musical instrument accessories, FM transmitters and receivers. Many illustrations.—**Audiex Electronics**, P.O. Box 156, Station "S", Toronto, Ontario, Canada M5M 4L7.

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BUSINESS FORMS CATALOG. 32-page catalog for television and appliance firms contains multipart service order forms, repair tags, sales forms and billing forms. These forms are in duplicate and triplicate sets, consecutively numbered and imprinted with your firm's name and address. Also featured are business cards, pressure sensitive labels, carbonless register forms, bookkeeping systems and many other business forms. Illustrations in color.—New England Business Service, Inc., P.O. Box 500, Townsend, MA 01469.

Circle 51 on reader service card

CHART, Increase Your Viewing Pleasure. Complete buyers' and sellers' guide to RCA Permacolor outdoor antennas, uhf-vhf/FM, vhf/FM, uhf-only, FM-only; rotators (including Selecta-channel 10W606); three different types of antenna mounting kits and Mini-State antenna system with hand-held rotator remote control unit. 11 x 44 in.; shows inside components of Mini-State antenna and cabinet design of rotators; also lists components of antenna mounting kits that are available.— RCA Parts and Accessories, P.O. Box 100, Deptford, NJ 08096.

Circle 52 on reader service card

HI-FI LOUDSPEAKER SYSTEMS CATALOG. 24-page illustrated brochure describes floor standing loudspeaker systems, compact loudspeaker systems, Stonehenge I and III loudspeaker systems as well as components and utility systems. Price list is inserted in brochure.—Altec Sound Products Division, 1515 South Manchester, Anaheim, CA 92803.

Circle 53 on reader service card

1974-75 VHF-UHF-FM TUNER REPLACE-MENT GUIDE AND PARTS CATALOG NO. 4. 95-page catalog contains exact tuner replacements, widely used tuner parts, chemicals and tools. Indexes for blow-ups and uhf tuners. Covers Standard Kollsman, Oak, Sarkes Tarzian, RCA, Zenith, Philoti, Motorola, G.I., miscellaneous, domestic and foreign made tuners. Includes antenna inatching coils and antenna coil replacement guide. \$2.00; refundable on first order for goods or services.—**PTS Electronics, Inc.**, **P**O. Box 272, 5322 Hwy. 37 S., Bloomington, IN 47401.

STEREO & 4-CHANNEL CATALOG. 32-page catalog contains 8-track stereo recording decks, AM/FM stereo systems, turntables, mini changers, TV tuner and electronic control cleaner, speaker systems, recording tapes, hi-fi shelving unit, tape recorded control center, headphones, audio gadgets and many illustrations.—Etco Electronics, Box 741, Montreal, Quebec, Canada. R-E





COSMOS PROJECTS

(continued from page 60)

voltage swing of C1 is clamped to the limits of the power supply voltage by the input protection diodes of the cos/mos gates, the operating frequency is influenced by variations in the supply voltage: Typically, a 40% variation in supply vol-

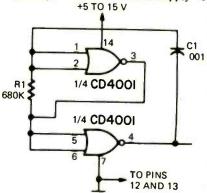
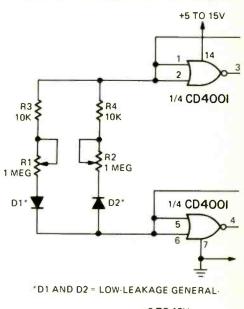


FIG. 30-BUFFERED-OUTPUT 1-KHZ astable



+5 TO 15V 2 **R1** 1/4 CD400I D1* 100K **R2** 1 MEG D2* **R**3 100K 1/4 CD4001 5

*D1 AND D2 = LOW-LEAKAGE GENERAL-

FIG. 31-a-VARIABLE MARK/SPACE RATIO VIBRATOR with independently variable on

tage causes a 5% variation in frequency. Another disadvantage is that the frequency of operation is influenced by the transition voltage values of the CD4001 gates and in practice, the actual frequency of operation may vary by 10% over the production spread of the CD-4001 when using identical R1 and C1 values

OUTPUT

1/4 CD400I

multivibrator.

10

+C1

TO PINS 8, 9, 12 AND 13

C1

TO PINS 8, 9, 12 AND 13

.001

PURPOSE SILICON DIODES

and off times.

astable multivibrator. b-ASTABLE MULTI-

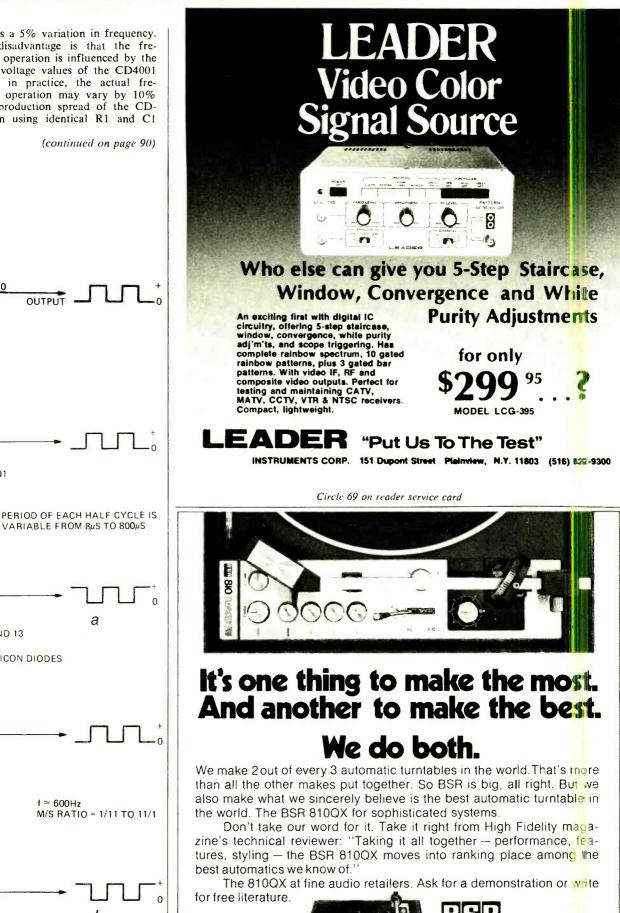
PURPOSE SILICON DIODES

(continued on page 90)

а

 $f \simeq 600 Hz$

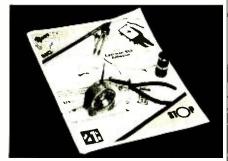
b





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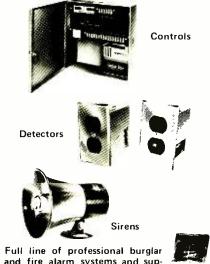


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COSMOS PROJECTS (continued on page 89)

Both of these disadavantages can be largely overcome by simply wiring a high value resistor in series with the input of gate A, as shown in Fig. 29, thus enabling the voltage swing of C1 to exceed the supply voltage. Limiting resistor R2 must have a value at least double that of timing resistor R1.

In practice, the operating frequency of this circuit is subject to a change of less than 5% over the production spread of transfer voltages, and to a frequency shift of less than 2% with a 40% change in supply voltage. Another advantage conferred by the use of R2 in the Fig. 29 circuit is that of excellent thermal stability: The operating frequency typically varies by only 1% over the temperature range -40° C to $+85^{\circ}$ C.

Minor disadvantages of both the Fig. 26 and Fig. 29 circuits are that the leading and trailing edges of the output waveforms sometimes contain a certain amount of sag and 'mush', and the operating frequency is influenced by variations in the output loading conditions. Both of these disadvantages can be overcome by interposing an inverting buffer stage between the output of the astable multivibrator and the input of the external loading circuit, as shown in Fig. 30.

A final disadvantage of the Fig. 26 circuit, and to a lesser degree of the Fig. 29 circuit, is that the symmetry or mark/ space ratio of the output waveform depends on the transition voltage value of the individual CD4001 that is used. An IC with a transition voltage value of 35% gives a mark/space ratio of approximately 35/65, and an IC with a value of 60% gives a mark/space ratio of approximately 60/40. A true square wave (50/50) output is available only if the IC has a transition voltage value of exactly 50%.

The mark/space ratio of the output waveform of the astable circuit can be made variable by using steering diodes to select alternative charge and recharge resistance paths for the time-constant network, as shown in Figs. 31-a and 31-b.

In the Fig. 31-a circuit, the capacitor charges via D1 and the low half of the resistance chain in one half cycle, and via D2 and the top half of the resistance chain in the other half cycle. The mark/space ratio can be varied over the range 1/11 to 11/1 via R2, and the circuit operates at a frequency of roughly 600 Hz.

The Fig. 31-b circuit has independently variable ON and OFF times. In one half cycle, the capacitor charges via D1—R1 and R3, and in the other half cycle, it charges via D2—R2 and R4. The period of each half cycle is variable over the approximate range 8 μ s to 800 μ s using the component values shown.

In this part of the series we have looked at practical ways of using the CD4001 in monostable and astable multivibrator applications. In the coming part of the series we shall go on to look at sixteen ways of using the CD4001 in lamp flasher, time delay, oscillator, and alarm applications. **R-E**



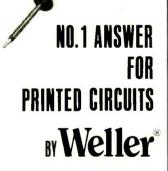
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APEX, NORTH CAROLINA 27502 Circle 75 on reader service card

COMPUTER TERMINAL

(continued from page 44)

key sends a pulse to the 2-bit page counter which increases its count by 1 and advances the page controls 1 step.

In AUTO, the page will automatically change every time a character is entered into the last position in a page. The instant after the page change, the new page's home position is at the cursor position. The black "P" key can still be used to change pages in the AUTO mode.

In the AUTO STOP mode, the operation is identical except that the automatic page change can be stopped on any page desired by wiring from the PAGE switch to one of four points. This gives the operator the advantage of being able to receive data into memory in the automatic mode and retain it, say, in the first 3 pages, and work on the 4th page without writing over it, and not having to change any switches.

In either automatic mode, pressing the clear key (black "C") will have the same effect as entering data into memory in the last position. This results in a page change every time you clear a page in automatic. This gives the operator the advantage of clearing all 4 pages with 4 key strokes of the clear key.

Power supply

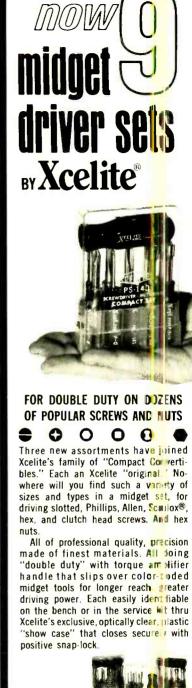
The power supply consists of two paralleled power transformers (for added current and packaging requirements), a +250 volt unregulated supply, two +5 volt regulated supplies, a -10 volt an -12 volt Zener regulated supply.

The +250 volt supply runs the self scan plasma display. One of the +5 volt supplies runs all logic on the main board, and the other runs the keyboard, modem/coupler board, and add on memory board. The -10 volt supply powers only the memory, while the -12 volt supply is connected to the UART and to the modem/coupler board to power the op-amp and XR210 demodulator.

Tape recorder memory

Using the tape record feature to record and play tapes from the CT-256, a medium quality (cost greater than \$50) or better cassette recorder is advisable along with a good quality recording tape. Of course a good reel to reel machine would insure better data integrity but good results are obtainable from a cassette machine.

Making a recording is as simple as connecting a miniature phone plug to the jack on the back of the CT-256 and the other end to the "mic." input on your tape recorder. Once you have (continued on page 106)



NEW!

PS130 — 3 slot tip, 2 Phillips screwdrivers, 5 nutdrivers PS140 - 4 slot tip, 3 Phillips screwdrivers, 3 nutdrivers PS6 - 3 slot tip, 3 Phillips screwt rivers PLUS - PS88, PS120, PS7, PS89, PS44, and PS-TR-1 with varying selec tions of screwdrivers and nutdrivers. 11 20

Ask your local distributor or write

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www.americanradiohistory.com

There's a new Heathkit everyone on The Heathkit Digital Color TV is for two kinds

12:27:46

of people

... those who understand electronics, and those who don't

People who understand electronics will appreciate the GR-2000's advanced digital design, incorporating on-screen channel readout and optional clock. Digital logic circuitry programs up to 16 stations in any sequence. Then just press a button - you'll never have to switch through a "dead" channel again. And our exclusive VHF/UHF varactor tuner eliminates clunking

contacts that corrode and noisy motors that break down.

The GR-2000 also has the industry's first fixed-filter IF amplifier. There's no need for instrument IF alignment ever, so the picture stays bright and clear year after year. And even in

urban areas where stations are packed closely together, there's virtually no adjacent channel interference. The 100% solid-state chassis uses 19 integrated circuitsmore than any other TV

around. You'll get superior performance and reliability

no conventional set can match.

A built-in dot generator and test meter make it easy to keep the GR-2000 in peak condition without expensive service calls. The slide-out service drawer and hinged, swing-out chassis put everything in easy reach. If anything ever goes wrong, an extensive trouble-shooting guide will help you fix it.

And people who don't understand

electronics will enjoy the best looking picture around. Popular Electronics said the picture on the 25" (diagonal) screen "can only be described as superb. The Black (Negative) Matrix CRT, the tuner and IF strip, and the video amplifier provide a picture equal to that of many studio monitors ... "

Everyone likes the on-screen readout that puts the channel number into the picture whenever you want it. When you change channels or touch the recall button, the big, bright digits reappear. Add the optional clock module and you'll see the time as well as the channel.

The optional wireless remote control makes the GR-2000 even more enjoyable. Change channels, adjust the volume, set tint and color intensity and turn the set on or off from across the room. And, a touch of the Volume bar automatically returns the digital readout to the screen momentarily. It's an amazing handful of convenience.

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structions, prefabricated wiring harnesses, transistor and IC sockets and modular circuit boards greatly simplify assembly.

See the TV the experts are talking about. Popular Electronics summed it all up: "In our view, the color TV of the future is here-and Heath's GR-2000 is it!"

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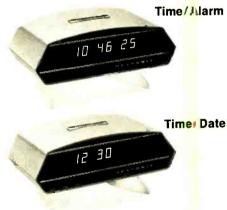
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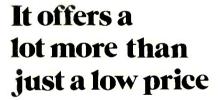
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DECEMBER 1974

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TO * FLYBACK TRANSFORMER 200 for all type TV's incl schematic 2	TUBE SPECIAL	100—ASST 2/56 SC	REWS 100	Silicon NPN HV TRANSI ITOR
70° TV DEFLECTION YOKE 700	6DQ5 - 12BH7 - 18FY6	and 100-2/56 HEX	REWS 100	L RCASK-3021-Hep-210 169
70° TV DEFLECTION YOKE 200 for all type TV's incl schematic 20 SHARP 110° FLYBACK &	6043 - 126H7 - 18F16	and 100-4/40 HEX	NUTS	RCA—SK-3026—Hep-241 I Transistor Specials—Year Choice
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70 COLORE YOKE 1095	335H3 - 305H3	L most useful selected	R BUMPERS 100	4"-1 Oz. Magnet-8 Ol ms 50
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🗨 41mc	100-ASST 1/2 WATT RESISTORS 100	Compact design f	layback Deck 2750 its anywhere 100	STEREO MICROPHONES FL 1979/01 Made in Helland SET 50 25' Shielded MIKE CABLE 100
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all 41 mc TV's,	stand, choice ohmages, some in 5%	I I I5" SPEAKER	139	Dopular asstd, ampere rith gs 1 50—RADIO & TV SOCKITS 100
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4 Channel closed circuit 495 PHILCO TV TUNERS 495	□ 1 amp., 1000 PIV □ □ 1 amp., 1000 PIV □ 000 000 000 0000 0000 0000 000000000	VARCO Stereo Ca	c Type—8 Ohm tridge-CN-72	Boathook Clamp 7" [mg 4
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Circle 81 on reader service card

BUILD—with 1 IC 3-way function generator

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By ROBERT COLMAN

A LARGE NUMBER OF Radio-Electronics READERS OWN elaborate and costly high-quality, high-fidelity sound systems. To check the performance of sound systems of this type requires the use of sophisticated high-performance signal generators. Unfortunately, such instruments are usually very costly and would not be used often enough to justify their purchase.

But there is an alternative. It is a 14-pin monolithic integrated circuit which can deliver sine, square, triangle and pulse waveforms that are highly accurate. This new IC is the Intersil 8038. It operates over a frequency range from .001 Hz to 1 MHz and is highly stable over a wide range of temperature and supply voltages. By using additional external voltages, it is even possible to use the IC as a sweep generator and add FM modulation. The device uses the latest technology, including thin-film resistors and Schottkybarrier layer diodes.

Although the more complex functions of the 8038 are certain to interest some readers, we were primarily interested in the design of a basic audio signal generator that would deliver signals from 20 Hz to 20 kHz using only a single tuning control. The output signals produced by the generator are square, triangle and sine waves.

How the circuit works

A block diagram of the 8038 IC function generator is shown in Figure 1. The external timing capacitor C1 is alternately charged and discharged by two current sources.

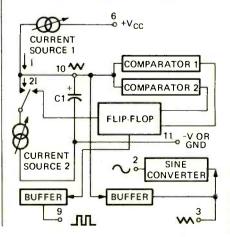
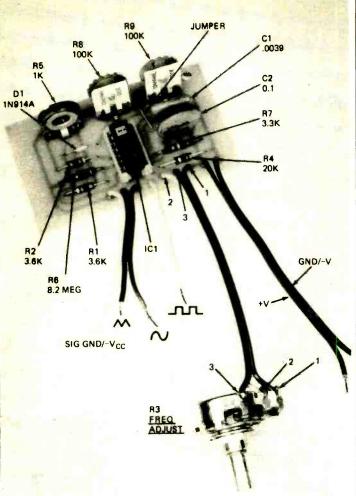


FIG. 1 - BLOCK diagram of waveform generator. All elements, except for C1, are in the IC.

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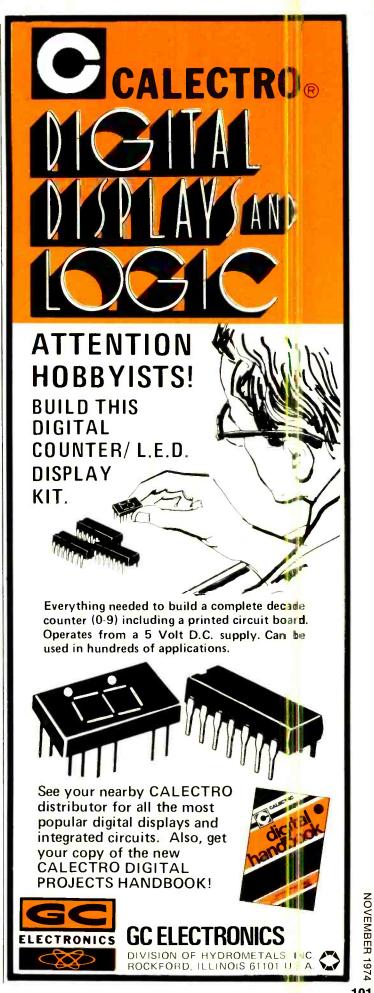
CALLOUTS IN PHOTO of completed generator show where to mount parts on the circuit board.

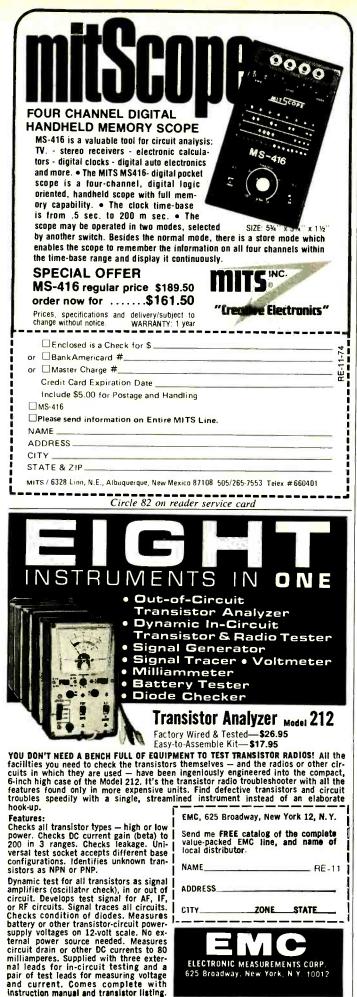
Current source 1 is on at all times while current source 2 is switched on and off by a flip-flop.

Assuming that, initially, the flip-flop turns off current source 2, the capacitor is charged by current source 1 with a current I. As a result, the voltage across the capacitor rises linearily with time. When the voltage across the capacitor reaches the threshold voltage of comparator 1 (which is set at $\frac{2}{3}$ of the supply voltage), the flip-flop changes state and turns on current source 2 which carries a current of 2I. The capacitor is discharged with a net current I and the voltage across it drops linearily with time. As the capacitor discharges toward a negative peak, it eventually reaches the threshold voltage of comparator 2 (set at $\frac{1}{3}$ of the supply voltage). When this occurs, the comparator output resets the flip-flop to its original state and current source 2 is turned off. At this point, the cycle is repeated.

The triangular waveform, which is developed across the timing capacitor, is fed internally to a buffer amplifier and is available for external use at the output pin 3. In addition, the triangle waveform is fed to a sine converter, which consists of a non-linear network, for conversion to a sinusoidal waveform. According to Intersil, the typical total harmonic distortion of the sine wave output is less than 1%. With careful adjustment, distortion levels as low as 0.5% are possible.

The square wave output is taken from the flip-flop and fed to another buffer amplifier, the collector of which is connected to output pin 9. In this manner, the supply voltage for the square wave output is independent of the rest of the circuitry and a separate 5 V supply may be used to provide TTL compatibility.





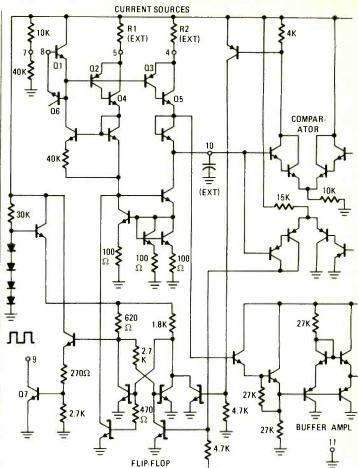


FIG. 2—DETAILED CIRCUIT DIAGRAM of the Intersil 8038 IC waveform generator.

Design

Since we propose to sweep the frequency of the generator over a 1000:1 range, let's take a look at what determines the output frequency. Figure 2 shows the detailed circuit diagram of the 8038 IC waveform generator.

The voltage developed across the two external resistors, R1 and R2, produces two currents to charge and discharge the timing capacitor tied to pin 10. Because this is a linear system, dropping the voltage across the external resistors from 10 volts to 1 volt will also drop the lower output frequency by a factor of 10. This will increase the output frequency range by 10:1. Lowering the voltage still further from 1 volt to 100 mV will also increase the output frequency range by another 10:1. By causing the voltage across the external resistors to change, say from 10 V to 10 mV, we can vary the output frequency at least 1000:1.

Transistors Q2 and Q3 supply the charging current to the external capacitor. This current is determined by the value of resistors R1 and R2, as well as the bias current of

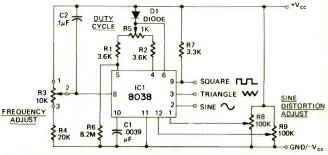
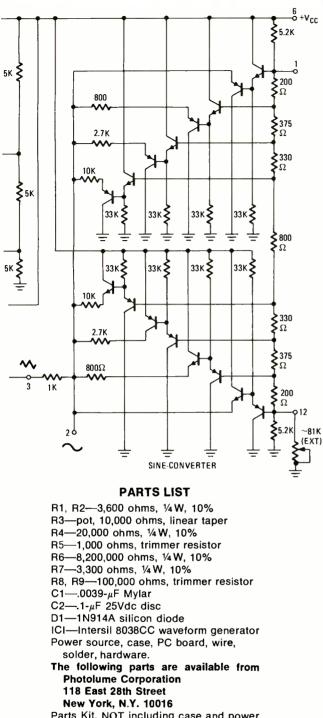


FIG. 3—SCHEMATIC OF THE GENERATOR. Circuit is built around the Intersil 8038 waveform generator IC.

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Parts Kit, NOT including case and power supply — \$10.95 incl. postage and insurance. Circuit board—\$2.50.

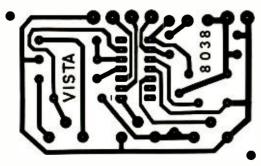
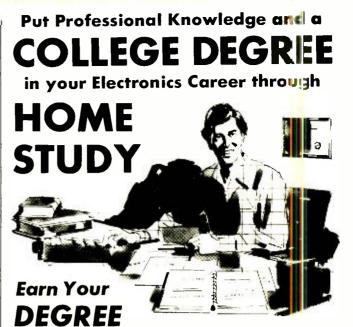


FIG.4—FULL-SIZE FOIL PATTERN of the circuit board for the generator.



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ee hotline, John Fluke Mfg. Co., Inc., P.O. Box 7428, Seattle, WA 98133 Circle 85 on reader service card transistor Q1. Due to the V_{be} mismatch between transistors Q1 and Q2 (also Q1 and Q3) and because of the circuit geometries and current levels involved, the voltage across the external resistors R1 and R2, with pin 8 connected directly to $+V_{ce}$, will be 100 mV or more, with a 100:1 sweep ratio. To obtain the smaller voltages necessary for the required 1000:1 frequency range, the voltage at pin 8 must be raised above $+V_{ce}$. The required voltage difference need only be a few hundred millivolts, which we can get without a separate power supply by simply adding a series diode from pin 6 to the external resistors R1 and R2 (see Fig. 3). This raises the applied voltage to pin 8 by one diode drop above $+V_{ce}$.

The charging current carried by transistors Q2 and Q3 is determined by the impedance between pins 4 and 5, as well as the bias currents. Any small offset or differential voltage will cause an imbalance in the charge and discharge currents and a marked change in the duty cycle. While a single external resistor is fine for simple circuits, for our more demanding performance requirement, we use the separate external resistors R1 and R2. By using separate resistors, we can vary the ratio of the charge-to-discharge rate of the external capacitor. In this manner, the duty cycle of the square wave output signal is variable from 2% to 98% and the triangle output waveform can be adjusted for either a positive or negative going sawtooth or ramp.

To further lower the output distortion, the voltages applied to pins 1 and 12 are adjusted using two trim resistors (see Fig. 3). In addition, we can compensate for the remaining duty-cycle error by connecting a high value of resistance from pin 5 to $-V_{\rm ec}$ which bleeds a small amount of current away from pin 5 and tends to bring the duty cycle back to 50%. With these basic adjustments, we have a reasonable compromise between low distortion and wide frequency range.

The schematic diagram of the actual generator circuit is shown in Fig. 3. The oscillator frequency of the 8038 IC is set by the value of timing capacitor C1 (.0039 μ F) and the voltage applied to pin 8.

Construction

Construction of the actual audio function generator is easy. Only a few components are required in addition to the IC and power supply. Printed circuit construction is recommended and a foil pattern (Fig. 4) is supplied for the reader who wants to make his own. An etched and drilled circuit board is available (see parts list) for those who prefer to purchase one. While component tolerances are not critical, the use of a good quality Mylar film capacitor for C1 is recommended for stability of the output frequencies.

All the parts of the generator, with the exception of the FREQUENCY ADJUST potentiometer, are mounted on the circuit board. Parts layout is shown in the head photo.

Install and solder all resistors, capacitors and trimmer resistors on the PC board first. Solder the jumper in place on the foil side of the board. Next, install and solder diode. D1, being sure to observe the polarity.

Now install IC1 on the board. We recommend the use of an IC socket to prevent possible damage to the IC during soldering and to provide for easy replacement in case it malfunctions. The parts kit which is available (see parts list) includes an IC socket which consists of two MOLEX connectors and two plastic insulating jackets. Install the MOLEX connectors into the plastic jackets and solder the units to the PC board, being careful not to melt the plastic jackets with the heat from the soldering iron. After soldering, carefully break off the metal tab on each connector and install the IC.

The entire generator board with power supply or bat-

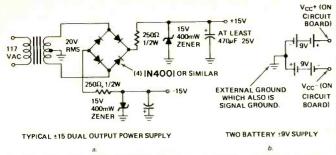


FIG. 5—POWER SUPPLY CIRCUITS. a—A Zener regulated supply. b—How batteries can be used.

teries and FREQUENCY ADJUST pot will fit into a case of the type readily available to readers. It will be necessary to obtain either output jacks or a terminal strip for the outputs.

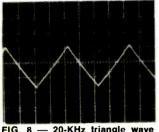
Install the FREQUENCY ADJUST pot and output jacks on the case and solder leads to the appropriate points on the PC board. Install the PC board in the case, along with a source of power and a switch for turning it off and on.

Any simple power supply having reasonable regulation may be used. But be sure you do not exceed the manufacturer's recommended rating of ± 15 Vdc or +30 Vdc of the 8038 IC. The circuit of a Zener regulated supply is shown in Fig. 5-a. Batteries can also be used, but they should be connected as shown in Fig. 5-b. Two 9-volt batteries should supply ample power, but keep in mind that the unit draws about 15 mA when selecting the batteries.



FIG. 7 — 100-Hz SINE-WAVE

FIG. 6 — DISTORTED output waveform.



 20-KHz triangle wave FIG. 9 — 20-KHz SQUARE wave output signal.

output.

Adjustment

output.

When assembly is completed and you are ready to put the function generator into operation, apply dc power to the unit.

To adjust for minimum distortion, connect your scope probe to the triangle waveform output and observe the symmetry of the waveform while adjusting the duty cycle trimmer R5. Adjust the sine-wave next by observing the waveform and alternately adjusting trimmer potentiometers R8 and R9 for minimum distortion. Figure 6 shows the distorted sine-wave when the trimmer pot is not adjusted correctly. If you have a distortion meter, you may use it as a final check on the setting of the sine-wave trimmers and adjusting them for minimum distortion. Check the square-wave output and readjust trimmer R5 if necessary for a 50% duty cycle. This completes the adjustments of the generator. The actual output waveforms are shown in Fig. 7, 8 and 9.



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(continued from page 91)

connected to the computer and the phone is in the top of the terminal. you can set your audio level. If the recorder used has an automatic level control, use it; if not, record at a "0" dB level (maximum undistorted level).

To play a tape back, the MODE switch should be in the IN/OUT position and the playback level should be twice as high as to cause the CARRIER LED to light. Make sure the baud rate is set for the proper data rate on the recording. The connection to the CT-256 stays the same, just change the connection on the recorder from MIC. input to line out or ext. speaker.

Assembly

Building a one page CT 256 includes parts installation and wiring of 2 large double sided circuit boards. one medium and one small single sided board. For a multipage unit there is a third large double sided board containing up to three additional pages of memory plus power switching circuitry. First, parts are installed on all boards. (Be sure to follow handling instructions for MOS chips.) Switches and connectors are wired to the main board before its installation. Once the main board is installed in the chassis, the power supply board is wired in, the 5 volt regulators are installed and wired, and wiring to the acoustic coupler board completed (the kit comes with the acoustic coupler board assembled, tested, adjusted and ininstalled in top cover of main case). Next, the switches, connectors and displays are mounted.

The keyboard assembly should be completed at this time, including assembly and wiring of keyboard connector and cable.

After a final wiring check and inspection for solder bridges, connect keyboard to main unit, connect self scan display to the main board, and set MODE switch to LOCAL. Connect to a 115 Vac power source and turn power switch to on. The page 1 LED should light, and characters should be entered from the keyboard. If problems arise, isolate the problems and analyze them using information from the text and diagrams. An oscilloscope is indispensable in trouble shooting this type of circuitry.

The following items are available from MITS, Micro-Instrumentation Telemetry Systems Inc., 6328 Linn, N.E., Albuquerque, NM 87108.

Complete kit of all parts\$495.00 Kit less cabinet & power supply \$395.00 Assembled Terminal\$695.00

TABLE OF CONTROL CHARACTERS AND THEIR FUNCTION IN CT256

- Control G-Bell signal-used to alert operator-a 1/2 second 1-kHz audible tone.
- Control H-Backspace-moves data in display one position to the right-does not change data in memory.
- Control I-Advance space-moves data in display one position to the left-does not change data in memory.
- Control J--Control character for linefeed. Since it has no meaning in the CT-256 it is decoded and entered into memory as a space.

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Circle 92 on reader service card

- Control K—Home—homes memory address counters to cursor position.
- Control L—Home and clear—homes memory address and clears page.
- Control M—Control character for carriage return—has no meaning for the CT256. It is decoded and entered into memory as a space.
- Control N-Control character for cursor up-has no meaning for the CT256 and is decoded and entered into memory as a space.
- Control O—Address function—sets up receive circuitry to use the next two characters to shift data address to a selected line and position. (See explanation of address function.)

DEFINITIONS FOR SWITCHES AND CONNECTORS CT256 KEYBOARD

Special Key Functions (Top Row of Black Keys)

- [←] Shift left—Moves data left one position (advance).
- [H] Home Returns data to 0, 0 position.
- [→] Shift right—Moves data right one position (backspace).
- [A] Address—Three keystrokes are necessary to select an address (an exact position on a page). Operator goes to desired position on the page by pressing [A], then presses the specific key for line position (1-16), then presses the third key which selects data position in the line (1-16). Characters are not entered until address sequence has been completed.
- [C] Clear—Clears page and returns data to 0, 0 position (home).
- [T] Transmit—Automatically transmits character in cursor position to computer and is used to transmit information line by line from the terminal memory to the computer. Since the terminal memory does not store carriage returns (end of line), the "@" symbol (shift [P]) is placed in memory at the end of each line. The "@" symbol stops transmission and the operator can manually press "return" to indicate end of line.

Other Special-Function Keys

- Rept Repeat—Causes a character to be entered repeatedly. Press character key and Rept. key.
- Rub Deletes previous character.
- Out Shift When working with computer. Allows entry of upper-case characters indicated on keytops. Press shift, then upper-case character desired.
- Ctrl Control—Allows entry of special control signals to computer, i.e., Ctrl and G is bell signal.

INDICATORS on FRONT of CT256. P1-P4 Indicates page displayed.

Carrier Indicates when 2-kHz tone is received from computer via telephone or tape recording. R-E



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RESISTIVE AND REACTIVE CIRCUITS, by Albert Paul Malvino. McGraw-Hill Book Co., 1221 Avenue of the Americas, New York, NY 10020, 592 pp. 91/4x71/4 in. Hardcover \$12.95.

A comprehensive textbook that provides all the information needed to prepare a technician for more advanced electronic courses. The first part of this book discusses resistive circuits with dc or ac sources as these are very prominent today because of directcoupled circuits. The second part of the book covers reactive circuits such as transients, ac theory without using trigonometry or complex numbers. The final section of the book which does require a knowledge of trigonometry goes into extensive coverage of things such as phasor analysis, resonance and instantaneous ac analysis. Definitely a textbook quite valuable to anyone who wants to more fully understand both resistive and reactive circuitry.

SOLID-STATE IGNITION SYSTEMS, by R.F. Graf and G.J. Whalen. Howard W. Sams & Co., Inc., 4300 W. 62 St., Indianapolis, IN 46268. 136 pp. 8¼x5¼ in. Softcover \$4.50 (in Canada \$5.40).

Solid-state ignition is a fact of life in the modern car. There are many types of systems reflecting the various schools of thought about what constitutes the ideal solid-state ignition system. In this book, you will find all the known commercially available methods of solid-state ignition. The authors have conducted careful examinations of original equipment designs as well as add-on systems and all are presented here in great detail. The first chapter describes the phenomenon of spark ignition in easy-to-understand terms. Chapter two then relates how the conventional ignition system produces a spark. Chapter three covers semiconductors and how they are used in ignition systems. Chapters four and five give complete details on existing systems. The last chapter provides data for servicing and troubleshooting modern electronics ignition systems.

HANDBOOK OF MODERN SOLID-STATE AMPLIFIERS, by John D. Lenk. Prentice-Hall, Inc., Englewood Cliffs, NJ 07632. 414 pp. 91/4x6 in. Hardcover \$15.00.

Here is a detailed treatment of both the theory and practice of modern electronic amplifiers. It is perhaps the most comprehensive handbook available today on circuit theory and analysis at the technician level featuring simplified guidelines for practical design, complete test procedures and practical troubleshooting techniques. The book describes all types of amplifiers in common use-audio, rf, direct-coupled, differential, compounds and op-amps. It also covers both discrete amplifier circuits and selected IC's. It is well suited to a board readership-students designers, technicians and anyone else who would like to have a source of up-to-date information on solid-state amplifiers.

TTL COOKBOOK, by Donald E. Lancaster. Howard W. Sams & Co., Inc., 4300 W. 62 St., Indianapolis, IN 46268. 335 pp. 81/4x51/4 in. Softcover \$8.95 (in Canada \$10.75).

In mid-1972, an electronic revolution took place. For the first time, a person could go out and purchase a logic gate for 5c provided you bought four of them at once in a single 20c package. These gates were TTL (transistor-transistor-logic), a very versatile, widely available and fast way of performing logic operations. The TTL Cookbook is about TTL. It shows you what TTL is and how to use it. It is written at a time when TTL IC's are widely and readily available. After covering the basics of TTL, who makes it and where to get data, it goes on to a kind of catalog of TTL devices. Ten applications and illustrations of TTL IC use start coming up. There is a complete chapter on logic applications, another on gate and timer circuits, still another on clock logic and off we go. We continue through divide-by-N counters, shift registers, noise generators and rate multipliers. The final chapter, called Getting It All Together, shows several up-to-the-minute appications of real devices that can be built using TTL logic. R-E

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11 \$60.05	LM380N LM3900	N	Quad Al	MP DIP			.55
ail \$69.95. F RONICS,	LM3905		Precision NOP.A				.65 3/1.00
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-	LM300 LM301H/	Pos.	V Reg roved O		o 5		\$.85 .40
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	LM304H LM305H	Neg Posi	ative Vo itive Vol	itage Regu tage Regul			1.10 1.00
Adda A	LM307H/	/N Op.	Amp (Si	uper 741)			.40
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og featur- s. Unique	LM319H	Hi-S	Speed Du	ual Comp.			1.55
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DIP SOLDER TAIL SOCKETS OUAL IN-LINE SOLDER TAIL SOCKETS GOLD CONTACTS N 44 18 PIN 74 28 PIN. 52 22 PIN 1.00 36 PIN. N 54 24 PIN 1.05 40 PIN available - wire wrap sockets - 1/2/3 levels wr -large volumn DISCOUNTS

74157 \$ 1.55

1.75

3.00 1.75 1.85

74157 74160 74161 74163 1.65 1.65 1.65 2.50

74164 74165 2.50 2.50

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7453 \$ 7454

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CI OS

CD40C1 CD40C2 CD40C9 CD4010 CD4011 CD4012 CD4012 CD4016 CD4007 CD4010 CD40010 CD4002 C

8 PIN

7400 7401

7402

7403

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7409 7410

PIN 16 PIN

Also available

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.23 .23 .23

.25 .24 .50 .50 .25 .25 .23

NOVEMBER 1974

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7-Segment Readuut IR-PIN DIP Received with right-hand decimal Plugs into OIP sockets 7400 DIP 7400 S.25 7400 S.25 7410 S				_
Three digits with right-hand decimal 74400 35 Plugs inilar to (LITRONIX) DL337 744010 35 * Magnified digit approximately _1" 7440 35 * Segments are parallel for multiple 510 Map resegment 7440 35 * Segments are parallel for multiple 7440 35 * Segments are parallel for multiple 7440 35 * Sold Map resegment 7440 35 * AD of Actacts 7440 35 * AD of Actacts 7440 35 * Ad OC (10.5 MA coil) \$1.50 EA 7440 35 * Ad of Subtract, multiply, and divide 7441 36 * 120 VAC (10.5 MA coil) \$1.50 EA 7440 35 * Ad of Subtract, multiply, and divide 7441 36 * 120 vide (16 vide adiculate 7441 36 * True credit balance sign output 7440 35 * True credit balance sign output 7441 36 * Ad of Subdrable 7441 36 * Complete with only.1 51.00 7441 36 * Cot		ut		
* Binalitar to (LITRONIX) 0.137 ************************************	= Three digits with right-hand d	<mark>ecima</mark> l	7401	. 35
* Segments are parallel for multiple 7406 .35 * Segments are parallel for multiple 7406 .36 * Segments are parallel for multiple 7406 .36 * Add. solo 4 (12 Digits) \$11.00 7408 .36 * Add. solo 4 (12 Digits) \$11.00 7408 .36 * Add. solo 24 VDC (650 coil) \$1.50 EA. 7420 .25 * Add. subtract. multiply, and divide 7441 .25 .7420 .25 * Add. subtract. multiply, and divide 7441 .25 .7420 .25 * Add. subtract. multiply, and divide 7441 .25 .7421 .25 * Add. subtract. multiply, and divide 7441 .25 .7441 .25 * Add. subtract. multiply, and divide 7441 .25 .7441 .25 * Add. subtract. multiply, and divide 7441 .25 .7441 .25 * Add. subtract. multiply, and divide 7441 .25 .7441 .25 * Add. subtract. multiply, and divide .7441 .25 .7441 .25 * Complete With .5.00 .5.00 .745 .7400	<pre># Similar to (LITRONIX) DL337 # Magnified digit approximately</pre>	. 1"	74H01	. 35
e 5-10 MA per segment 7408 7008 <t< th=""><th><pre># Lathode for each digit # Segments are parallel for mult operation</pre></th><th>iple</th><th>74H04 7405</th><th>. 35 . 28</th></t<>	<pre># Lathode for each digit # Segments are parallel for mult operation</pre>	iple	74H04 7405	. 35 . 28
POTTER & BRUMFIELD Type KHP Relay 4 for 3a Contacts Avoc (650 coil) \$1.50 EA. Avoc (10.5 MA coil) \$1.50 EA. Avoc (10.5 MA coil) \$1.50 EA. Avoc (10.5 MA coil) \$1.50 EA. Add, subtract, multiply, and divide 12-Digit display and calculate Chain calculations The credit balance sign output Automatic overflow indication Fried decimal point at 0.2,3, or 4 Leading zero suppression DATA ONLY (refundable with purchase of chip). Durit on Digital Display Tube, incan- descent 5-volt 7-segment: .6" High numeral visible from 30 ft Standard 9-pin base (solderable) Leath and decimal point EACH \$5.00 DMETER KI MALANA COMPLETE KIT only \$11.95; FULLY-ASSEM Standard 9-pin base (solderable) Leath Avd seven-segment driver, and RA DE2010. COMPLETE KIT only \$11.95; FULLY-ASSEM Standard 9-pin base (solderable) Leath Avd seven-segment driver, and RA day 23%. These are used, no sche matic is available. CompLETE KIT only \$11.95; FULLY-ASSEM Standard 9-pin base (solderable) Leath Avd 5200. CompLETE KIT only \$11.95; FULLY-ASSEM Standard 9-pin base (solderable) Leath Avd 5200. CompLETE KIT only \$11.95; FULLY-ASSEM Standard 9-pin base (solderable) Standard 9-pin base (solderable) CompLETE KIT only \$11.95; FULLY-ASSEM Standard 9-pin base (solderable) Standard 9-pin base (solderable) CompLETE KIT only \$11.00 Complete Avd 9, 25%. Booldes, capactirs,	□ 5-10 MA per segment	\$11.00	7408	. 35
BRUMMFIELD 720 720 Type RP Relay 7400 7400 A voc (650 coil) \$1.50 EA. 7430 752 A voc (10.5 MA coil) \$1.75 EA. 7430 752 A off, subtract, multiply, and divide 7430 752 12.00 VAC (10.5 MA coil) \$1.75 EA. 7430 752 A off, subtract, multiply, and divide 7440 752 12.01 VAC (10.5 MA coil) \$1.75 EA. 7440 752 A off, trendsblance sign output 7441 753 A tota (coil) coil and tota (2,2,3, or 4 753 753 DATA ONLY (refundable with granthe coil 7,550 755 7453 750 A off, trendsblance sign output 7417 750 753 750 A off, trendsblance sign output 7417 750 751 750 751 750 750 751 750 751 750 751 750 751 750 751 750 751 750 750 751 750 751 750 751 750 751 750 751 750 751 750 751 750 751	POTTER &		7410 7413	.25
A PDT BA Contacts A PARAY A VOC (650 coil) \$1,50 EA. Add Contacts A VOC (650 coil) \$1,50 EA. Add Contacts A VOC (10.5 MA coil) \$1,75 EA. Add Subtract, multiply, and divide a Add, subtract, multiply, and divide Add Subtract, multiply, and divide a Add, subtract, multiply, and divide Fixed decimal point at 0,2,3, or 4 DATA ONLY (refundable with The credit balance sign output Add subtract, multiply, and point Fixed decimal point at 0,2,3, or 4 DATA ONLY (refundable with The credit balance sign output Add add subtract For Secont Scout Scout Complete with output For Secont Scout Complete with output For Secont Complete with output For Secont <th>BRUMFIE</th> <th>LD</th> <th>7420</th> <th>.25</th>	BRUMFIE	LD	7420	.25
24 v0C (650 coil) \$1.50 EA. 7430 2730 7430 7410 7410			74H20	. 35
100 The (1003 in 001) 91/13 LA 7440 7440 7440 7440 7440 7440 7440 7440 7440 7440 7440 7440 7442 1.20 a Ado matic all display and calculates a calculations 7442 1.20 7442 1.20 a Adomatic overflow indication a calculations 7442 1.20 7443 1.25 a Automatic overflow indication a calculations 7454 2.50 7455 2.5 DIA ONLY (refundable with purchase of chip) 51.00 7454 35.00 7455 2.5 RCA 2010 Numitron Digital Display Tube, incandescents-voil 7-segment 7477 4.60 7473 6.00 COMPLETE WITH DATA. 500 for \$20.00 7474 .60 CD - 2 COUNTER KIT 7474 .60 7473 .60 CACH SD.00 5 for \$20.00 7478 .60 7474 .60 CMADE Speenster segment driver, and RA MADI dodes, capacitors, traisitor, and resitors, A1 .7474 .60 .7478 .748 .748 .748 .748 .748 .748 .748 .7478 .7476 .7478<			74H30	. 25 . 35
add, subtract, multiply, and divide 742 1.20 add, subtract, multiply, and divide 7447 1.25 altonatic overflow indication 7451 25 attonatic overflow indication 7451 25 Prize credit balance sign output 7447 1.50 attonatic overflow indication 7451 25 DATA ONLY (refundable with purchase of chip) 56.95 7453 20 COMPLETE WITH DATA 56.95 7453 20 COMPLETE with DATA 56.95 7460 25 6." High numeral visible from 30 ft Standard 9-pin base (solderable) Left-hand decimal point EACH 95.00 5 FOR \$20.00 CDP-2 COUNTER KIT 7475 40 Unit includes board, 7490, 7475, quad latch, 7447 seven-segment driver, and RCA DR2010 7475 40 COMPLETE KIT only \$11.95; FULLY-ASSEM- BLD \$15.00; boards can be supplied separately at \$2.50 per digit. 7478 80 TAS 50, 20, 20 7478 7455 749 7455 740 COMPLETE KIT only \$11.95; FULLY-ASSEM- BLD \$15.00; boards can be supplied separately at \$2.50 per digit. 7478 80 TAS 50, 20, 20 7478 7478 80 <t< th=""><th></th><th></th><th>7440</th><th>.25</th></t<>			7440	.25
* Chain calculations 7450 .25 * True credit balance sign output 7450 .25 * True credit balance sign output 7450 .25 * Fixed decimal point at 0.2.3, or 4 .26 .7451 .25 * Fixed decimal point at 0.2.3, or 4 .26 .7451 .25 * Cade Composition .51.00 .7454 .20 * Munit on Digital Display Tube, incandes composition .7474 .20 * Composition .7490 .20 .7474 .20 * Composition .7490 .7490 .7490	# Add, subtract, multiply, and d	ivide	7441	1.20
n Automatic overflow indication 7451 .25 e Leading zero suppression 7451 .30 DATA ONLY (refundable with purchase of chip) .51.00 7454 .25 COMPLETE WITH DATA .56.95 741.54 .35 RCA 2010 .51.00 7454 .25 Numitron Digital Display Tube, incan- descent 5-volt 7-segment: .6" High numeral visible from 30 ft Standard 9-pin base (solderable) Left-hand decimal point .26 .4171 .00 Left-Hand decimal point .5608 \$20.00 .00 .4744 .60 CDP-2 COUNTER KIT .4174 .60 .4174 .60 Mata Att/3 seven-segment driver, and RCA pg2010 .4174 .60 .4174 .60 COMPLETE KIT only \$11.95; FULLY-ASSEM- BLED \$15.00; baards can be supplied separately at \$2.50 per digit. .400 .406 .65 Tam bat systems unit; 10 keys 0.9; 3 .60 .4195 .100 .4195 .10 Stand w/14 1M4001 ciodes, capacitors, transistor, and resistors, A11 moun- ted in an attractive case approx. 44 .449 .61 .4195 .10 74556 .150 .26 .200 .74105 .20 .74195 .200 <td>Chain calculations</td> <td></td> <td>7450</td> <td>.25</td>	Chain calculations		7450	.25
DATA ONLY (refundable with purchase of chip)	# Automatic overflow indication # Fixed decimal point at 0,2,3,		74L51	. 25
COMPLETE WITH DATA	DATA ONLY (refundable with	\$1 00	7453	. 20
Numitron Digital Display Tube, incan- descent 5-volt 7-segment: .6" High numeral visible from 30 ft Standard 9-pin base (solderable) Left-hand decimal point EACH 55.00 7473 30 Left-hand decimal point EACH 55.00 5 FOR \$20.00 7473 60 CD-2 COUNTER KIT Unit includes board, 7490, 7475, quad latch, 7447 seven-segment driver, and RCA DR2010. 7474 80 COMPLETE KIT only \$11.95; FULLY-ASSEM- BLED \$15.00; boards can be supplied separately at \$2.50 per digit. 7483 1.00 TRW Data Systems unit; 10 keys 0-9; 3 (or 4) 2 4V lamps; printed ci r c uit board w/l4 1N4001 diodes, capacitors, transistor, and resistors. All moun- ted in an attractive case approx. 44, x 4\\$ x 2\\$". These are used; no sche- matic is available. EACH 56.95 7-5EGMENT READOUT: First-quality, made by H-P, Lh-hand decimal point, segment pin-out same as MMA-L, common anode. EACH \$1.75 CMOOS ILINEARS NE560 3.25 CA302600 NE5667 C0400175 NE5603.25 CA3026100 NE5664.00 NB0 NE5603.25 CA302600 NE5667 NB0 NU5024 Red T0-1B High Dome @ 2V 5.20; 10/51.25 Die Kindow 100/510.00 MV5024 Red T0-1B king home @ 2V 5.20; 10/51.25 Die Ma10A with dia- grams for many ap- plications. EACH	COMPLETE WITH DATA	\$6.95	74L54 74L55	. 35
descent 5-volt 7-segment: .6" High numeral visible from 30 ft 7412 50 .6" High numeral visible from 30 ft .6" High numeral visible from 30 ft 7412 .50 Left-hand decimal point .6" High numeral visible from 30 ft .74173 .60 Left-hand decimal point .6" High numeral visible from 30 ft .74174 .60 Left-hand decimal point .6" High numeral visible from 30 ft .74174 .60 Unit includes board. 7490, 7475, quad .6" Att78 .80 .74174 .80 RCA DR2010.	Numitron Digital Display Tube,	incan-	74L71	. 30
Standard 9-pin base (solderable) 7473 75 Left-hand decimal point 7474 65 CD-2 COUNTER KIT 7474 66 Mit includes board, 7490, 7475, quad 7476 60 Iatch, 7447 seven-segment driver, and 7476 60 COMPLETE KIT only \$11.95; FULY-ASSEM 7480 65 Standard y 2:50 per digit. 7476 60 VOMPLETE KIT only \$11.95; FULY-ASSEM 7493 1.50 Standard y 4:52:50 per digit. 7495 1.15 MUT and resistors. All mounted in an attractive case approx. 4x x 4% x 2%". These are used; no scher 74173 75 CMADEARS Fors 516:00 CMOS CMOS CMOS LINEARS Segment allole. EACH 56.95 75 NE540	descent 5-volt 7-segment: .6" High numeral visible from	30 ft	74L72 7473	.50 .60
CD-2 COUNTER KIT Virt includes board, 7490, 7475, quad latch, 7447 seven-segment driver, and rest for seven leads of the supplication of the seven leads of the supplication of the suppli	Left-hand decimal point		74L73 7474	.75
latch, 7447 seven-segment driver, and RCA DR2010. 74278 .80 7480 .80 7490 .12 7495 .12 7495 .12 7495 .12 7495 .12 7495 .12 7495 .12 7495 .15 7495 .15 7495 .15 7495 .15 7495 .15 7495 .15 74195 .10 74180 .20 74180 .20 74180 .20 74180 .20 74180 .20 74180 .20 74180 .20 74180 .20 74180 .20 74180 .20 74200 .75 74220 .75 74220 <th></th> <th>ouad</th> <th>7475</th> <th>1.40</th>		ouad	7475	1.40
COMPLETE KIT only \$11.95; FULLY-ASSEMBLED \$15.00; boards can be supplied separately at \$2.50 per digit. 7489 4.00 COMPLETE KIT only \$11.95; FULLY-ASSEMBLED \$15.00; boards can be supplied separately at \$2.50 per digit. 7489 4.00 COMPLETE KIT only \$11.95; FULLY-ASSEMBLED \$15.00; boards can be supplied separately at \$2.50 per digit. 7489 4.00 Complete Kit only \$11.95; FULLY-ASSEMBLED \$1.50 7495 1.15 THE Data Systems unit; 10 keys 0.9; 3 74145 1.20 Yamasi tor, and resistors. All mounted in an attractive case approx. 44; 4 \$4, \$2, \$2". These are used; no schematic is available. EACH \$6.95 7-SEGMENT READOUT: First-quality, made by H - P, th-hand decimal point, segment pin-out same as MAN-1, common anode. Impos \$1.00 NE540\$2.00 NE555	latch, 7447 seven-segment drive	r, and	7480	.80 .65
COMPLETE KIT only \$11.95; FULLY-ASSEM- BLED \$15.00; boards can be supplied separately at \$2.50 per digit. 7492 90 7493 1.15 7495 1.15 7495 1.15 7495 2.00 74107 .70 74145 1.20 74133 1.50 74107 .70 74145 1.20 74133 1.50 74195 1.00 KEYBOARD ASSEMBLY TRW Data Systems unit; 10 keys 0-9; 3 (or 4) 2 4V lamps; printed cir c uit board w/14 1N4001 ciodes, capacitors, transistor, and resistors. All moun- red in an attractive case approx. 44 x 44 x 22". These are used; no sche- matic is available. EACH \$6.95 IM703 7-SEGWENT READOUT: First-quality, made by H- P, h-hand decimal point, segment pin-out same as YMN-1, common anode. EACH \$1.75 BPECIAL 10 F0# \$16.00 IM703 NE540 52:00 NE5563.25 CA30261.00 NE5663.25 LM309H00 74151.50 LM309H2.00 LM1595 4-quad. mult. S2.00 NUM5024 Red T0-18 High Dome @ 2V S.20; 10/S1.20 NUM-108 Visible Red S-70 MAC2V S.30; 10/S2.50 IMA-3 Seven-segment readout: EACH ONLYS1.25 10 0 R MORE, EACH1.00 MNA-1 LED 0isplay3.25 MN-10B Visible Red S-70 MAC2V S.30; 10/S2.50 IMA-3 Seven-segment treadout: EACH D1/S2.75 IMA-4 Seven-segment treadout: EACH D1/S2.75 IMA-3 Seven-segment diply-tested; leads plate	the mil		7489	4.00
BLED \$15.00; boards can be supplied separately at \$2.50 per digit. 74195 1.00 740.57 740.57 2.00 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74145 1.20 74155 1.00 Per siter. A day of the siter	COMPLETE KIT only \$11.95; FULLY-	ASSEM-	7492 7493	.90 1.15
KEYBOARD ASSEMBLY 74145 1.20 TRW Data Systems unit; 10 keys 0-9; 3 (or 4) 2 4 V lamps; pointed circuit; board w/14 1N4001 doides, capacitors, transistor, and resistors. All moun- matic is available. 74145 1.20 TRW Data Systems unit; 10 keys 0-9; 3 (or 4) 2 4 V lamps; pointed circuit; board w/14 1N4001 doides, capacitors, transistor, and resistors. All moun- matic is available. 74173 1.50 Tystematic is available. EACH 56.95 RF-1F amp epoxy 10-5. RF-1F amp epoxy 10-5. Tystematic is available. EACH 50.95 RF-1F amp epoxy 10-5. RF-1F amp epoxy 10-5. Tystematic is available. EACH 50.95 RF-1F amp epoxy 10-5. RF-1F amp epoxy 10-5. State Answer is MAN-1, common anode. CO40015.75 CD400175 NE540S2.00 NE5653.25 CA3045100 NE5653.25 CA3045100 RF-1F amp egulator chip 1- 40075 NE567 LM1051.25 Dewer Supply Seven-segment mult. S2.00 Seven Supply MV-508 Red Emitting 10-40 (Ale 2V S.20; 10/51.20 SIO H300430 MV-508 Red Emitting 10-40 (Ale 2V S.20; 10/52.50 RFIAC MV-508 Red Emitting 10-40 (Ale 2V S.20; 10/52.50 RFIAC MV-508 Red Emitting 10-40 (Ale 2V S.20; 10/51.20 RA4 600V BA To- 20EACH S.7	BLED \$15.00; boards can be su		74L95	2.00
(or 4) 24 V lamps; printed circuit 74195 1.00 toard w/14 IN4001 diodes, caracitors; 74195 1.00 wats z2". These are used; no schematic is available. EACH 56.95 7-SEGMENT READOUT: First-quality, made Power Support. R F - 1 F amperations ande. pin-out same as MAN-1, common ande. ID FOR 53.50 CMOOS NE540s2.00 Image: common ande. CD4001			74145 74180	1.20 1.25
transistor, and resistors. All moun- ted in an attractive case approx. 4% x 4% x 2%". These are used; no sche- matic is available. EACH 56.95 INTO 3 7-SEGMENT READOUT: First-quality, made pin-out same as MAN-1, common anode. EACH 51.75 special 10 F0% 516.00 RF-1F amp epoxy T0-5. LINEARS NE54052.00 CMOOS NE555150 74851.00 NE5563.25 CA3045100 C0402175 NE5653.25 CA3045100 742.00 NE5653.25 CA3045100 742.00 NE5653.25 CA3045100 Power Supply special: 00 NE5653.25 CA3045100 Power Supply special: 00 NE5653.00 (M302125 70945 LM3082.00 Power Supply special: 00 71075 LM311175 Power Supply special: 00/51.00 74155 LM309H00 Power Supply special: 00/51.00 74751.50 LM309H00 Power Supply spications. 74155 LM309H00 Power Supply spications. 74751.50 LM309H100 Power Supply spications. 74751.50 LM309H100 </th <th>(or 4) 24V lamps; printed cir</th> <th>cuit</th> <th></th> <th>1.50</th>	(or 4) 24V lamps; printed cir	cuit		1.50
matic is available. EACH \$6.95 epoxy T0-5. 7-SEGMENT READOUT: First-quality, made EACH \$6.95 EACH.5.45 by H - P, th-hand decimal point, segment 10 FOR \$16.00 CMOOS LINEARS CD40015.75 CD400275 NE54052.00 CD400175 CD401175 NE5503.25 CA3018100 CD402375 NE5653.25 CA3018100 CD402375 NE5653.25 CA3018100 NE567 NE5653.25 CA3045100 NE567 NE5664.00 LM1001.00 NE567 NE56745 LM302125 742(6053.25 T0-53.00 LM302125 742(6053.25 T0-53.00 LM3072.00 Netsof	transistor, and resistors. All ted in an attractive case approximately a	moun- ox. 44		
by H - P, Lh-hand decimal point, segment pin-out same as MAN-1, common anode. EACH 31.75 10 FOR \$3.50 LINE ARS NE540 \$2.00 CMOS LINE ARS NE555 1.50 CA3026 1.00 NE560 32.5 CA3026 1.00 NE561 3.25 CA3026 1.00 NE565 3.25 CA3026 1.00 NE565 3.25 CA3025 1.00 NE565 3.25 CA3045 1.00 NE565 3.25 CA3045 1.00 NE565 3.25 CA3045 1.00 NE565 3.25 CA3045 1.00 NE565 3.00 LM00 1.00 NE565 3.00 LM00 1.00 709 45 LM308 2.00 710 75 LM309H 1.00 741 51.50 LM309H 1.00 741 51.50 LM00Y 2.00 741 51.50 LM00Y 2.00 747 51.50 LM0Y 51.25 100/510.00 TRIAC 2V S.20; 10/51.26 <th>matic is available. EACH</th> <th>\$6.95</th> <th>ероху</th> <th>TO-5.</th>	matic is available. EACH	\$6.95	ероху	TO-5.
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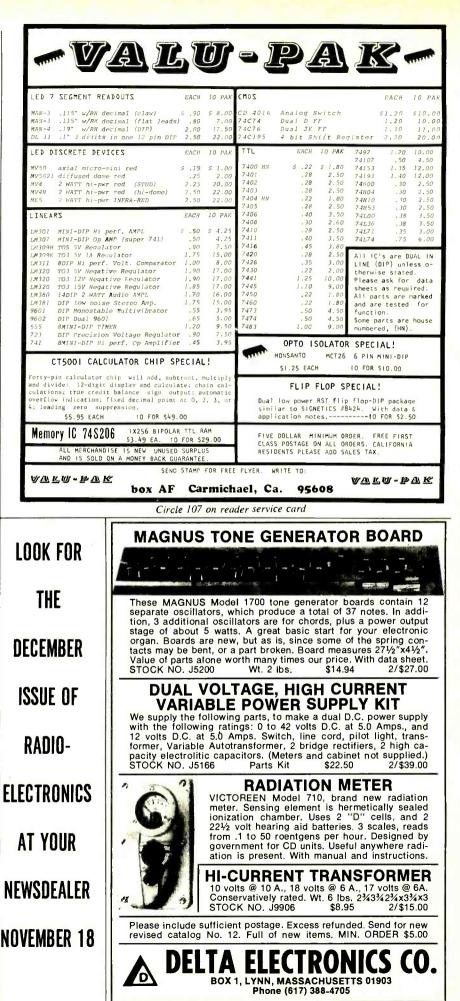
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Portable All-Transitorized 3* Sol 740 Clo 550 Portable All-Transitorized 3* Sol Sol 3* Sol Sol 3* Sol Sol <th>TEKTRONIX 3214</th> <th>TRANSISTOR SPECIALS</th> <th>C/MOS (DIODE CLAMPED)</th>	TEKTRONIX 3214	TRANSISTOR SPECIALS	C/MOS (DIODE CLAMPED)
3.7.5 e.a. 3/\$2.00 2/\$366 PPI \$100 C 3.60 MULTI-TURN TRIM POTS 2/\$366 PPI \$100 C 3.60 Similar to Bourns 3010 style 2/\$376 PPN \$102 C 5.55 Similar to Bourns 3010 style 2/\$376 PPN \$102 C 5.55 Si.00 c 2000, 5000, 1000 2000 FPN \$102 C 5.55 Si.00 e.a. 3/\$4.00 2/\$220 S 5.60 CD 4011 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 S 5.60 CD 4022 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 NPN \$51 0.56 S 5.60 CD 4022 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 NPN \$51 0.56 S 600 C 4022 S 5.55 Si.00 e.a. 5/\$1.75 600 Jan 151 5.5 a.00 400 Jan 151 5.5 a.00 MUE TUBES 5/\$1.75 500 DUF LECT - 4/\$1.00 KAMAA READOUT \$1.75 A0 600 Jan 151 5.5 a.00 Similar to Raytheon 8650 Joop FLAT AN SA 75 Solo F	Portable All-Transistorized 3".	2N256 PNP GE TO-3	\$ 50 74C 02 \$ 55
3.7.5 e.a. 3/\$2.00 2/\$366 PPI \$100 C 3.60 MULTI-TURN TRIM POTS 2/\$366 PPI \$100 C 3.60 Similar to Bourns 3010 style 2/\$376 PPN \$102 C 5.55 Similar to Bourns 3010 style 2/\$376 PPN \$102 C 5.55 Si.00 c 2000, 5000, 1000 2000 FPN \$102 C 5.55 Si.00 e.a. 3/\$4.00 2/\$220 S 5.60 CD 4011 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 S 5.60 CD 4022 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 NPN \$51 0.56 S 5.60 CD 4022 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 NPN \$51 0.56 S 600 C 4022 S 5.55 Si.00 e.a. 5/\$1.75 600 Jan 151 5.5 a.00 400 Jan 151 5.5 a.00 MUE TUBES 5/\$1.75 500 DUF LECT - 4/\$1.00 KAMAA READOUT \$1.75 A0 600 Jan 151 5.5 a.00 Similar to Raytheon 8650 Joop FLAT AN SA 75 Solo F	6MHz Triggered Scopes with 10:1	2N404 PNP GE TO-5	\$1.00 74C 10 \$.60
3.7.5 e.a. 3/\$2.00 2/\$366 PPI \$100 C 3.60 MULTI-TURN TRIM POTS 2/\$366 PPI \$100 C 3.60 Similar to Bourns 3010 style 2/\$376 PPN \$102 C 5.55 Similar to Bourns 3010 style 2/\$376 PPN \$102 C 5.55 Si.00 c 2000, 5000, 1000 2000 FPN \$102 C 5.55 Si.00 e.a. 3/\$4.00 2/\$220 S 5.60 CD 4011 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 S 5.60 CD 4022 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 NPN \$51 0.56 S 5.60 CD 4022 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 NPN \$51 0.56 S 600 C 4022 S 5.55 Si.00 e.a. 5/\$1.75 600 Jan 151 5.5 a.00 400 Jan 151 5.5 a.00 MUE TUBES 5/\$1.75 500 DUF LECT - 4/\$1.00 KAMAA READOUT \$1.75 A0 600 Jan 151 5.5 a.00 Similar to Raytheon 8650 Joop FLAT AN SA 75 Solo F	Probe	2N1137B PNP GE TO-3	\$.95 74C 157 \$2.15
3.7.5 e.a. 3/\$2.00 2/\$366 PPI \$100 C 3.60 MULTI-TURN TRIM POTS 2/\$366 PPI \$100 C 3.60 Similar to Bourns 3010 style 2/\$376 PPN \$102 C 5.55 Similar to Bourns 3010 style 2/\$376 PPN \$102 C 5.55 Si.00 c 2000, 5000, 1000 2000 FPN \$102 C 5.55 Si.00 e.a. 3/\$4.00 2/\$220 S 5.60 CD 4011 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 S 5.60 CD 4022 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 NPN \$51 0.56 S 5.60 CD 4022 S 5.55 Si.00 e.a. 3/\$4.00 2/\$220 NPN \$51 0.56 S 600 C 4022 S 5.55 Si.00 e.a. 5/\$1.75 600 Jan 151 5.5 a.00 400 Jan 151 5.5 a.00 MUE TUBES 5/\$1.75 500 DUF LECT - 4/\$1.00 KAMAA READOUT \$1.75 A0 600 Jan 151 5.5 a.00 Similar to Raytheon 8650 Joop FLAT AN SA 75 Solo F	MINIATURE TRIM POTS	2N1016A NPN Si TO-82	\$1.95 74C 165 \$3.50
4/2 X D-2 Signifier		MRS2202 NPN SI 10-82	\$2.50 CD 4001
4/2 X D-2 Signifier	5 7 5 an	2N3866 NPN Si TO-52	\$ 75 CD 4002
4/2 X D-2 Signifier	\$.75 ea. 3/\$2.00	2N2369 NPN Si TO-18	\$1.00 CD 4010 \$ 65
4/2 X D-2 Signifier	MULTI-TURN TRIM POTS	2N3767 NPN Si TO-66	5.70 CD 4011
4/2 X D-2 Signifier		2N2222 NPN Si TO-18	\$1.00 CD 4012\$.55
4/2 X D-2 Signifier		2N3055 NPN St T0-3	\$1.00 CD 4013\$1.20
4/2 X D-2 Signifier	50 100 500 2000 5000	2N6109 PNP Si T0-220	5.50 CD 4016
4/2 X D-2 Signifier	50, 100, 500, 2000, 5000,	2N4898 PNP Si TO-66	\$.60 CD 4022
4/2 X D-2 Signifier		MJ2252 NPN Si TO-66	\$.90 CD 4025 \$ 55
4/2 X D-2 Signifier	\$1.50 ea. 3/\$4.00	2N3638 NPN Si TO-5	\$1.00 CD 4027\$1.35
4/2 X D-2 Signifier	PRINTED CIRCUIT BOARD	2N2218A NPN SI TU-54/3	\$1.00 CD 4030\$.65
The Area of the analysis of the		CAPACITORS MAN	-1, Red or Yellow Full Wave Bridges
\$.40 ea. 5/\$1.75 IV IDUF FLECT 5/\$1 MANA READOUT \$2.00 200 39 124 400 Similar to Raytheon 8650 tubes, with socket and data sheet \$2.25 3/\$50.00 FLECT 5/\$1 501 COUNT ELECT 5/\$1 600 1.35 1.75 600 1.55 500 COUNT ELECT 5/\$1 600 1.55 1.55 5.00 1.00 200 .95 1.25 4.00 4.00 1.55 5.00 1.00 2.00 .01 1.55 5.00 1.00 2.05 5.01 CLOCK CHIP 6 0.01 1.55 1.05 5.01 CLOCK CHIP 6 0.05 CLOCK CHIP 6 0.05 CLOC	date board 1/" thick unstabled	20V / 7UF TANT 5/\$1 LEU	2 PEADOUT \$2.50 PRV 2A 6A 25A
Similar to Raytheon 8650 tubes, with socket and data sheet \$2.25 Similar to Raytheon 8650 tubes, with socket and data sheet \$2.25 Similar to Raytheon 8650 to 225 Similar to Raytheon 8650 to 2255 Similar to Raytheon 8650 to 225		12V 10UF ELECT 5/\$1 MAN	4 READOULT \$2 00 200 .95 1.25 4.00
Similar to Raytheon 8650 tubes, with socket and data sheet \$2.25 Similar to Raytheon 8650 tubes, with socket and data sheet \$2.25 Similar to Raytheon 8650 to 225 Similar to Raytheon 8650 to 2255 Similar to Raytheon 8650 to 225	\$.40 ea. 5/\$1.75	50V 100UF ELECT\$.40 SLA	3 400 1.15 1.50 5.00
Similar to Raytheon 8650 tubes, with socket and data sheet \$2.25 Similar to Raytheon 8650 tubes, with socket and data sheet \$2.25 Similar to Raytheon 8650 to 225 Similar to Raytheon 8650 to 2255 Similar to Raytheon 8650 to 225	NIXIE TUBES	25V 30UF ELECT4/\$1.00 RED	OR YELLOW \$4.50 600 1.35 1.75 6.00
Sined: Size: Size: <t< th=""><th></th><th>1103 1024 bit RAM\$4.75</th><th>5311 - CLOCK CHIP 6 DIGIT BCD</th></t<>		1103 1024 bit RAM\$4.75	5311 - CLOCK CHIP 6 DIGIT BCD
Sined: Size: Size: <t< th=""><th></th><th>NEC 6003 2048 bit RAM. \$9.50</th><th>HOLD COUNT, OUTPUT STROBE \$8.50</th></t<>		NEC 6003 2048 bit RAM. \$9.50	HOLD COUNT, OUTPUT STROBE \$8.50
2NA851 UIT 5:50 Nom 34.75 251.3 6.87X5 ER900 RIGGER 100 25.13 6.87X5 51.150 5.87X5 VERIPAX PC BOARD 5.75 File calculator keyboard. 4.74% 50.7% 51.81 56.0% This board is a 3/4" single sided (standard veripax). Points 57.95 57.95 57.95 57.95 This board is a 3/4" single sided (standard veripax). Points 57.95 57.95 57.95 57.95 Sho etched for .22 pin connections. IS. 7400 18 7485 100 0m as pacing 55.93 FLV 100 VISIBLE LED 5.50 7402 18 7486 47.92 75 Tob VISIBLE LED 5.50 7402 74.749 75 741.40 741.00 5.95 Tob VISIBLE LED 5.60 7402 74.749 75 741.40 741.00 75.95 Tob VISIBLE LED 5.60 7405 7405 720 700 77.94 723 741.00 741.00 741.00 741.00		1101 200 DIL RAW	DIAL OUTPUT STROPS
2NA851 UIT 5:50 Nom 34.75 251.3 6.87X5 ER900 RIGGER 100 25.13 6.87X5 51.150 5.87X5 VERIPAX PC BOARD 5.75 File calculator keyboard. 4.74% 50.7% 51.81 56.0% This board is a 3/4" single sided (standard veripax). Points 57.95 57.95 57.95 57.95 This board is a 3/4" single sided (standard veripax). Points 57.95 57.95 57.95 57.95 Sho etched for .22 pin connections. IS. 7400 18 7485 100 0m as pacing 55.93 FLV 100 VISIBLE LED 5.50 7402 18 7486 47.92 75 Tob VISIBLE LED 5.50 7402 74.749 75 741.40 741.00 5.95 Tob VISIBLE LED 5.60 7402 74.749 75 741.40 741.00 75.95 Tob VISIBLE LED 5.60 7405 7405 720 700 77.94 723 741.00 741.00 741.00 741.00		8223-PROGRAMMABLE	5316 - ALARM CLOCK CHIP \$12.50
ER80F U1 Stop 2M807 Stop Stop 2M807 Stop Stop 2M807 Stop Stop 2M807 S	TIS 73 N FET\$.50		2513 - 64x7v5
VERIPAX PC BOARD This board is a λ_i'' single side in the single of the second is a λ_i'' single side in the single of the second is a single side in the second is single side in the second is single side side in the	ER900 TRIGGER DIODES 4/61 00		CHARACTER GEN. \$11.50
VERIPAX PC BOARD This board is a λ_i'' single side in the single of the second is a λ_i'' single side in the single of the second is a single side in the second is single side in the second is single side side in the	2N6027 PROG. UIT \$.75	profile calculator keyboard A	2516 — 64x6x8 STATIC
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21 single 14 pin 1C/5 or 8, 16 74100 30 7476 478 476 478 478 478 478 478 478 478 478 478 478 478 478 478 478 478 477 477 477 479 477 477 479 477 477 479 477 477 479 477 477 479 477	VERIPAX PC BOARD	19SK-6 keyboard having 0-9, •,	SANKEN AUDIO POWER AMPS
21 single 14 pin 1C/5 or 8, 16 74100 30 7476 478 476 478 478 478 478 478 478 478 478 478 478 478 478 478 478 478 477 477 477 479 477 477 479 477 477 479 477 477 479 477 477 479 477	This board is a 1/6" single sided	$+, -, \times, -, =, K+C$ buttons with off on switch \$6.00	SI 1010 Y 10 WATTS
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Power Supply connections. Is also etched for 22 pin connect for. 7401- 18 74831.10 also etched for 22 pin connect for. \$5.25 7403- 18 7486- 48 M 309K 5V 1A REGULATOR \$1.65 FLV 100 VISIBLE LED \$.50 7405- 22 7490- 75 301/748-Hi Per. Op. Amp. \$.58 MCD-2 OPTO-ISOL \$.90 7407- 37 7491- 10 20 50 7405- 22 7490- 75 301/748-Hi Per. Op. Amp. \$.38 MCD-2 OPTO-ISOL \$.40 7407- 37 7491- 74 10 30 56 \$.50 GREEN GAP OSL-16 LED \$.60 7408- 24 7493- 75 7414 or 741C OP. AMP. \$.35 14 PIN DIP SOCKETS \$.40 7411- 30 7496- 95 3407-5 12 1.5 10 90 220 \$1.75 10 WATT ZENERS \$.30 EA 7416 37 7412- 50 36-FET INPUT OPER. AMP. \$1.05 \$1.65 \$2.20 7426-	21 single 14 pin IC's or 8, 16	74L0030 747647	
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FLV 100 VISIBLE LED .5.0 ME-4 IR LED .5.00 7406 .37 7491 .1.30 LM 320 -5 or -1.5 V REC S1.75 LM 320 -740 -0.40 V REGULATOR \$5.80 MCD-2 OPTO-ISOL .5.90 7406 .37 7491 -1.30 LM 320 -5 or -1.5 V REG \$1.75 GREEN GAP OSL-16 LED .5.40 7410 .18 7492 .75 7410 -7410 P.08 .33 14 PIN DIP SOCKETS .5.40 7411 .30 7495 .99 7902 OPER. AMP. \$.29 10 WATT ZENERS .5.50 7413 .75 74107 .50 101 OPER. AMP. HI PERFORM. \$.75 3.9, 5.6, 6.8 0R 12 V .5.30 EA .7412 .45 8200 .100 PAMP. \$2.60 Silicon Power Rectifiers .7426 .30 .74126 .10 .10 .10 PERCINON P. AMP. \$2.60 100 .06 .11 .30 <td< th=""><th></th><th></th><th></th></td<>			
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RED GAP OSL 3 LÉD \$40 7430 125 7430 743<	ME-4 IR LED 540	7405— .22 7490— .75	301/748-Hi Per. Op. Amp\$.35
RED GAP OSL 3 LÉD \$40 7430 125 7430 743<	MCD-2 OPTO-ISOI \$ 90		LM 320 -5 or -15 V REG\$1.75
14 PIN DIP SOCKETS	GREEN GAP OSL-16 LED\$.60	7408 24 7493 75	741A or 741C OP AMP \$ 35
14 PIN DIP SOCKETS	RED GAP OSL-3 LED	741018 749599	709C OPER. AMP. \$.29
10 WATT ZENERS 7413—.75 74107—.50 101 OPER. AMP, HI PERFORM\$.75 3.9, 4.7 OR 5.6 V		741130 749695	340T-5, 12, 15, 18, 24V
3.9, 9, 47 OR 5.6 V \$.75 EA. 7416—37 74121—60 IM 308 Oper. Amp., Low Power \$1.05 3.9, 5.6, 6.8 OR 12 V \$.30 EA. 7420—18 74125—1.40 530—FET INPUT OPER. AMP. \$2.60 Silicon Power Rectifiers 7427—33 74150—1.15 IM 390.0—QUAD OP. AMP. \$2.60 Var 7420—1.8 74150—1.15 IM 390.0—QUAD OP. AMP. \$2.60 100 .06 .11 .30 80 7432—30 74151—95 200 .07 .16 .35 1.15 7438—37 74157—1.25 565—PHASE LOCK LOOP \$2.60 200 .07 .16 .35 1.10 7440—21 7416—1.55 565—PHASE LOCK LOOP \$2.60 400 .09 .20 .50 1.40 7442—1.00 74163—1.60 565—PHASE LOCK LOOP \$2.60 600 .11 .25 .70 1.80 7442—1.00 74163—1.60 555—2.24 \$2.81 \$1.55 800 .15 .35 .90 2.00 7445—1.10 74174—1.80 \$1.85 \$1.85 1000 .20 .45 1.10 2.60 7445—1.10		741245 8220-1.50	POS. REG. TO-220 \$1.75
7417—37 74123—100 747—0UAL 741 5.76 3.9, 5.6, 6.80 N12 V 5.30 EA 7417—37 74123—100 747—0UAL 741 5.76 Silicon Power Rectifiers 7427—33 74126—1.40 536—FET INPUT OPER AMP. \$2.60 7427—33 74126—1.40 537—PRECISION OP. AMP. \$2.60 PRV 1A 3A 12A 50A 7432—33 74150—1.15 LM 3900—QUAD OP. AMP. \$2.60 100 .06 .11 30 80 7437—44 74153—1.10 560—PHASE LOCK LOOP \$2.60 200 .07 .16 .35 1.15 7440—2.1 74163—66 567—TONE DECODER \$2.95 400 .09 .20 .50 1.40 7417—31.80 \$7415—1.25 566—PHASE LOCK LOOP \$2.60 600 .11 .25 .70 1.80 7441—1.05 74164—2.05 TM370—AGC SQUELCH AMP. \$1.55 1000 .20 .45 1.10 2.60 7446—1.15 74176—1.80 \$32—TRANSISTOR ARARY \$.95 1000 .20 .45 1.10 2.60 7447—1.15 74176—1.80	10 WATT ZENERS		IM 308 Oper Amp Low Power \$1.05
3.9, 5.6, 6.8 OR 12 V	4 WATT ZENERS	7417-37 74123-1.00	747_0141 741 \$ 75
100 06 .11 .30 .80 100 06 .11 .30 .80 200 .07 .16 .35 1.15 400 .09 .20 .50 1.40 600 .11 .25 .70 .80 600 .11 .25 .70 .80 7442 .10 .74154 .100 .66 600 .11 .25 .70 .80 7442 .10 .74163 .100 .66 7442 .10 .74164 .205 .703 .747 800 .15 .35 .90 .20 .7445 .10 .74173 .80 1000 .20 .45 1.10 2.60 .7445 .115 .74176 .80 .7242 .74176 .80 .7242 .74181 .30 .80 .7442 .116 .74176 .80 .72 .80 .73 .43 .74192 .80 .7442 .74176 .80 .74183 .74176 .80 <	3.9, 5.6, 6.8 OR 12 V\$.30 EA.	7420	536-FET INPUT OPER. AMP. \$2.60
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800 15 .35 90 2.20 1000 .20 .45 1.10 2.60 REGULATED MODULAR POWER SUPPLIES 7416-1.15 74176-1.80 585-2 2.65 2.46 1.10 2.60 + .15 74176-1.15 74177-1.80 8822-TRANSISTOR ARRAY .95 Atta .10 2.60 7446-1.15 74177-1.80 8822-TRANSISTOR ARRAY .95 M300-2W AUDIO AMP .260 7446-1.15 74177-1.80 100 3822-TRANSISTOR ARRAY .95 -15VDC AT 100 ma, .7474-43 74192-1.50 100 381-STEREO PREAMP \$1.51 5VDC AT 1A, 115VAC \$19.95 7474-43 74195-1.00 100 319-DULA HUIP COMPARATOR \$165 INPUT \$19.95 747575 759491-1.10 TRIACS SCR'S IN 4148 14/\$1.00 sign square and triangular out oot triangular out triangular out oot triangular out triangular out triangular out triang		7442-1.00 74165-2.05	
REGULATED MODULAR POWER SUPPLIES 7448—1.20 7472—40 74181—3.60 7472—40 74181—3.60 74192—1.50 M37/—2w Stereo Audio Amp. \$2.60 + —15VDC AT 100 ma, 115VAC INPUT \$19.95 7472—40 74192—1.50 M382—DUAL AUDIO PREAMP \$1.75 5VDC AT 10, INPUT \$19.95 7474—4.3 74195—1.00 M319—Dual Hi Speed Comp. \$1.25 INPUT \$19.95 7475—7.75 75491-1.10 X333—OUAD COMPARATOR \$1.65 IN 4148 14/\$1.00 Similar to 8038C IC Voitage controlled oscillator, as fea tured in Oct. 73 P.E. they have sine square and triangularout puts good to IMHz. Two of check or Money Order. Include postage. Minimum Order \$3.00. FM generator 100 400 1.01 1.50 2.60 1.00 200 .70 1.30 200 .20 200 .20<	800 .15 .35 .90 2.20	7445-1.10 74173-1.80	555-2 µs - 2 HR. TIMER\$.98
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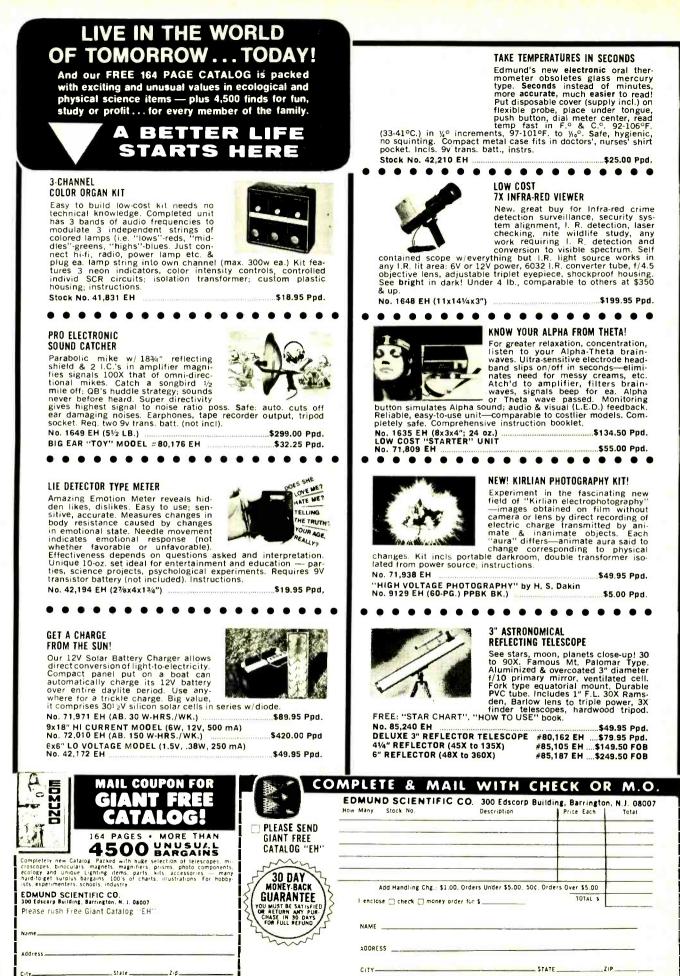
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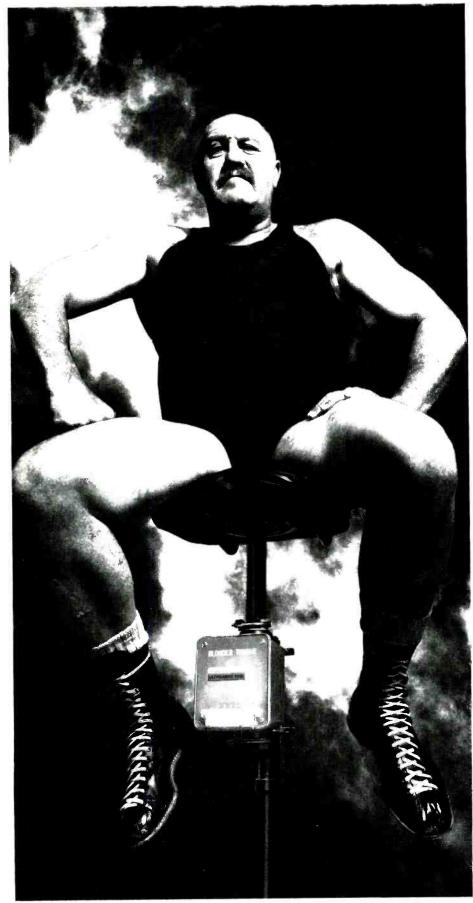
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